

# PROJECT MOORETOWN 220 kV SUBSTATION

Drainage and Water Services Report





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PROJECT CIRRUS  
Drainage and Water Services Report

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# 1. Introduction

This document provides a brief description of the proposed drainage and water services works adopted in the design and general requirements.

It is provided to assist understanding of the development proposals and the clients design requirements only and does not supersede in any way the requirements of the contract, drawings specifications and other documents formally issued for the works.

## 1.1 Site

The site is located approximately 500m north of the N2 / M50 junction in Huntstown, Co. Dublin. The land is currently in agricultural use and has an area of circa 12.95 hectares (32.15 Acres). Field boundaries are fenced with hedges and trees on all sides. A small existing watercourse runs roughly south to north through the site and will be diverted as part of the design as noted below. The land is generally flat, there are slight slopes to the watercourse and to the north with low points along the watercourse.

## 1.2 Development Description

The development by Huntstown Power Company located at Huntstown, Co. Dublin involves the construction of a new electrical substation and associated grid connection (known as the Customer Compound), which will serve the site including a proposed Data Centre development which will be located immediately to the east of the development, as well as any future development on the wider landholding. The details contained in this strategy and application include information relating to elements of the concurrent planning application for the Data Centre under application Ref FW21A/0151.

A separate Drainage and Water Services report has been produced by Clifton Scannell Emerson Associates (CSEA) for the Data Centre which is included in Appendix A of this report which takes into account surface and foul drainage discharges from the substation and Customer Compound identified in this report.

Whilst it is the intention that in the permanent condition the substation and the Customer Compound drainage systems will be connected into the Data Centre drainage network, the drainage design has been planned to accommodate any possible delay to the construction of the Data Centre to allow both areas to operate as standalone drainage systems prior to the Data Centre being constructed however this will necessitate incorporating part of the works previously intended to form part of the Data Centre scheme as noted below:

- Forming a road access to the south of the site off of the existing campus road including associated drainage works.
- Installation of a 900 diameter ditch diversion. Refer Section 5 of CSEA's Drainage and Water Services report in Appendix A
- Construction of an attenuation basin to the north of the site. Refer Clifton Scannell Emerson Associates (CSEA) drawing 20\_099-CSE-00-XX-DR-C-2116 in Appendix B.

## 2. Drainage

### 2.1 Surface Water

The proposed development will be connected to a SUDS facility to provide attenuation in compliance with the requirements of the Greater Dublin Strategic Drainage Study (GDSDS). The following section outlines the surface water drainage proposals for the development for each area. All SUDS elements have been designed as per the recommendation of the SuDS Manual 2015. All surface water works including connections will be carried out in accordance with the Greater Dublin Regional Code of Practice for Drainage Works.

The sites for the EirGrid substation and Customer Compound will provide a first level of SUDS treatment described below and a final treatment together with attenuation will be provided in the attenuation basin to the north of the site. This basin will, in the temporary condition, provide attenuation for the substation and Customer Compound and in the permanent condition, will also form part of the attenuation system for the Data Centre.

#### 2.1.1 EirGrid Compound

A surface water drainage network separate from the adjacent Customer Compound will be formed via a solid walled pipe system. Pipes will be used, connected to a Class 1 full retention interceptor prior to discharge to the attenuation basin which will provide the final treatment and attenuation from the compound.

It is proposed that the interceptor, installed downstream of the compound surface water network and upstream of the attenuation basin, will be a Class 1 full retention interceptor designed to accept and treat the full design flow delivered in the surface water drainage system.

A system of road gullies and linear drainage channels will direct the surface water run-off from the impermeable areas into the surface water system with manholes and catch pits located on all drains to minimise silt transfer and intercept contamination.

During oiling of transformers surface water drainage from the road area can be closed off after the interceptor to prevent a catastrophic large volume leak of oil reaching the SUDS treatment.

#### 2.1.2 Customer Compound

The proposed surface water drainage will be similar to that proposed for the EirGrid compound above with a series of gullies and linear drainage channels collecting surface water run-off from the compound access road and yard connecting into a solid walled pipe system.

Drainage will discharge into a full retention Class 1 interceptor prior to discharge into the attenuation basin for final treatment and attenuation.

Transformer bases will provide for a leak retention of a minimum of 110% of the stored oil in the transformer. Surface water from each will be pumped from the sump via an Aquasentry pump and monitoring system which will shut down and alarm in the event of oil contamination.

Surface water from the normal delivery of the pumps will discharge to the surface water pipes and Class 1 interceptor system to prevent contamination.

A surface water ditch diversion pipe as noted in Item 1.2 above is shown within the Customer Compound. This diversion will require to be installed to provide a temporary surface water connection for the southern access road drainage system and to allow the construction of the Customer Compound. For details of the proposed ditch diversion refer to Section 5 in CSEA's Drainage and Water Services in Appendix A.

## 2.2 Foul Drainage

### 2.2.1 EirGrid Compound

The pipe network is designed in accordance with the requirement of Table 6.4 of the Greater Dublin Strategic Drainage Study

The proposed foul water network collects foul water flows from the toilet, shower and mess facilities within the GIS building.

The substation building is an unmanned facility with visiting maintenance crews. This is generally a two man crew visiting site for two days per month.

As a result, this development is not covered by the types of activities listed in Appendix D of the Irish Water Code of Practice for Wastewater Infrastructure. Accordingly, proposed wastewater flows have been based on the assumed usage rates of the appliances in the building.

The proposed foul water flows from the development are estimated to be a maximum of 400l/day during occupation, with a peak discharge of 1.6l/sec during an 8hr shift period.

Drainage from the GIS building will be gathered to a centrally located manhole where, in the permanent condition, it will then be pumped offsite to the adjacent Data Centre private sewer (refer to CSEA drawing 20\_099-CSE-00-XX-DR-C-2210 in Appendix B and Section 3 of CSEA's Drainage and Water Services report in Appendix A). The route, flows and general levels of the rising main has been agreed with the Data Centre designers and allows for local flow buffering at the pump station before discharge. In this condition the foul drainage from the GIS building will be drained to a cesspool and tankered off-site for disposal.

The proposed network will adhere to the minimum pipe gradients set out in Table 6 of the "Building Regulations Technical Guidance Document H". It is proposed to take all foul drainage from the buildings by means of 100mm $\varnothing$  pipes with minimum gradients of 1:60 which connect to 150mm $\varnothing$  pipes laid at minimum gradients of 1:100. The key design parameters are summarised as follows:-

- Minimum Self-Cleansing Velocity for Gravity Sewer = 1.0 m/s;
- Minimum gradient of gravity sewer = 1:60
- Roughness Co-efficient for Gravity Sewer (ks) = 0.6mm

### 2.2.2 Customer Compound

There is no proposed foul water network for the Customer Compound area.

## 3. Water Supply

A water supply will be provided from the Huntstown Power Station private water supply. A peak water demand of 400 litres/day during an 8 hour occupied shift has been allowed. Due to the gaps in use from the supply, potable water will be imported bottled water.

## 4. Firefighting Water

No provision is required within the EirGrid substation or Customer Compounds.

## 5. Schedule of Aecom Drawings

Drawing No. 60641561-DWG-713 Outline Drainage Layout

## 6. Framework of Specifications (EIRGRID)

Not applicable.

# **Appendix A - CSEA Engineering Planning Report – Drainage and Water Services for Huntstown Data Centre Facility (produced by Clifton Scannell Emerson Associates)**

20\_099-CSE-00-XX-RP-C-005

Engineering Planning Report - Drainage and Water Services





**Clifton Scannell Emerson**  
Associates

# Engineering Planning Report - Drainage and Water Services

## Huntstow Data Centre Facility

**energia**  
group

Client: Huntstow Power Company  
Ltd.

Date: 9<sup>th</sup> April 2021

Job Number: 20\_099

Civil  
Engineering

Structural  
Engineering

Transport  
Engineering

Environmental  
Engineering

Project  
Management

Health  
and Safety

CONSULTING ENGINEERS



## Document Control Sheet

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Filename: 20\_099-CSE-00-XX-RP-C-005

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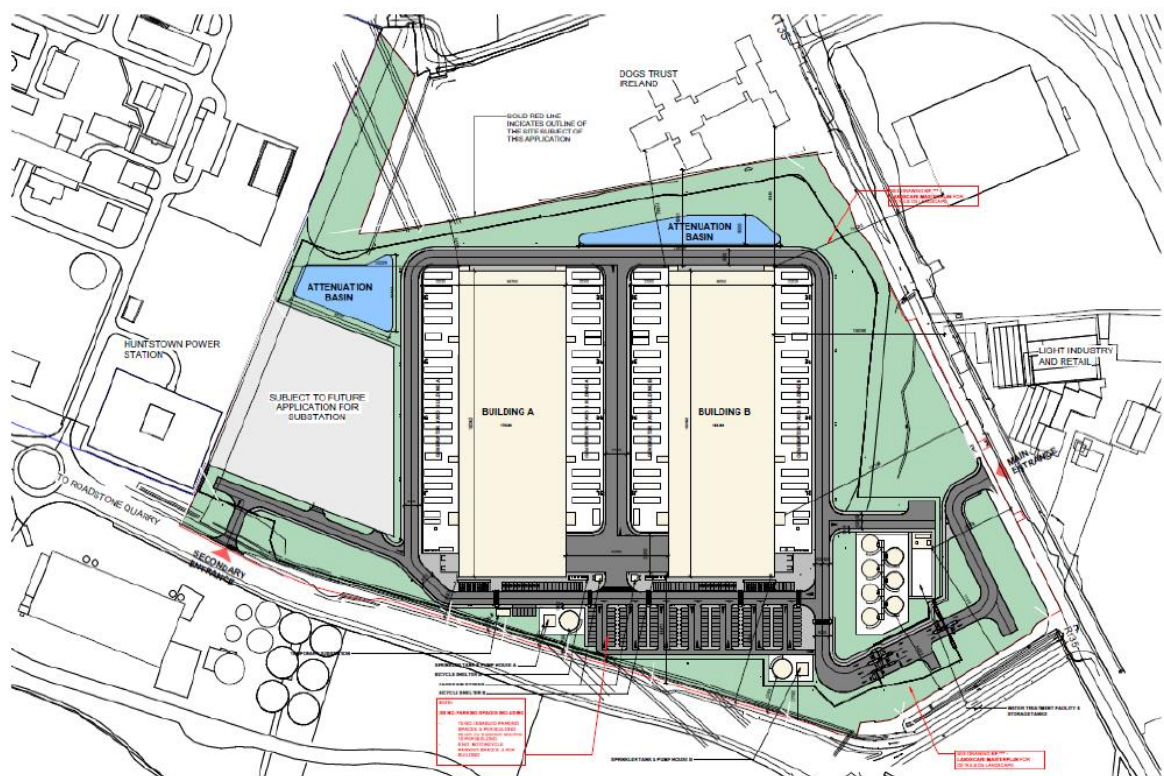
## 1 Introduction

This report is being submitted as part of the planning application for Energia Group for the proposed data storage facility and energy centre development on site at Huntstown, Dublin 11. The report outlines the proposals for drainage services, water supply and flood risk assessment for the development. The proposed development site is approximately 13.30 Hectares in size.

### 1.1 Development Description

The proposed development of a greenfield site of approximately 13.30 Hectares. It is located approximately 500m north of the N2 / M50 junction in Huntstown, Co. Dublin. The development will consist of the construction of two separate data centre buildings to be constructed over a 10 year period.

Huntstown Power Company Limited, intends to seek permission for the development of 2 no. data hall buildings and ancillary structures on this site. The extent of the site layout is highlighted in Figure 1.1 below:-



**Figure 1.1 – Proposed Site Masterplan**

The proposed development is described as follows:

- Demolition of 2 no. existing residential dwellings to the east of the site (c. 344 sqm in area);
- Construction of 2 no. data hall buildings (Buildings A and B) comprising data hall rooms, mechanical and electrical galleries, ancillary offices including meeting rooms, workshop spaces, staff areas including break rooms, toilets, shower/changing facilities, storage areas, lobbies, loading bays and docks, associated plant throughout, photovoltaic panels and screened plant areas at roof levels, circulation areas and stair and lift cores throughout;

- External plant and 58 no. generators located within a generator yard to the east and west of Buildings A and B at ground level. The area is enclosed by a c.6.5m high louvred screen wall;
- The proposed data halls (Buildings A and B) are arranged over 3 storeys with a gross floor area of c.37,647sqm each;
- The overall height of the data hall buildings is c.28m to roof parapet level and c.32m including roof plant, roof vents and flues. The total height of Buildings A and B does not exceed 112m OD (above sea level);
- The proposed development includes the provision of a temporary substation (c.32sqm), water treatment building (c. 369sqm and c.7.5m high), 7 no. water storage tanks (8,200m<sup>3</sup> c.6.35m high), 2 no. sprinkler tanks (c.670m<sup>3</sup> each and c.7.2m high) with 2 no. pump houses each (c.40sqm c.6m high);
- The total gross floor area of the data halls and ancillary structures is c.75,775sqm;
- All associated site development works, services provision, drainage upgrade works, 2 no. attenuation basins, landscaping and berming (c.6m high), boundary treatment works and security fencing c.2.4m high, new vehicular entrance from the North Road, secondary access to the south west of the site from the existing private road, all internal access roads, security gates, pedestrian/cyclist routes, lighting, 2 no. bin stores, 2 no. bicycle stores serving 48 no bicycle spaces, 200 no. car parking spaces and 8 no. motorcycle parking spaces;
- A proposed 220kv substation located to the south west of this site will be subject of a separate Strategic Infrastructure Development application to An Bord Pleanála under section 182A of the Planning and Development Act 2000 (as amended);
- An Environmental Impact Assessment Report (EIAR) is submitted with this application.

## **1.2 Existing Land Use**

The existing site is a greenfield site which is currently used as agricultural land.

## 2 Surface Water Drainage

### 2.1 General

The proposed development will provide attenuation in compliance with the requirements of the Greater Dublin Strategic Drainage Study (GDSDS). The following section outlines the surface water drainage proposals for the development. All SUDS elements have been designed as per the recommendation of the SuDS Manual 2015.

All surface water works including connections will be carried out in accordance with the Greater Dublin Regional Code of Practice for Drainage Works.

### 2.2 Drawings

The following drawings are provided in support of the planning application to surface water drainage

- Drawing No. 20\_099-CSE-00-XX-DR-C-2110 Proposed Overall Surface Water Drainage Layout
- Drawing No. 20\_099-CSE-00-XX-DR-C-2111- Proposed Surface Water Drainage Sheet 1
- Drawing No. 20\_099-CSE-00-XX-DR-C-2112- Proposed Surface Water Drainage Sheet 2
- Drawing No. 20\_099-CSE-00-XX-DR-C-2115 Surface Water Attenuation Basin 1 Plan and Sections
- Drawing No. 20\_099-CSE-00-XX-DR-C-2116 Surface Water Attenuation Basin 2 Plan and Sections
- Drawing No. 20\_099-CSE-00-XX-DR-C-2910 Standard Trench Details
- Drawing No. 20\_099-CSE-00-XX-DR-C-2911 Proposed Drainage Details Sheet 1
- Drawing No. 20\_099-CSE-00-XX-DR-C-2911 Proposed Drainage Details Sheet 2
- Drawing No. 20\_099-CSE-00-XX-DR-C-2911 Proposed Drainage Details Sheet 3

### 2.3 Existing Surface Water Network

There is no drainage system currently serving the site. The lands fall to the north west of the site and are bordered by a drainage ditch which flows to the Huntstown Stream which is a tributary of the Ward River. The ditch in question joins the Ward approximately 5 km north east of the site.



## 2.4 Proposed Surface Water Network

### 2.4.1 Overview

The proposed surface water networks for the development collect runoff from roofs, roads and other hard standing areas in a sealed system of pipes and gullies. There are two separate surface water drainage networks in the proposed development which flow to separate surface water attenuation basins (Refer to Drawing No s 20\_099-CSE-00-XX-DR-C-2115 and 20\_099-CSE-00-XX-DR-C-2116) from which attenuated flows are discharged, via carrier drains, to the adjacent ditch, described in Section 2.3, adjacent to the north west corner of the site.

### 2.4.2 Surface Water Network Design

The pipe network is designed in accordance with the requirement of Table 6.4 of the Greater Dublin Strategic Drainage Study (GSDSDS) See Fig 2.1 below.

| Parameter                        | Surface Water Sewers  |
|----------------------------------|---|
| Minimum depth                    | 1.2m cover under highways<br>0.9m elsewhere   |
| Maximum depth                    | Normally 5m   |
| Minimum sewer size               | 225mm   |
| Runoff factors for pipe sizing   | 100% paved and roof surfaces<br>0% off pervious surfaces  |
| Rainfall for initial pipe sizing | 50mm/hr rainfall intensity  |
| Minimum velocity (pipe full)     | 1.0m/s  |
| Flooding                         | Checks made for adequate protection *<br>No flooding for return period less than 30 years except where explicitly planned<br>Simulation modelling is required for sites greater than 24ha** |
| Roughness – ks                   | 0.6mm   |

**Fig 2.1 – GSDSDS Pipe Design Criteria**

In addition to the criteria outlined in Fig 2.1 no flooding of buildings will occur for return periods less than 100 years. Car parks and roadways may flood between 30-100 years. Simulation, drainage design and site levels should take account of this criteria.

Manholes shall be provided at junctions in the network, at changes of direction and gradient and at no more than 90m centres.



The surface water pipe network has been modelled using WinDes™ software and detailed calculations are provided in Appendix A.

### 2.4.3 Pollution Control Measures

It is proposed to provide a number of full retention hydrocarbon interceptors in the surface water drainage scheme.

Due to generator refuelling activities taking place on roads throughout the development it is proposed to provide a Class 1 full retention separators downstream of all roads and upstream of the proposed surface water attenuation basins in accordance with Section 20 of the Greater Dublin Regional Code of Practice. The full retention separator is designed to treat the full design flow that can be delivered in the drainage system, which is normally equivalent to the flow generated by a rainfall intensity of 50mm/hour.

There is potential for surface water and condensate to accumulate in the exhaust stacks which serve the generators. Gullies which serve the exhaust stacks will discharge to a dedicated surface water drainage pipe which will be connected to a Class 1 full retention separator. Two full retention interceptors will be required per building to serve the exhaust stacks.

Details of the full retention separator proposed are provided in Appendix B to this report and are outlined in Table 2.1 below.

| Ref  | Type           | Class | Model Specification<br>(by Klargestor or equivalent) | Design Flow Rate (l/s) | Oil Capacity (l) |
|------|----------------|-------|--|------------------------|------------------|
| PI-1 | Full Retention | 1     | NSFP003  | 3                      | 30               |
| PI-2 | Full Retention | 1     | NSFA200  | 200                    | 2000             |
| PI-3 | Full Retention | 1     | NSFP003  | 3                      | 30               |
| PI-4 | Full Retention | 1     | NSFA200  | 200                    | 2000             |
| PI-5 | Full Retention | 1     | NSFP003  | 3                      | 30               |
| PI-6 | Full Retention | 1     | NSFP003  | 3                      | 30               |
| PI-7 | Bypass         | 1     | NSBE020  | 20                     | 300              |

**Table 2.1 – Petrol Interceptor Details**

In addition to the full retention separators two hydrodynamic solid separators will also be provided within the drainage network to screen rubbish, debris and sediment from the surface water runoff before it enters the attenuation pond.

Details of the hydrodynamic solid separator proposed are provided in Appendix C to this report.

#### **2.4.4 Proposed Permeable Paving**

It is proposed to provide permeable paving in the car parking areas to the south of the development in order to reduce the hard standing areas discharging to the surface water drainage network insofar as possible. Locations where permeable paving is being proposed is indicated on Drawing No. s 20\_099-CSE-00-XX-DR-C-2021 and 20\_099-CSE-00-XX-DR-C-2022 and details of the permeable paving system is indicated on Drawing No. s 20\_099-CSE-00-XX-DR-C-2900.

#### **2.4.5 Surface Water Attenuation**

The surface water network has been designed to provide sufficient capacity to contain and convey all surface water runoff associated with the 1 in 100 year event to the attenuation basins without any overland flooding. This complies with Criterion 3 of Table 6.3 of Volume 2 of the GDSDS.

All calculations have allowed for an additional allowance of 10% in rainfall intensities to allow for climate change as per Table 6.1 of Volume 2 of the GDSDS.

The allowable discharge rate from the site (QBAR) has been calculated in accordance with the following equation as per Section 6.3.1.2.2 of the GDSDS. Calculations are provided D to this report.

The proposed development will have two attenuation basins, one located to the north of the site and a second basin located to the west of the site. The total allowable discharge from the site has been calculated as 28.26 l/s which has been split between the attenuation basins with 12.0 l/s discharging from the north basin and 16.26 l/s discharging from the west basin. Discharge from both basins will be controlled by hydrobrake vortex control units as outlined below and details are provided in Appendix E:-

- Attenuation Basin 1 (North) SHE-0143-1200-2000-1200
- Attenuation Basin 2 (West) - SHE-0174-1650-1600-1650

Analysis of the Windes<sup>TM</sup> results for the data storage facility's drainage network identified the 240 minute winter storm during the 1 in 100 year return period as the critical storm in terms of attenuation storage volume. The design information for both attenuation basins is outlined below. See Appendix A for details of the Windes<sup>TM</sup> calculations.

##### **Attenuation Basin 1 (North)**

- Basin Invert Level = 76.704m OD
- Proposed Ground Level at Basin = 79.00m approx.
- Discharge Rate = 12 l/s
- Design Head = 2.0m
- Critical Storm Event = 240 Minute Winter
- High Water Level during 1 in 100 year event = 78.704m

- Storage Volume required for proposed development = 1,233m<sup>3</sup>

#### **Attenuation Basin 2 (West)**

- Basin Invert Level = 75.800m OD
- Proposed Ground Level at Basin = 77.60m approx.
- Discharge Rate = 16.26 l/s
- Design Head = 1.6m
- Critical Storm Event = 240 Minute Winter
- High Water Level during 1 in 100 year event = 77.390m
- Storage Volume required for proposed development = 2,439m<sup>3</sup>

Attenuation Basin 2 has additional capacity to facilitate the development of the proposed GIS substation which is being carried out by others.

## **2.5 Rainwater Harvesting**

It is proposed to provide 6000 litre rainwater harvesting tanks to serve grey water usage in the Administration Area of both buildings. The roof downpipes serving the Administration Area will be connected upstream of the rainwater harvesting tanks and rainwater will be pumped into the building plumbing system to serve grey water usage purposes. An overflow will be provided to the main surface water drainage system.

It is possible that rainwater harvesting from the data hall roof of Building B could be used to augment the cooling water supply. This will be subject to a full cost benefit analysis and detailed design.

## **2.6 Surface Water Drainage Design Summary**

The proposed surface water drainage network has been designed in accordance with GDSDS and Greater Dublin Regional Code of Practice. The proposed surface water network flows in a north westly direction and is attenuated before discharging to the Huntstown Stream. The allowable discharge from the site is 28.26 l/s and the total attenuation storage volume provided is 3,672 m<sup>3</sup> in two attenuation basins. A number of petrol interceptors are provided throughout the network to manage water quality and permeable paving has been provided in car parking areas in order to minimise surface water runoff.

## **3 Foul Water Drainage**

### **3.1 General**

A pre-connection enquiry (PCE) form was submitted to Irish Water on 26<sup>th</sup> July 2020 which addressed water and wastewater demand for the development. The reference number for the Pre-Connection Enquiry is CDS 200004468. Irish Water subsequently provided a Confirmation of Feasibility (CoF) on 31<sup>st</sup> March 2021 (Refer to Appendix F for details) which indicated that it is feasible to connect foul water flows from the proposed development without any infrastructure upgrades by Irish Water. It is proposed to outfall the foul drainage from the site to the existing 225mm foul sewer in the R135 to the east of the development site.

### **3.2 Drawings**

The following drawings are provided in support of the planning application to foul water drainage:-

- Drawing No. 20\_099-CSE-00-XX-DR-C-2210 Proposed Overall Foul Water Drainage Layout
- Drawing No. 20\_099-CSE-00-XX-DR-C-2211 - Proposed Foul Water Drainage Sheet 1
- Drawing No. 20\_099-CSE-00-XX-DR-C-2212 - Proposed Foul Water Drainage Sheet 2
- Drawing No. 20\_099-CSE-00-XX-DR-C-2910 Standard Trench Details
- Drawing No. 20\_099-CSE-00-XX-DR-C-2911 Proposed Drainage Details Sheet 1
- Drawing No. 20\_099-CSE-00-XX-DR-C-2911 Proposed Drainage Details Sheet 2
- Drawing No. 20\_099-CSE-00-XX-DR-C-2911 Proposed Drainage Details Sheet 3

### **3.3 Existing Infrastructure**

An existing 225mm foul sewer located in the R135 Regional Road to the east of the site which has capacity to serve the development as noted in the Irish Water CoF referenced in Section 3.1 above.

### **3.4 Proposed Foul Water Drainage Network**

#### **3.4.1 Overview**

The proposed foul water drainage network collects domestic foul water flows from the administration block of the proposed Data Storage Facilities and the adjacent GIS substation. A gravity sewer will flow in an easterly direction where it will discharge to a proposed pumping station. It will be necessary to pump foul flows to a discharge manhole at the site boundary which will outfall by gravity to the existing 225mm sewer in the R135.

### 3.4.2 Foul Water Demand

Foul demand for the proposed development is a combination of domestic demand (admin area etc.) and industrial demand has been estimated as follows.

#### Domestic Demand

- Population (max) ( $P_E$ ) = 256
- Consumption ( $G_E$ ) = 50 litres per head per day (office/ Factory with Canteen) as per Appendix C of the Irish Water Code of Practice for Wastewater Infrastructure (IW-CDS-5030-03).
- Daily Demand ( $P_E G_E$ ) = 12,800 litres or  $12.8\text{m}^3$
- Infiltration ( $I$ ) = 10% of  $P_E G_E$  =  $1.28\text{m}^3$

#### Industrial Demand

We estimate that the peak discharge from the process systems will be approximately 19l/s with the site at full load. The process discharge will only occur during the extreme warm ambient days and as an estimate based on historical weather data for Dublin, the annual discharge will be approximately 24 hours per annum. However, this maybe more if re-entrainment of warm air occurs on the site, which could necessitate the requirement for additional evaporative cooling during the extreme warm ambient days. We are currently evaluating this through Computational Fluid Dynamic (CFD) simulations.

As part of the design intent, the peak discharge of circa 19l/s will be collected underground and retreated for re-use in the cooling process. We estimate that approximately 25-30% of this peak discharge (i.e. 19 l/s) will be of no use for the cooling process and will be discharged to waste drain. This flow corresponds to 4.75 l/s -5.70 l/s.

#### Dry Weather Flow

Dry Weather Flow ( $PG+I+E$ ) from the proposed development is calculated as follows:-

- Typical working day = 8.00-17.00 (9 hours)
- Dry Weather Flow (Domestic) =  $(12.8+1.28)*1000 / 9*60*60 = 0.43 \text{ litres/sec}$
- Dry Weather Flow (Industrial) =  $35.5*1000 / 24*60*60 = 0.41 \text{ litres/sec}$

### 3.4.3 Foul Water Pipe Design

The network has been designed to ensure that the foul discharge maintains a self-cleansing velocity. The proposed network adheres to the minimum pipe gradients set out in Table 6 of the "Building Regulations Technical Guidance Document H". It is proposed to take all foul drainage from the buildings by means of 100mm pipes with minimum gradients of 1:60 which connect to 150mm pipes laid at minimum gradients of 1:100. The key design parameters are summarised as follows:-

- Minimum Self-Cleansing Velocity for Gravity Sewer = 0.75 m/s;

- Minimum gradient of gravity sewer = 1:100
- Roughness Co-efficient for Gravity Sewer ( $k_s$ ) = 1.5mm
- Design Flow = as per Appendix B of the Irish Water Code of Practice for Wastewater Infrastructure (IW-CDS-5030-03).

### Calculation of Design Flow

Design Flow has been calculated based on the requirements of Appendix B of the Irish Water Code of Practice for Wastewater Infrastructure (IW-CDS-5030-03). The parameters are outlined as follows:-

- Design Flow = Design Foul Flow + Surface Water Allowance (Commercial/Industrial) ( $SW_E$ ) where
- Design Foul Flow =  $P_{EGE} \times P_{f_{dom\ ind}} + I + E \times P_{f_{trade}}$  where
  - $P_{EGE} = 12.8\text{m}^3$  or 0.4 litres/sec (9 hour day)
  - $I = 10\%$  of  $P_{EGE} = 1.28\text{m}^3$  or 0.04 litres/sec
  - $E = 35.5\text{m}^3$  or 0.41 litres/sec (24 hour day)
  - $P_{f_{dom\ ind}} = 4.5$
  - $P_{f_{trade}} = 3.0$
- $SW_E$  = Surface Water Allowance =  $Q = 2.78CiA$  (as per Appendix B of the Irish Water Code of Practice for Wastewater Infrastructure (IW-CDS-5030-03) Section 2.2.10.2.2) where
  - Runoff Co-Efficient ( $C$ ) = 1.0
  - Rainfall Intensity ( $I$ ) = 50mm/hour
  - Area ( $A$ ) = 0.025 hectares (Estimate Misconnection of surface water is envisaged to be low as this is a new development).

Based on the above the design flow from the proposed development is as follows

Design Flow  $\Rightarrow (0.4 \times 4.5) + 0.04 + (0.41 \times 3.0) + 2.78 (1.0 \times 50 \times 0.025) \Rightarrow$  **6.5 litres/sec.**

Foul sewer network calculations are outlined in Appendix G.

### 3.4.4 Foul Water Pumping Station

As noted in Section 3.3 and 3.4.1 a foul water pumping station will be required to serve the development due to site topography and the level of the existing 225mm foul sewer. The design will comply with the requirements of Part 5 of the Irish Water Code of Practice for Wastewater Infrastructure (IW-CDS-5030-03). The key design parameters are outlined below:-

- Storage Volume (24 hours) =  $20\text{m}^3$  provided ( $12.8\text{m}^3$  required)
- Flow Rate ( $Q$ ) = 3.76 litres/sec (Flow required to achieve velocity of 0.75 m/s in 80mm - This is a higher flow than 6 x DWF (Domestic) ( $6 \times 0.43$  litres/sec = 2.58 litres/sec).
- Rising Main Diameter = 80mm
- Rising Main Length = 186m
- Rising Main Volume =  $0.93\text{m}^3$
- No. of times Rising Main empties per day = 1
- Mean Rising Main Velocity = 0.75 m/sec
- Roughness Value ( $K_s$ ) = 0.15mm
- Static Head = 3.891m
- Friction Head Loss (FHL) (Estimate based on Colebrook-White) = 1.77m
- Fitting (Estimate) = 0.177m (10% of FHL)
- Total Estimated Design Head = 5.838m approx. (Subject to Detailed Design).

### 3.4.5 Proposed Substation

It is proposed to provide a sleeve to facilitate a rising main connection from the proposed sub-station development (subject to a separate planning application).

### 3.4.6 Internal Cooling Water Drainage (CWD)

In addition to the domestic foul sewer an additional Cooling Water Drainage (CWD) drainage network is required. This sewer will collect discharge from the AHU units and flows in a northerly direction towards a site pumping station which will pump CWD flows to the Water Treatment Plant where it will be treated and re-used. Typically discharge to the CWD drainage will be approximately 17 litres/sec. CWD Network calculations are provided in Appendix G. The CWD pumping station has been designed based on the following criteria.

- Storage Volume = 20 m<sup>3</sup>
- Flow Rate (Q) = 5.89 litres/sec (Flow required to achieve velocity of 0.75 m/s in 100mm )
- Rising Main Diameter = 100mm
- Rising Main Length = 255m
- Rising Main Volume = 2.0m<sup>3</sup>
- No. of times Rising Main empties per day = 1
- Mean Rising Main Velocity = 0.75 m/sec
- Roughness Value (Ks) = 0.15mm
- Static Head = 6m
- Friction Head Loss (FHL) (Estimate based on Colebrook-White) = 1.78m
- Fitting (Estimate) = 0.178m (10% of FHL)
- Total Estimated Design Head = 7.96m approx. (Subject to Detailed Design).

## 3.5 Foul Drainage Design Summary

The proposed foul water drainage network has been designed in accordance with the requirements of Appendix B of the Irish Water Code of Practice for Wastewater Infrastructure (IW-CDS-5030-03). The domestic foul sewer flows in a easterly direction towards a proposed pumping station which pumps to a discharge manhole adjacent to the existing Irish Water 225mm foul sewer in the R135 road to the east of the site. The proposed CWD drainage drains by gravity to a pumping station located to the northeast of Building B where it will be pumped to the Water Treatment Plant. Foul discharge from the Water Treatment Plant Building will discharge by gravity to the Irish Water Network. Irish Water have provided a Confirmation of Feasibility for the proposed water supply connection (Ref CDS 200004468).

## **4 Water Supply**

### **4.1 General**

A pre-connection enquiry (PCE) form was submitted to Irish Water on 26<sup>th</sup> July 2020 which addressed water and wastewater demand for the development. The reference number for the Pre-Connection Enquiry is CDS 200004468. Irish Water subsequently provided a Confirmation of Feasibility (CoF) on 31<sup>st</sup> March 2021 (refer to Appendix F for details) which indicated that it is feasible to provide supply to the site subject to upgrades. The upgrade works involve the replacement of approx. 1500m of new 450mm pipe main to replace the existing 6" uPVC main in the R135 and the upgrade of pumps at Ballycoolen Highlands Tower. The CoF notes that the developer is to fund a portion of the upgrade works.

### **4.2 Drawings**

The following drawings are provided in support of the planning application to water supply:-

- Drawing No. 20\_099-CSE-00-XX-DR-C-2310 Proposed Overall Water Supply Layout Plan
- Drawing No. 20\_099-CSE-00-XX-DR-C-2311- Proposed Water Supply Layout Plan Sheet 1
- Drawing No. 20\_099-CSE-00-XX-DR-C-2312- Proposed Water Supply Layout Plan Sheet 2
- Drawing No. 20\_099-CSE-00-XX-DR-C-2910 Standard Trench Details

### **4.3 Existing Infrastructure**

There is an existing 150mm water main located in the R1135. Irish Water are proposing updates to the network which will serve the development. As noted in Section 4.1 this watermain is to be upgraded with a new 450mm watermain.

### **4.4 Proposed Water Supply**

It is proposed to connect a 200mm watermain to this upgraded 450mm pipe in the R135.

It is proposed to provide connections from the 200mm incoming water supply main to the admin area of the data centre buildings, the water treatment plant room, the two no sprinkler storage tanks and to the adjacent GIS Substation (being designed by others).

#### **4.4.1 Domestic Water Demand**

Domestic water supply demand for the proposed development has been estimated as follows (As per Section 3.7.2 of the Irish Water Code of Practice (IW-CDS-5020-03) .



- Population = 256
- Consumption = 45 litres per person per day
- Daily Demand = 11,520 litres per day
- Average Flow = 0.13 litres/sec
- Average Day/Peak Week Demand =  $1.25 \times 0.13 = 0.17$  litres/sec
- Peak Demand =  $5.0 \times 0.17$  litres/sec = 0.85 litres/sec

#### 4.4.2 Process Water Demand

We estimate that the peak process water demand will be approximately 56l/s with the site at full load. This estimate excludes periodic flushing and washdown. The peak process water demand will only occur during the extreme warm ambient days and as an estimate based on historical weather data for Dublin, this should be approximately 24 hours per annum. However, this maybe more if re-entrainment of warm air occurs on the site, which could necessitate the requirement for additional evaporative cooling during the extreme warm ambient days. We are currently evaluating this through Computational Fluid Dynamic (CFD) simulations.

On-site storage will be provided as part of the development. Water storage (2590m<sup>3</sup>) will be provided for the evaporative cooling hours required in the worst case summer 48 hour period. The water fill from the Irish Water main can be adjusted to fill the system over this time period.

Process water supply demand for the proposed development has been estimated in the Table below.

| DUB DC       | Water Requirement (m <sup>3</sup> /year) | Cumulative (m <sup>3</sup> /year) | Projected Timeframe |
|--------------|--|-----------------------------------|---------------------|
| COLO 1       | 346                                      | -                                 | July 2023           |
| COLO 2       | 346                                      | 691.2                             | October 2023        |
| COLO 3       | 346                                      | 1037.2                            | December 2023       |
| COLO 4       | 346                                      | 1383.3                            | February 2024       |
| COLO 5       | 346                                      | 1729.2                            | April 2024          |
| COLO 6       | 346                                      | 2075.2                            | July 2024           |
| COLO 7       | 346                                      | 2421.2                            | September 2024      |
| Building A   | 2,421.2                                  |                                   | December 2024       |
| Building B   | 2,421.2                                  |                                   | January 2025        |
| <b>Total</b> |  | <b>4,842.4</b>                    |                     |

**Table 4.1 – Proposed Water Demand Estimate**

#### **4.5 Fire Hydrant Main**

The proposed development will be served by a 250mm fire hydrant main which is connected to two proposed sprinkler tanks (Each tank has a capacity of 670m<sup>3</sup>) and associated pump houses. The fire hydrants will be provided at appropriate locations in accordance with the specialist fire protection contractors design and Fingal County Council requirements.

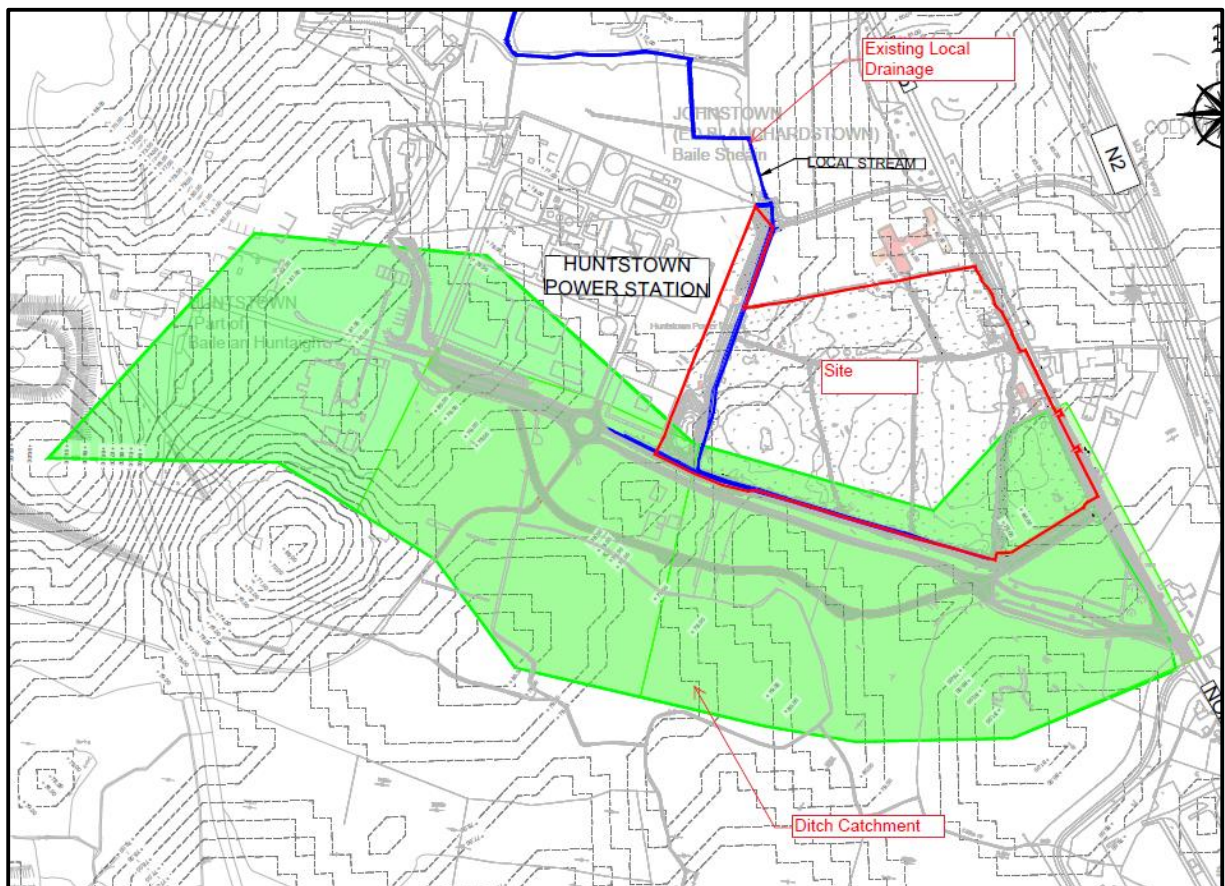
#### **4.6 Water Supply Summary**

The proposed Water Supply Network will comprise of a 200mm which will be connected to the Irish Water supply network in the R135 which is to be upgraded to 400mm . The water main will serve the proposed buildings, water treatment plant, sprinkler tanks and proposed substation. A separate fire hydrant main will be provided to serve the fire hydrants which will be feed from the sprinkler tanks. Irish Water have provided a Confirmation of Feasibility for the proposed water supply connection (Ref CDS 200004468).

## 5 Ditch Diversion

### 5.1 Catchment Study

As noted in section the proposed development site is traversed by an existing ditch which forms the Huntstown Stream. In order to facilitate the development of the site it is necessary to remove a section of the ditch and replace with a new 900mm pipe (minimum size required by OPW Guidelines for the Construction, Replacement or Alteration of Bridges and Culverts (OPW Guidelines)) which will traverse the western section of the site. The catchment area draining to the ditch is estimated using contour mapping to be 0.4 km<sup>2</sup> (see Fig 5.1 below catchment highlighted in green).



**Table 5.1 – Catchment Mapping**

The catchment area is determined to be 30.77 Hectares (highlighted in green) and the percentage impermeable area (highlighted grey on attached map is estimated to be 10%.

The catchment map is included in Appendix H of this report.

## **5.2 Ditch Diversion Design Parameters**

The proposed ditch diversion is required to take account of the requirements of OPW Guidelines for the Construction, Replacement or Alteration of Bridges and Culverts (OPW Guidelines)) which are outline below:-

- Diversion pipe to be capable of passing a fluvial flood flow with a 1% annual exceedance probability (AEP) or 1 in 100 year flow without significantly changing the hydraulic characteristics of the watercourse;
- Diversion pipe to maintain a freeboard of 300mm;
- Diversion pipe capable of operating under the above design conditions without causing a hydraulic loss of no more than 300mm;
- Diameter must not be less than 900mm;
- All calculations have allowed for an additional allowance of 10% in rainfall intensities to allow for climate change as per Table 6.1 of Volume 2 of the GDSDS.

## **5.3 Calculations**

The proposed ditch diversion has been simulated using Civil 3D and WinDes™ software. Calculations are provided in Appendix I of this report.

## **5.4 Drawings**

The following drawings are provided in support of the planning application for the ditch diversion.

- Drawing No. 20\_099-CSE-00-XX-DR-C-2117 Ditch Diversion Layout Plan and Longitudinal Sections.

## **5.5 Design Summary**

The proposed ditch diversion has been designed as a 900mm at gradient of 1:479. The pre-development water level upstream of the ditch diversion has been assessed at the start of the proposed diversion works at Nodes ST 1 and ST2 indicated on Drawing No. 20\_099-CSE-00-XX-DR-C-2117. The water Levels are outlined in Table 5.1 overleaf:-

| <b>Node</b> | <b>Pre-Development Water Level (mOD)</b> | <b>Post-Development Water Level (mOD)</b> | <b>Difference (m)</b> |
|-------------|--|---|-----------------------|
| <b>ST 1</b> | 76.794                                   | 76.888                                    | +0.094                |
| <b>ST 2</b> | 77.277                                   | 77.154                                    | -0.123                |

**Table 5.1 – Pre and Post Development Water Levels**


As noted above there is an increase in water level of 0.094m or 94mm at ST 1 to the west of the diversion and a decrease 0.123m or 123mm at ST 2 to the east of the diversion. The minimum freeboard is 307mm. The above information is outlined in the Windes calculations included in Appendix I.

The proposed ditch diversion complies with the OPW Guidelines in terms of capable to pass the required return period of the 1 in 100 year event. A minimum freeboard of 307mm has been provided, in excess of the 300mm required by the OPW Guidelines and hydraulic loss across the diversion route are calculated to be below the 300mm allowed by the OPW Guidelines.

## **5.6 Environmental Summary**

The existing onsite drainage ditches have been assessed by the project ecologist and hydrologist in respect of the applicability of the Objective WQ05 within the Fingal County Development Plan 2017-2023. Objective WQ05 requires the establishment of a riparian corridors free from new development along all significant watercourses and streams in the County. Chapter 7 (Hydrology) of the EIAR notes that these are existing manmade ditches with intermittent or ephemeral characteristics are not considered to be a significant watercourse or stream, therefore Objective WQ05 is not considered to apply to any of the local drainage ditches on the site. Furthermore, Chapter 8 (Biodiversity) of the EIAR has assessed these onsite ditches for ecological value and concluded that due to their ephemeral nature have and they have no fisheries value and are also unfavourable for amphibians.

## **Appendix A – Surface Water Drainage Calculations**

|  |  |   |
|--|--|---|
| Clifton Scannell Emerson Associates                                |  | Page 1  |
| Seefort Lodge<br>Castledawson Avenue, Blackrock<br>Dublin, Ireland | Project:<br>Huntstown data centre facility |  |
| Date 06/05/2021<br>File DUB041 SW Network-1.mdx                    | Designed by ZS<br>Checked by CD            |   |
| Innovyze   | Network 2020.1.3                           |   |

### STORM SEWER DESIGN by the Modified Rational Method

#### Design Criteria for Network 1

Pipe Sizes STANDARD Manhole Sizes STANDARD

FSR Rainfall Model - Scotland and Ireland

|                                      |        |                                       |       |
|--------------------------------------|--------|---------------------------------------|-------|
| Return Period (years)                | 25     | PIMP (%)                              | 100   |
| M5-60 (mm)                           | 16.500 | Add Flow / Climate Change (%)         | 0     |
| Ratio R                              | 0.300  | Minimum Backdrop Height (m)           | 0.200 |
| Maximum Rainfall (mm/hr)             | 50     | Maximum Backdrop Height (m)           | 1.500 |
| Maximum Time of Concentration (mins) | 30     | Min Design Depth for Optimisation (m) | 1.200 |
| Foul Sewage (l/s/ha)                 | 0.000  | Min Vel for Auto Design only (m/s)    | 1.00  |
| Volumetric Runoff Coeff.             | 0.750  | Min Slope for Optimisation (1:X)      | 500   |

Designed with Level Soffits

#### Time Area Diagram for Network 1






| Time<br>(mins) | Area<br>(ha) | Time<br>(mins) | Area<br>(ha) | Time<br>(mins) | Area<br>(ha) | Time<br>(mins) | Area<br>(ha) | Time<br>(mins) | Area<br>(ha) |
|----------------|--------------|----------------|--------------|----------------|--------------|----------------|--------------|----------------|--------------|
| 0-4            | 0.010        | 4-8            | 1.163        | 8-12           | 1.588        | 12-16          | 0.255        | 16-20          | 0.003        |

Total Area Contributing (ha) = 3.019

Total Pipe Volume (m³) = 147.103

#### Network Design Table for Network 1

« - Indicates pipe capacity < flow

| PN    | Length<br>(m) | Fall<br>(m) | Slope<br>(1:X) | I.Area<br>(ha) | T.E.<br>(mins) | Base<br>Flow (l/s) | k<br>(mm) | HYD<br>SECT | DIA<br>(mm) | Section Type | Auto<br>Design  |
|-------|---------------|-------------|----------------|----------------|----------------|--------------------|-----------|-------------|-------------|--------------|---|
| 1.000 | 16.964        | 0.085       | 199.6          | 0.017          | 5.00           | 0.0                | 0.600     | o           | 225         | Pipe/Conduit |  |
| 1.001 | 13.677        | 0.068       | 201.1          | 0.024          | 0.00           | 0.0                | 0.600     | o           | 225         | Pipe/Conduit |  |
| 1.002 | 46.642        | 0.155       | 300.9          | 0.017          | 0.00           | 0.0                | 0.600     | o           | 300         | Pipe/Conduit |  |
| 1.003 | 12.681        | 0.042       | 301.9          | 0.100          | 0.00           | 0.0                | 0.600     | o           | 300         | Pipe/Conduit |  |
| 1.004 | 40.946        | 0.136       | 301.1          | 0.024          | 0.00           | 0.0                | 0.600     | o           | 300         | Pipe/Conduit |  |

#### Network Results Table

| PN    | Rain<br>(mm/hr) | T.C.<br>(mins) | US/IL<br>(m) | E I.Area<br>(ha) | E Base<br>Flow (l/s) | Foul<br>(l/s) | Add Flow<br>(l/s) | Vel<br>(m/s) | Cap<br>(l/s) | Flow<br>(l/s) |
|-------|-----------------|----------------|--------------|------------------|----------------------|---------------|-------------------|--------------|--------------|---------------|
| 1.000 | 50.00           | 5.31           | 78.624       | 0.017            | 0.0                  | 0.0           | 0.0               | 0.92         | 36.7         | 2.3           |
| 1.001 | 50.00           | 5.55           | 78.539       | 0.041            | 0.0                  | 0.0           | 0.0               | 0.92         | 36.5         | 5.6           |
| 1.002 | 50.00           | 6.42           | 78.396       | 0.058            | 0.0                  | 0.0           | 0.0               | 0.90         | 63.7         | 7.8           |
| 1.003 | 50.00           | 6.65           | 78.241       | 0.158            | 0.0                  | 0.0           | 0.0               | 0.90         | 63.6         | 21.4          |
| 1.004 | 50.00           | 7.41           | 78.199       | 0.181            | 0.0                  | 0.0           | 0.0               | 0.90         | 63.7         | 24.6          |

Clifton Scannell Emerson Associates

Page 2

Seefort Lodge  
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Project:  
Huntstown data centre facility

Designed by ZS  
Checked by CD

Network 2020.1.3

Micro Drainage

Network Design Table for Network 1

| PN    | Length<br>(m) | Fall<br>(m) | Slope<br>(1:X) | I.Area<br>(ha) | T.E.<br>(mins) | Base<br>Flow (l/s) | k<br>(mm) | HYD<br>SECT | DIA<br>(mm) | Section Type | Auto<br>Design  |
|-------|---------------|-------------|----------------|----------------|----------------|--------------------|-----------|-------------|-------------|--------------|---|
| 2.000 | 21.396        | 0.107       | 200.0          | 0.030          | 5.00           | 0.0                | 0.600     | o           | 225         | Pipe/Conduit |    |
| 1.005 | 40.880        | 0.102       | 400.8          | 0.047          | 0.00           | 0.0                | 0.600     | o           | 450         | Pipe/Conduit |    |
| 1.006 | 20.017        | 0.050       | 400.3          | 0.101          | 0.00           | 0.0                | 0.600     | o           | 450         | Pipe/Conduit |    |
| 1.007 | 33.574        | 0.084       | 399.7          | 0.071          | 0.00           | 0.0                | 0.600     | o           | 450         | Pipe/Conduit |    |
| 1.008 | 52.436        | 0.131       | 400.3          | 0.222          | 0.00           | 0.0                | 0.600     | o           | 450         | Pipe/Conduit |    |
| 3.000 | 37.955        | 0.190       | 199.8          | 0.147          | 5.00           | 0.0                | 0.600     | o           | 225         | Pipe/Conduit |    |
| 1.009 | 64.358        | 0.161       | 399.7          | 0.240          | 0.00           | 0.0                | 0.600     | o           | 450         | Pipe/Conduit |    |
| 1.010 | 40.080        | 0.100       | 400.8          | 0.130          | 0.00           | 0.0                | 0.600     | o           | 450         | Pipe/Conduit |    |
| 1.011 | 24.280        | 0.049       | 495.5          | 0.257          | 0.00           | 0.0                | 0.600     | o           | 600         | Pipe/Conduit |   |
| 1.012 | 29.641        | 0.059       | 502.4          | 0.000          | 0.00           | 0.0                | 0.600     | o           | 600         | Pipe/Conduit |  |
| 1.013 | 65.828        | 0.132       | 498.7          | 0.157          | 0.00           | 0.0                | 0.600     | o           | 600         | Pipe/Conduit |  |
| 4.000 | 60.127        | 0.200       | 300.6          | 0.057          | 5.00           | 0.0                | 0.600     | o           | 300         | Pipe/Conduit |  |
| 1.014 | 13.518        | 0.027       | 500.7          | 0.099          | 0.00           | 0.0                | 0.600     | o           | 600         | Pipe/Conduit |  |
| 5.000 | 40.474        | 0.135       | 299.8          | 0.115          | 5.00           | 0.0                | 0.600     | o           | 300         | Pipe/Conduit |  |
| 5.001 | 43.937        | 0.146       | 300.9          | 0.131          | 0.00           | 0.0                | 0.600     | o           | 300         | Pipe/Conduit |  |

Network Results Table


| PN    | Rain<br>(mm/hr) | T.C.<br>(mins) | US/IL<br>(m) | Σ I.Area<br>(ha) | Σ Base<br>Flow (l/s) | Foul<br>(l/s) | Add Flow<br>(l/s) | Vel<br>(m/s) | Cap<br>(l/s) | Flow<br>(l/s) |
|-------|-----------------|----------------|--------------|------------------|----------------------|---------------|-------------------|--------------|--------------|---------------|
| 2.000 | 50.00           | 5.39           | 78.248       | 0.030            | 0.0                  | 0.0           | 0.0               | 0.92         | 36.6         | 4.1           |
| 1.005 | 50.00           | 8.09           | 77.913       | 0.259            | 0.0                  | 0.0           | 0.0               | 1.01         | 160.5        | 35.1          |
| 1.006 | 50.00           | 8.42           | 77.811       | 0.360            | 0.0                  | 0.0           | 0.0               | 1.01         | 160.6        | 48.7          |
| 1.007 | 50.00           | 8.97           | 77.761       | 0.431            | 0.0                  | 0.0           | 0.0               | 1.01         | 160.7        | 58.4          |
| 1.008 | 50.00           | 9.83           | 77.677       | 0.653            | 0.0                  | 0.0           | 0.0               | 1.01         | 160.6        | 88.4          |
| 3.000 | 50.00           | 5.69           | 77.959       | 0.147            | 0.0                  | 0.0           | 0.0               | 0.92         | 36.6         | 19.9          |
| 1.009 | 50.00           | 10.90          | 77.544       | 1.040            | 0.0                  | 0.0           | 0.0               | 1.01         | 160.7        | 140.8         |
| 1.010 | 50.00           | 11.56          | 77.383       | 1.170            | 0.0                  | 0.0           | 0.0               | 1.01         | 160.5        | 158.4         |
| 1.011 | 50.00           | 11.93          | 77.133       | 1.427            | 0.0                  | 0.0           | 0.0               | 1.09         | 307.4        | 193.2         |
| 1.012 | 50.00           | 12.39          | 77.084       | 1.427            | 0.0                  | 0.0           | 0.0               | 1.08         | 305.2        | 193.2         |
| 1.013 | 50.00           | 13.40          | 77.025       | 1.584            | 0.0                  | 0.0           | 0.0               | 1.08         | 306.4        | 214.5         |
| 4.000 | 50.00           | 6.11           | 77.381       | 0.057            | 0.0                  | 0.0           | 0.0               | 0.90         | 63.7         | 7.8           |
| 1.014 | 50.00           | 13.61          | 76.781       | 1.741            | 0.0                  | 0.0           | 0.0               | 1.08         | 305.8        | 235.7         |
| 5.000 | 50.00           | 5.75           | 78.366       | 0.115            | 0.0                  | 0.0           | 0.0               | 0.90         | 63.8         | 15.5          |
| 5.001 | 50.00           | 6.56           | 78.231       | 0.246            | 0.0                  | 0.0           | 0.0               | 0.90         | 63.7         | 33.3          |

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|                                |
|--------------------------------|
| Project:                       |
| Huntstown data centre facility |



Micro  
Drainage

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Network 2020.1.3

Network Design Table for Network 1

| PN    | Length<br>(m) | Fall<br>(m) | Slope<br>(1:X) | I.Area<br>(ha) | T.E.<br>(mins) | Base<br>Flow (l/s) | k<br>(mm) | HYD<br>SECT | DIA<br>(mm) | Section Type | Auto<br>Design  |
|-------|---------------|-------------|----------------|----------------|----------------|--------------------|-----------|-------------|-------------|--------------|---|
| 5.002 | 50.000        | 0.167       | 299.4          | 0.145          | 0.00           | 0.0                | 0.600     | o           | 300         | Pipe/Conduit |  |
| 5.003 | 33.783        | 0.113       | 299.0          | 0.169          | 0.00           | 0.0                | 0.600     | o           | 375         | Pipe/Conduit |  |
| 6.000 | 40.474        | 0.135       | 299.8          | 0.115          | 5.00           | 0.0                | 0.600     | o           | 300         | Pipe/Conduit |  |
| 6.001 | 43.937        | 0.146       | 300.9          | 0.131          | 0.00           | 0.0                | 0.600     | o           | 300         | Pipe/Conduit |  |
| 6.002 | 50.000        | 0.167       | 299.4          | 0.145          | 0.00           | 0.0                | 0.600     | o           | 300         | Pipe/Conduit |  |
| 6.003 | 33.783        | 0.113       | 299.0          | 0.169          | 0.00           | 0.0                | 0.600     | o           | 375         | Pipe/Conduit |  |
| 6.004 | 70.309        | 0.234       | 300.5          | 0.080          | 0.00           | 0.0                | 0.600     | o           | 375         | Pipe/Conduit |  |
| 5.004 | 36.054        | 0.120       | 300.5          | 0.080          | 0.00           | 0.0                | 0.600     | o           | 375         | Pipe/Conduit |  |
| 1.015 | 93.160        | 0.466       | 199.9          | 0.000          | 0.00           | 0.0                | 0.600     | o           | 300         | Pipe/Conduit |  |
| 1.016 | 63.465        | 0.317       | 200.2          | 0.000          | 0.00           | 0.0                | 0.600     | o           | 300         | Pipe/Conduit |  |
| 1.017 | 69.205        | 0.384       | 180.2          | 0.000          | 0.00           | 0.0                | 0.600     | o           | 300         | Pipe/Conduit |  |
| 1.018 | 5.054         | 0.033       | 153.2          | 0.000          | 0.00           | 0.0                | 0.600     | o           | 300         | Pipe/Conduit |  |

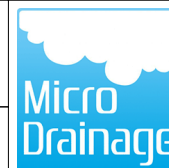
## Network Results Table

| PN    | Rain<br>(mm/hr) | T.C.<br>(mins) | US/IL<br>(m) | Σ I.Area<br>(ha) | Σ Base<br>Flow (l/s) | Foul<br>(l/s) | Add Flow<br>(l/s) | Vel<br>(m/s) | Cap<br>(l/s) | Flow<br>(l/s) |
|-------|-----------------|----------------|--------------|------------------|----------------------|---------------|-------------------|--------------|--------------|---------------|
| 5.002 | 50.00           | 7.48           | 78.085       | 0.390            | 0.0                  | 0.0           | 0.0               | 0.90         | 63.9         | 52.8          |
| 5.003 | 50.00           | 8.02           | 77.843       | 0.559            | 0.0                  | 0.0           | 0.0               | 1.04         | 115.2        | 75.7          |
| 6.000 | 50.00           | 5.75           | 78.268       | 0.115            | 0.0                  | 0.0           | 0.0               | 0.90         | 63.8         | 15.5          |
| 6.001 | 50.00           | 6.56           | 78.133       | 0.245            | 0.0                  | 0.0           | 0.0               | 0.90         | 63.7         | 33.2          |
| 6.002 | 50.00           | 7.48           | 77.987       | 0.390            | 0.0                  | 0.0           | 0.0               | 0.90         | 63.9         | 52.9          |
| 6.003 | 50.00           | 8.02           | 77.745       | 0.559            | 0.0                  | 0.0           | 0.0               | 1.04         | 115.2        | 75.7          |
| 6.004 | 50.00           | 9.15           | 77.632       | 0.639            | 0.0                  | 0.0           | 0.0               | 1.04         | 114.9        | 86.5          |
| 5.004 | 50.00           | 9.73           | 77.398       | 1.278            | 0.0                  | 0.0           | 0.0               | 1.04         | 114.9«       | 173.0         |
| 1.015 | 50.00           | 15.01          | 76.750       | 3.019            | 0.0                  | 0.0           | 0.0               | 1.11         | 78.3«        | 408.8         |
| 1.016 | 50.00           | 15.96          | 76.284       | 3.019            | 0.0                  | 0.0           | 0.0               | 1.11         | 78.3«        | 408.8         |
| 1.017 | 50.00           | 16.95          | 75.967       | 3.019            | 0.0                  | 0.0           | 0.0               | 1.17         | 82.6«        | 408.8         |
| 1.018 | 50.00           | 17.02          | 75.583       | 3.019            | 0.0                  | 0.0           | 0.0               | 1.27         | 89.6«        | 408.8         |

| Clifton Scannell Emerson Associates                                |           |              |               |  |       |                           |                        | Page 4  |                           |                        |               |
|--|-----------|--------------|---------------|--|-------|---------------------------|------------------------|---|---------------------------|------------------------|---------------|
| Seefort Lodge<br>Castledawson Avenue, Blackrock<br>Dublin, Ireland |           |              |               | Project:<br>Huntstown data centre facility |       |                           |                        |  |                           |                        |               |
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| Innovyze   |           |              |               |  |       |                           |                        | Network 2020.1.3  |                           |                        |               |
| <u>Manhole Schedules for Network 1</u>                             |           |              |               |  |       |                           |                        |   |                           |                        |               |
| MH Name  | MH CL (m) | MH Depth (m) | MH Connection | MH Diam.,L*W (mm)                          | PN    | Pipe Out Invert Level (m) | Pipe Out Diameter (mm) | PN  | Pipes In Invert Level (m) | Pipes In Diameter (mm) | Backdrop (mm) |
| S 1.0  | 80.043    | 1.419        | Open Manhole  | 1200                                       | 1.000 | 78.624                    | 225                    |   |                           |                        |               |
| S 1.1  | 79.974    | 1.435        | Open Manhole  | 1200                                       | 1.001 | 78.539                    | 225                    | 1.000   | 78.539                    | 225                    |               |
| S 1.2  | 79.910    | 1.514        | Open Manhole  | 1350                                       | 1.002 | 78.396                    | 300                    | 1.001   | 78.471                    | 225                    |               |
| S 1.3  | 79.712    | 1.471        | Open Manhole  | 1350                                       | 1.003 | 78.241                    | 300                    | 1.002   | 78.241                    | 300                    |               |
| S 1.4  | 79.672    | 1.473        | Open Manhole  | 1350                                       | 1.004 | 78.199                    | 300                    | 1.003   | 78.199                    | 300                    |               |
| S 2.0  | 79.663    | 1.415        | Open Manhole  | 1200                                       | 2.000 | 78.248                    | 225                    |   |                           |                        |               |
| S 1.5  | 79.433    | 1.520        | Open Manhole  | 1200                                       | 1.005 | 77.913                    | 450                    | 1.004   | 78.063                    | 300                    |               |
|  |           |              |               |  |       |                           |                        | 2.000   | 78.141                    | 225                    | 3             |
| S 1.6  | 79.108    | 1.297        | Open Manhole  | 1500                                       | 1.006 | 77.811                    | 450                    | 1.005   | 77.811                    | 450                    |               |
| S 1.7  | 79.068    | 1.307        | Open Manhole  | 1500                                       | 1.007 | 77.761                    | 450                    | 1.006   | 77.761                    | 450                    |               |
| S 1.8  | 79.138    | 1.461        | Open Manhole  | 1500                                       | 1.008 | 77.677                    | 450                    | 1.007   | 77.677                    | 450                    |               |
| S 3.0  | 79.452    | 1.493        | Open Manhole  | 1200                                       | 3.000 | 77.959                    | 225                    |   |                           |                        |               |
| S 1.9  | 79.128    | 1.584        | Open Manhole  | 1350                                       | 1.009 | 77.544                    | 450                    | 1.008   | 77.546                    | 450                    | 2             |
|  |           |              |               |  |       |                           |                        | 3.000   | 77.769                    | 225                    |               |
| S 1.10   | 79.207    | 1.824        | Open Manhole  | 1650                                       | 1.010 | 77.383                    | 450                    | 1.009   | 77.383                    | 450                    |               |
| S 1.11   | 79.207    | 2.074        | Open Manhole  | 1650                                       | 1.011 | 77.133                    | 600                    | 1.010   | 77.283                    | 450                    |               |
| S 1.12   | 79.330    | 2.246        | Open Manhole  | 1500                                       | 1.012 | 77.084                    | 600                    | 1.011   | 77.084                    | 600                    |               |
| S 1.13   | 79.330    | 2.305        | Open Manhole  | 1650                                       | 1.013 | 77.025                    | 600                    | 1.012   | 77.025                    | 600                    |               |
| S 4.0  | 79.000    | 1.619        | Open Manhole  | 1200                                       | 4.000 | 77.381                    | 300                    |   |                           |                        |               |
| S 1.14   | 79.818    | 3.037        | Open Manhole  | 1950                                       | 1.014 | 76.781                    | 600                    | 1.013   | 76.893                    | 600                    | 112           |
|  |           |              |               |  |       |                           |                        | 4.000   | 77.181                    | 300                    | 100           |
| S 5.0  | 79.867    | 1.501        | Open Manhole  | 1200                                       | 5.000 | 78.366                    | 300                    |   |                           |                        |               |
| S 5.1  | 79.857    | 1.626        | Open Manhole  | 1200                                       | 5.001 | 78.231                    | 300                    | 5.000   | 78.231                    | 300                    |               |
| S 5.2  | 79.845    | 1.760        | Open Manhole  | 1350                                       | 5.002 | 78.085                    | 300                    | 5.001   | 78.085                    | 300                    |               |
| S 5.3  | 79.831    | 1.988        | Open Manhole  | 1350                                       | 5.003 | 77.843                    | 375                    | 5.002   | 77.918                    | 300                    |               |
| S 6.0  | 79.823    | 1.555        | Open Manhole  | 1200                                       | 6.000 | 78.268                    | 300                    |   |                           |                        |               |
| S 6.1  | 79.824    | 1.691        | Open Manhole  | 1200                                       | 6.001 | 78.133                    | 300                    | 6.000   | 78.133                    | 300                    |               |
| S 6.2  | 79.824    | 1.837        | Open Manhole  | 1350                                       | 6.002 | 77.987                    | 300                    | 6.001   | 77.987                    | 300                    |               |
| S 6.3  | 79.823    | 2.078        | Open Manhole  | 1350                                       | 6.003 | 77.745                    | 375                    | 6.002   | 77.820                    | 300                    |               |
| S 6.4  | 79.569    | 1.937        | Open Manhole  | 1350                                       | 6.004 | 77.632                    | 375                    | 6.003   | 77.632                    | 375                    |               |
| S 5.4  | 79.573    | 2.175        | Open Manhole  | 1500                                       | 5.004 | 77.398                    | 375                    | 5.003   | 77.730                    | 375                    | 332           |
|  |           |              |               |  |       |                           |                        | 6.004   | 77.398                    | 375                    |               |
| S 1.15   | 79.000    | 2.250        | Open Manhole  | 2100                                       | 1.015 | 76.750                    | 300                    | 1.014   | 76.754                    | 600                    | 304           |
|  |           |              |               |  |       |                           |                        | 5.004   | 77.278                    | 375                    | 603           |
| S 1.16   | 78.963    | 2.679        | Open Manhole  | 2100                                       | 1.016 | 76.284                    | 300                    | 1.015   | 76.284                    | 300                    |               |
| S 1.17   | 77.991    | 2.024        | Open Manhole  | 2100                                       | 1.017 | 75.967                    | 300                    | 1.016   | 75.967                    | 300                    |               |
| S 1.18   | 77.551    | 1.968        | Open Manhole  | 2250                                       | 1.018 | 75.583                    | 300                    | 1.017   | 75.583                    | 300                    |               |
| MH80   | 77.451    | 1.901        | Open Manhole  | 1500                                       |       | OUTFALL                   |                        | 1.018   | 75.550                    | 300                    |               |
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| Huntstown data centre facility |



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






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Network 2020.1.3

### Manhole Schedules for Network 1

| MH Name | Manhole Easting (m) | Manhole Northing (m) | Intersection Easting (m) | Intersection Northing (m) | Manhole Access | Layout (North)  |
|---------|---------------------|----------------------|--------------------------|---------------------------|----------------|---|
| S 1.0   | 711876.988          | 741371.323           | 711876.988               | 741371.323                | Required       |    |
| S 1.1   | 711862.418          | 741362.634           | 711862.531               | 741362.548                | Required       |    |
| S 1.2   | 711858.853          | 741349.430           | 711858.957               | 741349.439                | Required       |    |
| S 1.3   | 711879.102          | 741307.413           | 711878.998               | 741307.401                | Required       |   |
| S 1.4   | 711876.368          | 741295.030           | 711876.286               | 741295.095                | Required       |  |
| S 2.0   | 711849.858          | 741258.554           | 711849.858               | 741258.554                | Required       |  |
| S 1.5   | 711839.478          | 741277.263           | 711839.478               | 741277.263                | Required       |  |
| S 1.6   | 711802.647          | 741259.524           | 711802.628               | 741259.628                | Required       |  |
| S 1.7   | 711782.708          | 741261.287           | 711782.785               | 741261.358                | Required       |  |
| S 1.8   | 711782.708          | 741294.861           | 711782.813               | 741294.861                | Required       |  |
| S 3.0   | 711820.658          | 741347.297           | 711820.658               | 741347.297                | Required       |  |
| S 1.9   | 711782.702          | 741347.297           | 711782.702               | 741347.297                | Required       |  |
| S 1.10  | 711782.700          | 741411.655           | 711782.670               | 741411.655                | Required       |  |
| S 1.11  | 711782.701          | 741451.735           | 711782.596               | 741451.735                | Required       |  |
| S 1.12  | 711782.702          | 741476.015           | 711782.522               | 741476.016                | Required       |  |

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Drainage

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Network 2020.1.3


### Manhole Schedules for Network 1

| MH Name | Manhole Easting (m) | Manhole Northing (m) | Intersection Easting (m) | Intersection Northing (m) | Manhole Access | Layout (North) |
|---------|---------------------|----------------------|--------------------------|---------------------------|----------------|----------------|
| S 1.13  | 711782.702          | 741505.657           | 711782.628               | 741505.583                | Required       |                |
| S 4.0   | 711656.747          | 741505.657           | 711656.747               | 741505.657                | Required       |                |
| S 1.14  | 711716.874          | 741505.657           | 711716.874               | 741505.657                | Required       |                |
| S 5.0   | 711682.023          | 741339.449           | 711682.023               | 741339.449                | Required       |                |
| S 5.1   | 711682.023          | 741379.923           | 711682.203               | 741379.923                | Required       |                |
| S 5.2   | 711682.023          | 741423.860           | 711682.128               | 741423.860                | Required       |                |
| S 5.3   | 711682.023          | 741473.860           | 711682.166               | 741473.860                | Required       |                |
| S 6.0   | 711752.332          | 741339.449           | 711752.332               | 741339.449                | Required       |                |
| S 6.1   | 711752.332          | 741379.923           | 711752.512               | 741379.923                | Required       |                |
| S 6.2   | 711752.332          | 741423.860           | 711752.437               | 741423.860                | Required       |                |
| S 6.3   | 711752.332          | 741473.860           | 711752.474               | 741473.860                | Required       |                |
| S 6.4   | 711752.332          | 741507.644           | 711752.231               | 741507.543                | Required       |                |
| S 5.4   | 711682.023          | 741507.644           | 711682.023               | 741507.644                | Required       |                |
| S 1.15  | 711716.189          | 741519.157           | 711716.189               | 741519.157                | Required       |                |
| S 1.16  | 711623.037          | 741520.297           | 711623.037               | 741520.297                | Required       |                |

### Manhole Schedules for Network 1

| MH Name | Manhole Easting (m) | Manhole Northing (m) | Intersection Easting (m) | Intersection Northing (m) | Manhole Access | Layout (North)  |
|---------|---------------------|----------------------|--------------------------|---------------------------|----------------|---|
| S 1.17  | 711559.632          | 741517.531           | 711559.632               | 741517.531                | Required       |  |
| S 1.18  | 711490.437          | 741516.384           | 711490.437               | 741516.384                | Required       |  |
| MH80    | 711487.406          | 741520.429           |                          |                           | No Entry       |   |

| Clifton Scannell Emerson Associates                                |            |             |         |  |             |             |               | Page 8  |      |
|--|------------|-------------|---------|--|-------------|-------------|---------------|---|------|
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| Date 06/05/2021  |            |             |         | Designed by ZS                             |             |             |               |   |      |
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| Innovyze   |            |             |         | Network 2020.1.3                           |             |             |               |   |      |
| <u>PIPELINE SCHEDULES for Network 1</u>                            |            |             |         |  |             |             |               |   |      |
| <u>Upstream Manhole</u>  |            |             |         |  |             |             |               |   |      |
| PN   | Hyd Sect   | Diam (mm)   | MH Name | C.Level (m)                                | I.Level (m) | D.Depth (m) | MH Connection | MH DIAM., (mm)  | L*W  |
| 1.000  | o          | 225         | S 1.0   | 80.043                                     | 78.624      | 1.194       | Open Manhole  |   | 1200 |
| 1.001  | o          | 225         | S 1.1   | 79.974                                     | 78.539      | 1.210       | Open Manhole  |   | 1200 |
| 1.002  | o          | 300         | S 1.2   | 79.910                                     | 78.396      | 1.214       | Open Manhole  |   | 1350 |
| 1.003  | o          | 300         | S 1.3   | 79.712                                     | 78.241      | 1.171       | Open Manhole  |   | 1350 |
| 1.004  | o          | 300         | S 1.4   | 79.672                                     | 78.199      | 1.173       | Open Manhole  |   | 1350 |
| 2.000  | o          | 225         | S 2.0   | 79.663                                     | 78.248      | 1.190       | Open Manhole  |   | 1200 |
| 1.005  | o          | 450         | S 1.5   | 79.433                                     | 77.913      | 1.070       | Open Manhole  |   | 1200 |
| 1.006  | o          | 450         | S 1.6   | 79.108                                     | 77.811      | 0.847       | Open Manhole  |   | 1500 |
| 1.007  | o          | 450         | S 1.7   | 79.068                                     | 77.761      | 0.857       | Open Manhole  |   | 1500 |
| 1.008  | o          | 450         | S 1.8   | 79.138                                     | 77.677      | 1.011       | Open Manhole  |   | 1500 |
| 3.000  | o          | 225         | S 3.0   | 79.452                                     | 77.959      | 1.268       | Open Manhole  |   | 1200 |
| 1.009  | o          | 450         | S 1.9   | 79.128                                     | 77.544      | 1.134       | Open Manhole  |   | 1350 |
| 1.010  | o          | 450         | S 1.10  | 79.207                                     | 77.383      | 1.374       | Open Manhole  |   | 1650 |
| 1.011  | o          | 600         | S 1.11  | 79.207                                     | 77.133      | 1.474       | Open Manhole  |   | 1650 |
| 1.012  | o          | 600         | S 1.12  | 79.330                                     | 77.084      | 1.646       | Open Manhole  |   | 1500 |
| 1.013  | o          | 600         | S 1.13  | 79.330                                     | 77.025      | 1.705       | Open Manhole  |   | 1650 |
| <u>Downstream Manhole</u>  |            |             |         |  |             |             |               |   |      |
| PN   | Length (m) | Slope (1:X) | MH Name | C.Level (m)                                | I.Level (m) | D.Depth (m) | MH Connection | MH DIAM., (mm)  | L*W  |
| 1.000  | 16.964     | 199.6       | S 1.1   | 79.974                                     | 78.539      | 1.210       | Open Manhole  |   | 1200 |
| 1.001  | 13.677     | 201.1       | S 1.2   | 79.910                                     | 78.471      | 1.214       | Open Manhole  |   | 1350 |
| 1.002  | 46.642     | 300.9       | S 1.3   | 79.712                                     | 78.241      | 1.171       | Open Manhole  |   | 1350 |
| 1.003  | 12.681     | 301.9       | S 1.4   | 79.672                                     | 78.199      | 1.173       | Open Manhole  |   | 1350 |
| 1.004  | 40.946     | 301.1       | S 1.5   | 79.433                                     | 78.063      | 1.070       | Open Manhole  |   | 1200 |
| 2.000  | 21.396     | 200.0       | S 1.5   | 79.433                                     | 78.141      | 1.067       | Open Manhole  |   | 1200 |
| 1.005  | 40.880     | 400.8       | S 1.6   | 79.108                                     | 77.811      | 0.847       | Open Manhole  |   | 1500 |
| 1.006  | 20.017     | 400.3       | S 1.7   | 79.068                                     | 77.761      | 0.857       | Open Manhole  |   | 1500 |
| 1.007  | 33.574     | 399.7       | S 1.8   | 79.138                                     | 77.677      | 1.011       | Open Manhole  |   | 1500 |
| 1.008  | 52.436     | 400.3       | S 1.9   | 79.128                                     | 77.546      | 1.132       | Open Manhole  |   | 1350 |
| 3.000  | 37.955     | 199.8       | S 1.9   | 79.128                                     | 77.769      | 1.134       | Open Manhole  |   | 1350 |
| 1.009  | 64.358     | 399.7       | S 1.10  | 79.207                                     | 77.383      | 1.374       | Open Manhole  |   | 1650 |
| 1.010  | 40.080     | 400.8       | S 1.11  | 79.207                                     | 77.283      | 1.474       | Open Manhole  |   | 1650 |
| 1.011  | 24.280     | 495.5       | S 1.12  | 79.330                                     | 77.084      | 1.646       | Open Manhole  |   | 1500 |
| 1.012  | 29.641     | 502.4       | S 1.13  | 79.330                                     | 77.025      | 1.705       | Open Manhole  |   | 1650 |
| 1.013  | 65.828     | 498.7       | S 1.14  | 79.818                                     | 76.893      | 2.325       | Open Manhole  |   | 1950 |
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PIPELINE SCHEDULES for Network 1

Upstream Manhole


| PN    | Hyd<br>Sect | Diam<br>(mm) | MH<br>Name | C.Level<br>(m) | I.Level<br>(m) | D.Depth<br>(m) | MH<br>Connection | MH DIAM., L*W<br>(mm) |
|-------|-------------|--------------|------------|----------------|----------------|----------------|------------------|-----------------------|
| 4.000 | o           | 300          | S 4.0      | 79.000         | 77.381         | 1.319          | Open Manhole     | 1200                  |
| 1.014 | o           | 600          | S 1.14     | 79.818         | 76.781         | 2.437          | Open Manhole     | 1950                  |
| 5.000 | o           | 300          | S 5.0      | 79.867         | 78.366         | 1.201          | Open Manhole     | 1200                  |
| 5.001 | o           | 300          | S 5.1      | 79.857         | 78.231         | 1.326          | Open Manhole     | 1200                  |
| 5.002 | o           | 300          | S 5.2      | 79.845         | 78.085         | 1.460          | Open Manhole     | 1350                  |
| 5.003 | o           | 375          | S 5.3      | 79.831         | 77.843         | 1.613          | Open Manhole     | 1350                  |
| 6.000 | o           | 300          | S 6.0      | 79.823         | 78.268         | 1.255          | Open Manhole     | 1200                  |
| 6.001 | o           | 300          | S 6.1      | 79.824         | 78.133         | 1.391          | Open Manhole     | 1200                  |
| 6.002 | o           | 300          | S 6.2      | 79.824         | 77.987         | 1.537          | Open Manhole     | 1350                  |
| 6.003 | o           | 375          | S 6.3      | 79.823         | 77.745         | 1.703          | Open Manhole     | 1350                  |
| 6.004 | o           | 375          | S 6.4      | 79.569         | 77.632         | 1.562          | Open Manhole     | 1350                  |
| 5.004 | o           | 375          | S 5.4      | 79.573         | 77.398         | 1.800          | Open Manhole     | 1500                  |
| 1.015 | o           | 300          | S 1.15     | 79.000         | 76.750         | 1.950          | Open Manhole     | 2100                  |
| 1.016 | o           | 300          | S 1.16     | 78.963         | 76.284         | 2.379          | Open Manhole     | 2100                  |
| 1.017 | o           | 300          | S 1.17     | 77.991         | 75.967         | 1.724          | Open Manhole     | 2100                  |
| 1.018 | o           | 300          | S 1.18     | 77.551         | 75.583         | 1.668          | Open Manhole     | 2250                  |

Downstream Manhole

| PN    | Length<br>(m) | Slope<br>(1:X) | MH<br>Name | C.Level<br>(m) | I.Level<br>(m) | D.Depth<br>(m) | MH<br>Connection | MH DIAM., L*W<br>(mm) |
|-------|---------------|----------------|------------|----------------|----------------|----------------|------------------|-----------------------|
| 4.000 | 60.127        | 300.6          | S 1.14     | 79.818         | 77.181         | 2.337          | Open Manhole     | 1950                  |
| 1.014 | 13.518        | 500.7          | S 1.15     | 79.000         | 76.754         | 1.646          | Open Manhole     | 2100                  |
| 5.000 | 40.474        | 299.8          | S 5.1      | 79.857         | 78.231         | 1.326          | Open Manhole     | 1200                  |
| 5.001 | 43.937        | 300.9          | S 5.2      | 79.845         | 78.085         | 1.460          | Open Manhole     | 1350                  |
| 5.002 | 50.000        | 299.4          | S 5.3      | 79.831         | 77.918         | 1.613          | Open Manhole     | 1350                  |
| 5.003 | 33.783        | 299.0          | S 5.4      | 79.573         | 77.730         | 1.468          | Open Manhole     | 1500                  |
| 6.000 | 40.474        | 299.8          | S 6.1      | 79.824         | 78.133         | 1.391          | Open Manhole     | 1200                  |
| 6.001 | 43.937        | 300.9          | S 6.2      | 79.824         | 77.987         | 1.537          | Open Manhole     | 1350                  |
| 6.002 | 50.000        | 299.4          | S 6.3      | 79.823         | 77.820         | 1.703          | Open Manhole     | 1350                  |
| 6.003 | 33.783        | 299.0          | S 6.4      | 79.569         | 77.632         | 1.562          | Open Manhole     | 1350                  |
| 6.004 | 70.309        | 300.5          | S 5.4      | 79.573         | 77.398         | 1.800          | Open Manhole     | 1500                  |
| 5.004 | 36.054        | 300.5          | S 1.15     | 79.000         | 77.278         | 1.347          | Open Manhole     | 2100                  |
| 1.015 | 93.160        | 199.9          | S 1.16     | 78.963         | 76.284         | 2.379          | Open Manhole     | 2100                  |
| 1.016 | 63.465        | 200.2          | S 1.17     | 77.991         | 75.967         | 1.724          | Open Manhole     | 2100                  |
| 1.017 | 69.205        | 180.2          | S 1.18     | 77.551         | 75.583         | 1.668          | Open Manhole     | 2250                  |
| 1.018 | 5.054         | 153.2          | MH80       | 77.451         | 75.550         | 1.601          | Open Manhole     | 1500                  |

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|--|----------------|--------------|--|--------------------|-------------------|---|
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| Innovyze   |                |              | Network 2020.1.3                           |                    |                   |   |
| <u>Area Summary for Network 1</u>                                  |                |              |  |                    |                   |   |
| Pipe<br>Number   | PIMP<br>Type   | PIMP<br>Name | PIMP<br>(%)                                | Gross<br>Area (ha) | Imp.<br>Area (ha) | Pipe Total<br>(ha)  |
| 1.000  | Classification | Roads        | 100  | 0.017              | 0.017             | 0.017   |
| 1.001  | Classification | Roads        | 100  | 0.013              | 0.013             | 0.013   |
|  | Classification | Grass        | 30   | 0.039              | 0.012             | 0.024   |
| 1.002  | Classification | Roads        | 100  | 0.017              | 0.017             | 0.017   |
| 1.003  | Classification | Roads        | 100  | 0.100              | 0.100             | 0.100   |
| 1.004  | Classification | Roads        | 100  | 0.024              | 0.024             | 0.024   |
| 2.000  | Classification | Roads        | 100  | 0.030              | 0.030             | 0.030   |
| 1.005  | Classification | Roads        | 100  | 0.047              | 0.047             | 0.047   |
| 1.006  | Classification | Roads        | 100  | 0.101              | 0.101             | 0.101   |
| 1.007  | Classification | Roads        | 100  | 0.025              | 0.025             | 0.025   |
|  | Classification | Roof         | 100  | 0.041              | 0.041             | 0.066   |
|  | Classification | Grass        | 30   | 0.017              | 0.005             | 0.071   |
| 1.008  | Classification | Roads        | 100  | 0.111              | 0.111             | 0.111   |
|  | Classification | Grass        | 30   | 0.020              | 0.006             | 0.117   |
|  | Classification | Roads        | 100  | 0.105              | 0.105             | 0.222   |
| 3.000  | Classification | Roads        | 100  | 0.034              | 0.034             | 0.034   |
|  | Classification | Roads        | 100  | 0.105              | 0.105             | 0.138   |
|  | Classification | Grass        | 30   | 0.028              | 0.008             | 0.147   |
| 1.009  | Classification | Roads        | 100  | 0.233              | 0.233             | 0.233   |
|  | Classification | Grass        | 30   | 0.024              | 0.007             | 0.240   |
| 1.010  | Classification | Roads        | 100  | 0.120              | 0.120             | 0.120   |
|  | Classification | Grass        | 30   | 0.035              | 0.011             | 0.130   |
| 1.011  | Classification | Roads        | 100  | 0.242              | 0.242             | 0.242   |
|  | Classification | Grass        | 30   | 0.050              | 0.015             | 0.257   |
| 1.012  | -              | -            | 100  | 0.000              | 0.000             | 0.000   |
| 1.013  | Classification | Roads        | 100  | 0.125              | 0.125             | 0.125   |
|  | Classification | Grass        | 30   | 0.037              | 0.011             | 0.136   |
|  | Classification | Grass        | 30   | 0.070              | 0.021             | 0.157   |
| 4.000  | Classification | Roads        | 100  | 0.057              | 0.057             | 0.057   |
| 1.014  | Classification | Roads        | 100  | 0.099              | 0.099             | 0.099   |
| 5.000  | Classification | Roof         | 100  | 0.115              | 0.115             | 0.115   |
| 5.001  | Classification | Roof         | 100  | 0.131              | 0.131             | 0.131   |
| 5.002  | Classification | Roof         | 100  | 0.145              | 0.145             | 0.145   |
| 5.003  | Classification | Roof         | 100  | 0.169              | 0.169             | 0.169   |
| 6.000  | Classification | Roof         | 100  | 0.115              | 0.115             | 0.115   |
| 6.001  | Classification | Roof         | 100  | 0.131              | 0.131             | 0.131   |
| 6.002  | Classification | Roof         | 100  | 0.145              | 0.145             | 0.145   |
| 6.003  | Classification | Roof         | 100  | 0.169              | 0.169             | 0.169   |
| 6.004  | Classification | Roof         | 100  | 0.080              | 0.080             | 0.080   |
| 5.004  | Classification | Roof         | 100  | 0.080              | 0.080             | 0.080   |
| 1.015  | -              | -            | 100  | 0.000              | 0.000             | 0.000   |
| 1.016  | -              | -            | 100  | 0.000              | 0.000             | 0.000   |
| 1.017  | -              | -            | 100  | 0.000              | 0.000             | 0.000   |
| 1.018  | -              | -            | 100  | 0.000              | 0.000             | 0.000   |
|  |                |              |  | Total              | Total             | Total   |
|  |                |              |  | 3.243              | 3.019             | 3.019   |
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Network Classifications for Network 1


| PN    | USMH<br>Name | Pipe<br>Dia<br>(mm) | Min Cover<br>Depth<br>(m) | Max Cover<br>Depth<br>(m) | Pipe Type    | MH<br>Dia<br>(mm) | MH<br>Width<br>(mm) | MH Ring<br>Depth<br>(m) | MH Type      |
|-------|--------------|---------------------|---------------------------|---------------------------|--------------|-------------------|---------------------|-------------------------|--------------|
| 1.000 | S 1.0        | 225                 | 1.194                     | 1.210                     | Unclassified | 1200              | 0                   | 1.194                   | Unclassified |
| 1.001 | S 1.1        | 225                 | 1.210                     | 1.214                     | Unclassified | 1200              | 0                   | 1.210                   | Unclassified |
| 1.002 | S 1.2        | 300                 | 1.171                     | 1.214                     | Unclassified | 1350              | 0                   | 1.214                   | Unclassified |
| 1.003 | S 1.3        | 300                 | 1.171                     | 1.173                     | Unclassified | 1350              | 0                   | 1.171                   | Unclassified |
| 1.004 | S 1.4        | 300                 | 1.070                     | 1.173                     | Unclassified | 1350              | 0                   | 1.173                   | Unclassified |
| 2.000 | S 2.0        | 225                 | 1.067                     | 1.190                     | Unclassified | 1200              | 0                   | 1.190                   | Unclassified |
| 1.005 | S 1.5        | 450                 | 0.847                     | 1.070                     | Unclassified | 1200              | 0                   | 1.070                   | Unclassified |
| 1.006 | S 1.6        | 450                 | 0.847                     | 0.857                     | Unclassified | 1500              | 0                   | 0.847                   | Unclassified |
| 1.007 | S 1.7        | 450                 | 0.857                     | 1.011                     | Unclassified | 1500              | 0                   | 0.857                   | Unclassified |
| 1.008 | S 1.8        | 450                 | 1.011                     | 1.132                     | Unclassified | 1500              | 0                   | 1.011                   | Unclassified |
| 3.000 | S 3.0        | 225                 | 1.134                     | 1.268                     | Unclassified | 1200              | 0                   | 1.268                   | Unclassified |
| 1.009 | S 1.9        | 450                 | 1.134                     | 1.374                     | Unclassified | 1350              | 0                   | 1.134                   | Unclassified |
| 1.010 | S 1.10       | 450                 | 1.374                     | 1.474                     | Unclassified | 1650              | 0                   | 1.374                   | Unclassified |
| 1.011 | S 1.11       | 600                 | 1.474                     | 1.646                     | Unclassified | 1650              | 0                   | 1.474                   | Unclassified |
| 1.012 | S 1.12       | 600                 | 1.646                     | 1.705                     | Unclassified | 1500              | 0                   | 1.646                   | Unclassified |
| 1.013 | S 1.13       | 600                 | 1.705                     | 2.325                     | Unclassified | 1650              | 0                   | 1.705                   | Unclassified |
| 4.000 | S 4.0        | 300                 | 1.319                     | 2.337                     | Unclassified | 1200              | 0                   | 1.319                   | Unclassified |
| 1.014 | S 1.14       | 600                 | 1.646                     | 2.437                     | Unclassified | 1950              | 0                   | 2.437                   | Unclassified |
| 5.000 | S 5.0        | 300                 | 1.201                     | 1.326                     | Unclassified | 1200              | 0                   | 1.201                   | Unclassified |
| 5.001 | S 5.1        | 300                 | 1.326                     | 1.460                     | Unclassified | 1200              | 0                   | 1.326                   | Unclassified |
| 5.002 | S 5.2        | 300                 | 1.460                     | 1.613                     | Unclassified | 1350              | 0                   | 1.460                   | Unclassified |
| 5.003 | S 5.3        | 375                 | 1.468                     | 1.613                     | Unclassified | 1350              | 0                   | 1.613                   | Unclassified |
| 6.000 | S 6.0        | 300                 | 1.255                     | 1.391                     | Unclassified | 1200              | 0                   | 1.255                   | Unclassified |
| 6.001 | S 6.1        | 300                 | 1.391                     | 1.537                     | Unclassified | 1200              | 0                   | 1.391                   | Unclassified |
| 6.002 | S 6.2        | 300                 | 1.537                     | 1.703                     | Unclassified | 1350              | 0                   | 1.537                   | Unclassified |
| 6.003 | S 6.3        | 375                 | 1.562                     | 1.703                     | Unclassified | 1350              | 0                   | 1.703                   | Unclassified |
| 6.004 | S 6.4        | 375                 | 1.562                     | 1.800                     | Unclassified | 1350              | 0                   | 1.562                   | Unclassified |
| 5.004 | S 5.4        | 375                 | 1.347                     | 1.800                     | Unclassified | 1500              | 0                   | 1.800                   | Unclassified |
| 1.015 | S 1.15       | 300                 | 1.950                     | 2.379                     | Unclassified | 2100              | 0                   | 1.950                   | Unclassified |
| 1.016 | S 1.16       | 300                 | 1.724                     | 2.379                     | Unclassified | 2100              | 0                   | 2.379                   | Unclassified |
| 1.017 | S 1.17       | 300                 | 1.668                     | 1.724                     | Unclassified | 2100              | 0                   | 1.724                   | Unclassified |
| 1.018 | S 1.18       | 300                 | 1.601                     | 1.668                     | Unclassified | 2250              | 0                   | 1.668                   | Unclassified |

Free Flowing Outfall Details for Network 1

| Outfall<br>Pipe Number | Outfall<br>Name | C. Level<br>(m) | I. Level<br>(m) | Min<br>I. Level<br>(m) | D,L<br>(mm) | W<br>(mm) |
|------------------------|-----------------|-----------------|-----------------|------------------------|-------------|-----------|
| 1.018                  | MH80            | 77.451          | 75.550          | 0.000                  | 1500        | 0         |

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| <p align="center"><u>Simulation Criteria for Network 1</u></p> <p> Volumetric Runoff Coeff 0.750    Additional Flow - % of Total Flow 0.000<br/> Areal Reduction Factor 1.000    MADD Factor * 10m³/ha Storage 2.000<br/> Hot Start (mins) 0    Inlet Coefficient 0.800<br/> Hot Start Level (mm) 0    Flow per Person per Day (l/per/day) 0.000<br/> Manhole Headloss Coeff (Global) 0.500    Run Time (mins) 60<br/> Foul Sewage per hectare (l/s) 0.000    Output Interval (mins) 1 </p> <p> Number of Input Hydrographs 0    Number of Storage Structures 1<br/> Number of Online Controls 1    Number of Time/Area Diagrams 0<br/> Number of Offline Controls 0    Number of Real Time Controls 0 </p> <p align="center"><u>Synthetic Rainfall Details</u></p> <p> Rainfall Model    FSR    Profile Type Summer<br/> Return Period (years) 25    Cv (Summer) 0.750<br/> Region Scotland and Ireland    Cv (Winter) 0.840<br/> M5-60 (mm) 16.500    Storm Duration (mins) 30<br/> Ratio R 0.300 </p> |  |   |
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|  |  |   |            |            |            |            |            |            |           |            |       |     |       |     |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |  |  |       |      |       |      |       |      |  |  |
|--|--|---|------------|------------|------------|------------|------------|------------|-----------|------------|-------|-----|-------|-----|-------|------|-------|------|-------|------|-------|------|-------|------|-------|------|-------|------|-------|------|-------|------|-------|------|-------|------|-------|------|-------|------|-------|------|-------|------|-------|------|-------|------|-------|------|-------|------|-------|------|-------|------|-------|------|-------|------|-------|------|-------|------|--|--|-------|------|-------|------|-------|------|--|--|
| Clifton Scannell Emerson Associates  |  | Page 13   |            |            |            |            |            |            |           |            |       |     |       |     |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |  |  |       |      |       |      |       |      |  |  |
| Seefort Lodge<br>Castledawson Avenue, Blackrock<br>Dublin, Ireland   | Project:<br>Huntstown data centre facility |  |            |            |            |            |            |            |           |            |       |     |       |     |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |  |  |       |      |       |      |       |      |  |  |
| Date 06/05/2021<br>File DUB041 SW Network-1.mdx  | Designed by ZS<br>Checked by CD            |   |            |            |            |            |            |            |           |            |       |     |       |     |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |  |  |       |      |       |      |       |      |  |  |
| Innovyze<br>Network 2020.1.3   |  |   |            |            |            |            |            |            |           |            |       |     |       |     |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |  |  |       |      |       |      |       |      |  |  |
| <div>Online Controls for Network 1</div> <div>Hydro-Brake® Optimum Manhole: S 1.15, DS/PN: 1.015, Volume (m³): 14.8</div> <div><div>Unit Reference MD-SHE-0144-1200-1950-1200</div><div>Design Head (m)1.950</div><div>Design Flow (l/s)12.0</div><div>Flush-Flo™Calculated</div><div>ObjectiveMinimise upstream storage</div><div>ApplicationSurface</div><div>Sump AvailableYes</div><div>Diameter (mm)144</div><div>Invert Level (m)76.750</div><div>Minimum Outlet Pipe Diameter (mm)225</div><div>Suggested Manhole Diameter (mm)1500</div></div> <div><div>Control Points</div><div>Head (m)Flow (l/s)</div><div>Design Point (Calculated)1.95012.0</div><div>Flush-Flo™0.56612.0</div><div>Kick-Flo®1.1779.5</div><div>Mean Flow over Head Range-10.5</div></div> <div>The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake® Optimum as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated</div> <div><table><tr><td>Depth (m)</td><td>Flow (l/s)</td><td>Depth (m)</td><td>Flow (l/s)</td><td>Depth (m)</td><td>Flow (l/s)</td><td>Depth (m)</td><td>Flow (l/s)</td></tr><tr><td>0.100</td><td>5.2</td><td>1.200</td><td>9.5</td><td>3.000</td><td>14.7</td><td>7.000</td><td>22.1</td></tr><tr><td>0.200</td><td>10.1</td><td>1.400</td><td>10.3</td><td>3.500</td><td>15.8</td><td>7.500</td><td>22.8</td></tr><tr><td>0.300</td><td>11.2</td><td>1.600</td><td>10.9</td><td>4.000</td><td>16.9</td><td>8.000</td><td>23.5</td></tr><tr><td>0.400</td><td>11.7</td><td>1.800</td><td>11.6</td><td>4.500</td><td>17.9</td><td>8.500</td><td>24.2</td></tr><tr><td>0.500</td><td>11.9</td><td>2.000</td><td>12.1</td><td>5.000</td><td>18.8</td><td>9.000</td><td>24.9</td></tr><tr><td>0.600</td><td>12.0</td><td>2.200</td><td>12.7</td><td>5.500</td><td>19.7</td><td>9.500</td><td>25.6</td></tr><tr><td>0.800</td><td>11.7</td><td>2.400</td><td>13.2</td><td>6.000</td><td>20.5</td><td></td><td></td></tr><tr><td>1.000</td><td>11.0</td><td>2.600</td><td>13.7</td><td>6.500</td><td>21.3</td><td></td><td></td></tr></table></div> <div>©1982-2020 Innovyze</div> |  |   | Depth (m)  | Flow (l/s) | Depth (m)  | Flow (l/s) | Depth (m)  | Flow (l/s) | Depth (m) | Flow (l/s) | 0.100 | 5.2 | 1.200 | 9.5 | 3.000 | 14.7 | 7.000 | 22.1 | 0.200 | 10.1 | 1.400 | 10.3 | 3.500 | 15.8 | 7.500 | 22.8 | 0.300 | 11.2 | 1.600 | 10.9 | 4.000 | 16.9 | 8.000 | 23.5 | 0.400 | 11.7 | 1.800 | 11.6 | 4.500 | 17.9 | 8.500 | 24.2 | 0.500 | 11.9 | 2.000 | 12.1 | 5.000 | 18.8 | 9.000 | 24.9 | 0.600 | 12.0 | 2.200 | 12.7 | 5.500 | 19.7 | 9.500 | 25.6 | 0.800 | 11.7 | 2.400 | 13.2 | 6.000 | 20.5 |  |  | 1.000 | 11.0 | 2.600 | 13.7 | 6.500 | 21.3 |  |  |
| Depth (m)  | Flow (l/s)                                 | Depth (m)   | Flow (l/s) | Depth (m)  | Flow (l/s) | Depth (m)  | Flow (l/s) |            |           |            |       |     |       |     |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |  |  |       |      |       |      |       |      |  |  |
| 0.100  | 5.2  | 1.200   | 9.5        | 3.000      | 14.7       | 7.000      | 22.1       |            |           |            |       |     |       |     |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |  |  |       |      |       |      |       |      |  |  |
| 0.200  | 10.1                                       | 1.400   | 10.3       | 3.500      | 15.8       | 7.500      | 22.8       |            |           |            |       |     |       |     |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |  |  |       |      |       |      |       |      |  |  |
| 0.300  | 11.2                                       | 1.600   | 10.9       | 4.000      | 16.9       | 8.000      | 23.5       |            |           |            |       |     |       |     |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |  |  |       |      |       |      |       |      |  |  |
| 0.400  | 11.7                                       | 1.800   | 11.6       | 4.500      | 17.9       | 8.500      | 24.2       |            |           |            |       |     |       |     |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |  |  |       |      |       |      |       |      |  |  |
| 0.500  | 11.9                                       | 2.000   | 12.1       | 5.000      | 18.8       | 9.000      | 24.9       |            |           |            |       |     |       |     |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |  |  |       |      |       |      |       |      |  |  |
| 0.600  | 12.0                                       | 2.200   | 12.7       | 5.500      | 19.7       | 9.500      | 25.6       |            |           |            |       |     |       |     |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |  |  |       |      |       |      |       |      |  |  |
| 0.800  | 11.7                                       | 2.400   | 13.2       | 6.000      | 20.5       |            |            |            |           |            |       |     |       |     |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |  |  |       |      |       |      |       |      |  |  |
| 1.000  | 11.0                                       | 2.600   | 13.7       | 6.500      | 21.3       |            |            |            |           |            |       |     |       |     |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |       |      |  |  |       |      |       |      |       |      |  |  |

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|--|--|---|
| Clifton Scannell Emerson Associates  |  | Page 14   |
| Seefort Lodge<br>Castledawson Avenue, Blackrock<br>Dublin, Ireland   | Project:<br>Huntstown data centre facility |  |
| Date 06/05/2021<br>File DUB041 SW Network-1.mdx  | Designed by ZS<br>Checked by CD            |   |
| Innovyze   | Network 2020.1.3                           |   |
| <div><div><div><div><div><div></div><div><u>Storage Structures for Network 1</u></div></div></div><div><div><div><div><div><div></div><div><u>Tank or Pond Manhole: S 1.15, DS/PN: 1.015</u></div></div></div><div><div><div><div><div><div></div><div>Invert Level (m) 76.750</div></div></div><div><div><div><div><div><div></div><div>Depth (m)</div><div>Area (m²)</div></div><div>0.000</div><div>329.0</div></div><div><div><div><div><div><div></div><div>Depth (m)</div><div>Area (m²)</div></div><div>2.250</div><div>1292.0</div></div></div></div></div><div><div><div><div><div><div></div><div><u>Manhole Headloss for Network 1</u></div></div></div><div><div><div><div><div><div></div><div>PN</div><div>US/MH</div><div>US/MH</div></div><div><div>Name</div><div>Headloss</div></div></div><div><div><div><div><div><div></div><div>1.000</div><div>S 1.0</div><div>0.500</div></div><div><div><div><div><div><div></div><div>1.001</div><div>S 1.1</div><div>0.500</div></div><div><div><div><div><div><div></div><div>1.002</div><div>S 1.2</div><div>0.500</div></div><div><div><div><div><div><div></div><div>1.003</div><div>S 1.3</div><div>0.500</div></div><div><div><div><div><div><div></div><div>1.004</div><div>S 1.4</div><div>0.500</div></div><div><div><div><div><div><div></div><div>2.000</div><div>S 2.0</div><div>0.500</div></div><div><div><div><div><div><div></div><div>1.005</div><div>S 1.5</div><div>0.500</div></div><div><div><div><div><div><div></div><div>1.006</div><div>S 1.6</div><div>0.500</div></div><div><div><div><div><div><div></div><div>1.007</div><div>S 1.7</div><div>0.500</div></div><div><div><div><div><div><div></div><div>1.008</div><div>S 1.8</div><div>0.500</div></div><div><div><div><div><div><div></div><div>3.000</div><div>S 3.0</div><div>0.500</div></div><div><div><div><div><div><div></div><div>1.009</div><div>S 1.9</div><div>0.500</div></div><div><div><div><div><div><div></div><div>1.010</div><div>S 1.10</div><div>0.500</div></div><div><div><div><div><div><div></div><div>1.011</div><div>S 1.11</div><div>0.500</div></div><div><div><div><div><div><div></div><div>1.012</div><div>S 1.12</div><div>0.500</div></div><div><div><div><div><div><div></div><div>1.013</div><div>S 1.13</div><div>0.500</div></div><div><div><div><div><div><div></div><div>4.000</div><div>S 4.0</div><div>0.500</div></div><div><div><div><div><div><div></div><div>1.014</div><div>S 1.14</div><div>0.500</div></div><div><div><div><div><div><div></div><div>5.000</div><div>S 5.0</div><div>0.500</div></div><div><div><div><div><div><div></div><div>5.001</div><div>S 5.1</div><div>0.500</div></div><div><div><div><div><div><div></div><div>5.002</div><div>S 5.2</div><div>0.500</div></div><div><div><div><div><div><div></div><div>5.003</div><div>S 5.3</div><div>0.500</div></div><div><div><div><div><div><div></div><div>6.000</div><div>S 6.0</div><div>0.500</div></div><div><div><div><div><div><div></div><div>6.001</div><div>S 6.1</div><div>0.500</div></div><div><div><div><div><div><div></div><div>6.002</div><div>S 6.2</div><div>0.500</div></div><div><div><div><div><div><div></div><div>6.003</div><div>S 6.3</div><div>0.500</div></div><div><div><div><div><div><div></div><div>6.004</div><div>S 6.4</div><div>0.500</div></div><div><div><div><div><div><div></div><div>5.004</div><div>S 5.4</div><div>0.500</div></div><div><div><div><div><div><div></div><div>1.015</div><div>S 1.15</div><div>0.500</div></div><div><div><div><div><div><div></div><div>1.016</div><div>S 1.16</div><div>0.500</div></div><div><div><div><div><div><div></div><div>1.017</div><div>S 1.17</div><div>0.500</div></div><div><div><div><div><div><div></div><div>1.018</div><div>S 1.18</div><div>0.500</div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div></div> |  |   |

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Seefort Lodge

Castledawson Avenue, Blackrock

Dublin, Ireland

Date 06/05/2021

File DUB041 SW Network-1.mdx

Project:

Huntstown data centre facility

Designed by ZS

Checked by CD

Innovyze

Network 2020.1.3

1 year Return Period Summary of Critical Results by Maximum Level (Rank 1)

for Network 1

Simulation Criteria

Areal Reduction Factor 1.000

Additional Flow - % of Total Flow 0.000

Hot Start (mins) 0

MADD Factor \* 10m³/ha Storage 2.000

Hot Start Level (mm) 0

Inlet Coeffiecient 0.800

Manhole Headloss Coeff (Global) 0.500

Flow per Person per Day (l/per/day) 0.000

Foul Sewage per hectare (l/s) 0.000

Number of Input Hydrographs 0

Number of Storage Structures 1

Number of Online Controls 1

Number of Time/Area Diagrams 0

Number of Offline Controls 0

Number of Real Time Controls 0

Synthetic Rainfall Details

Rainfall Model FSR

Ratio R 0.300

Region Scotland and Ireland Cv (Summer) 0.750

M5-60 (mm) 16.500 Cv (Winter) 0.840

Margin for Flood Risk Warning (mm) 300.0

DVD Status OFF

Analysis Timestep Fine

Inertia Status OFF

DTS Status ON

Profile(s) Summer and Winter

Duration(s) (mins) 15, 30, 60, 120, 240, 360, 480, 960, 1440

Return Period(s) (years) 1, 30, 100


Climate Change (%) 10, 10, 10

|       | US/MH  |            | Return | Climate | First (X)     | First (Y) | First (Z) | Overflow | Water  |
|-------|--------|------------|--------|---------|---------------|-----------|-----------|----------|--------|
| PN    | Name   | Storm      | Period | Change  | Surcharge     | Flood     | Overflow  | Act.     | Level  |
|       |        |            |        |         |               |           |           |          | (m)    |
| 1.000 | S 1.0  | 15 Winter  | 1      | +10%    |               |           |           |          | 78.662 |
| 1.001 | S 1.1  | 15 Winter  | 1      | +10%    |               |           |           |          | 78.597 |
| 1.002 | S 1.2  | 15 Winter  | 1      | +10%    | 100/15 Winter |           |           |          | 78.462 |
| 1.003 | S 1.3  | 15 Winter  | 1      | +10%    | 100/15 Summer |           |           |          | 78.357 |
| 1.004 | S 1.4  | 15 Winter  | 1      | +10%    | 100/15 Summer |           |           |          | 78.314 |
| 2.000 | S 2.0  | 15 Winter  | 1      | +10%    | 100/15 Summer |           |           |          | 78.299 |
| 1.005 | S 1.5  | 15 Winter  | 1      | +10%    | 100/15 Summer |           |           |          | 78.054 |
| 1.006 | S 1.6  | 15 Winter  | 1      | +10%    | 30/15 Winter  |           |           |          | 77.986 |
| 1.007 | S 1.7  | 15 Winter  | 1      | +10%    | 30/15 Winter  |           |           |          | 77.943 |
| 1.008 | S 1.8  | 15 Winter  | 1      | +10%    | 30/15 Summer  |           |           |          | 77.880 |
| 3.000 | S 3.0  | 15 Winter  | 1      | +10%    | 30/15 Summer  |           |           |          | 78.077 |
| 1.009 | S 1.9  | 15 Winter  | 1      | +10%    | 30/15 Summer  |           |           |          | 77.792 |
| 1.010 | S 1.10 | 15 Winter  | 1      | +10%    | 30/15 Summer  |           |           |          | 77.648 |
| 1.011 | S 1.11 | 480 Winter | 1      | +10%    | 30/60 Summer  |           |           |          | 77.571 |
| 1.012 | S 1.12 | 480 Winter | 1      | +10%    | 30/30 Winter  |           |           |          | 77.570 |
| 1.013 | S 1.13 | 480 Winter | 1      | +10%    | 30/30 Winter  |           |           |          | 77.569 |
| 4.000 | S 4.0  | 480 Winter | 1      | +10%    | 30/60 Summer  |           |           |          | 77.567 |
| 1.014 | S 1.14 | 480 Winter | 1      | +10%    | 1/120 Summer  |           |           |          | 77.567 |
| 5.000 | S 5.0  | 15 Winter  | 1      | +10%    | 30/15 Summer  |           |           |          | 78.467 |
| 5.001 | S 5.1  | 15 Winter  | 1      | +10%    | 30/15 Summer  |           |           |          | 78.375 |
| 5.002 | S 5.2  | 15 Winter  | 1      | +10%    | 30/15 Summer  |           |           |          | 78.266 |

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|  |  |   |
|--|--|---|
| Seefort Lodge<br>Castledawson Avenue, Blackrock<br>Dublin, Ireland | Project:<br>Huntstown data centre facility |  |
| Date 06/05/2021<br>File DUB041 SW Network-1.mdx                    | Designed by ZS<br>Checked by CD            |   |
| Innovyze<br>Network 2020.1.3                                       |  |   |

1 year Return Period Summary of Critical Results by Maximum Level (Rank 1)  
for Network 1

| PN    | US/MH<br>Name | Surcharged<br>Depth<br>(m) | Flooded<br>Volume<br>(m³) | Flow /<br>Cap. | Overflow<br>(l/s) | Half Drain<br>Time<br>(mins) | Pipe<br>Flow<br>(l/s) | Status     | Level<br>Exceeded |
|-------|---------------|----------------------------|---------------------------|----------------|-------------------|------------------------------|-----------------------|------------|-------------------|
| 1.000 | S 1.0         | -0.187                     | 0.000                     | 0.06           |                   |                              | 2.1                   | OK         |                   |
| 1.001 | S 1.1         | -0.167                     | 0.000                     | 0.15           |                   |                              | 4.7                   | OK         |                   |
| 1.002 | S 1.2         | -0.234                     | 0.000                     | 0.11           |                   |                              | 6.3                   | OK         |                   |
| 1.003 | S 1.3         | -0.184                     | 0.000                     | 0.31           |                   |                              | 16.2                  | OK         |                   |
| 1.004 | S 1.4         | -0.185                     | 0.000                     | 0.31           |                   |                              | 18.5                  | OK         |                   |
| 2.000 | S 2.0         | -0.174                     | 0.000                     | 0.11           |                   |                              | 3.8                   | OK         |                   |
| 1.005 | S 1.5         | -0.309                     | 0.000                     | 0.18           |                   |                              | 25.6                  | OK         |                   |
| 1.006 | S 1.6         | -0.275                     | 0.000                     | 0.26           |                   |                              | 33.6                  | OK         |                   |
| 1.007 | S 1.7         | -0.268                     | 0.000                     | 0.28           |                   |                              | 39.1                  | OK         |                   |
| 1.008 | S 1.8         | -0.247                     | 0.000                     | 0.38           |                   |                              | 55.3                  | OK         |                   |
| 3.000 | S 3.0         | -0.107                     | 0.000                     | 0.54           |                   |                              | 18.7                  | OK         |                   |
| 1.009 | S 1.9         | -0.202                     | 0.000                     | 0.57           |                   |                              | 84.8                  | OK         |                   |
| 1.010 | S 1.10        | -0.185                     | 0.000                     | 0.64           |                   |                              | 91.4                  | OK         |                   |
| 1.011 | S 1.11        | -0.162                     | 0.000                     | 0.11           |                   |                              | 27.3                  | OK         |                   |
| 1.012 | S 1.12        | -0.114                     | 0.000                     | 0.11           |                   |                              | 26.5                  | OK         |                   |
| 1.013 | S 1.13        | -0.056                     | 0.000                     | 0.10           |                   |                              | 28.3                  | OK         |                   |
| 4.000 | S 4.0         | -0.114                     | 0.000                     | 0.02           |                   |                              | 1.1                   | OK         |                   |
| 1.014 | S 1.14        | 0.186                      | 0.000                     | 0.17           |                   |                              | 27.6                  | SURCHARGED |                   |
| 5.000 | S 5.0         | -0.199                     | 0.000                     | 0.24           |                   |                              | 14.2                  | OK         |                   |
| 5.001 | S 5.1         | -0.156                     | 0.000                     | 0.45           |                   |                              | 26.9                  | OK         |                   |
| 5.002 | S 5.2         | -0.119                     | 0.000                     | 0.65           |                   |                              | 39.4                  | OK         |                   |

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Seefort Lodge  
Castledawson Avenue, Blackrock  
Dublin, Ireland

Date 06/05/2021  
File DUB041 SW Network-1.mdx

Project:  
Huntstown data centre facility

Designed by ZS  
Checked by CD

Innovyze

Network 2020.1.3

30 year Return Period Summary of Critical Results by Maximum Level (Rank 1)  
for Network 1

Simulation Criteria

Areal Reduction Factor 1.000

Additional Flow - % of Total Flow 0.000

Hot Start (mins) 0

MADD Factor \* 10m³/ha Storage 2.000

Hot Start Level (mm) 0

Inlet Coeffiecient 0.800

Manhole Headloss Coeff (Global) 0.500

Flow per Person per Day (l/per/day) 0.000

Foul Sewage per hectare (l/s) 0.000

Number of Input Hydrographs 0

Number of Storage Structures 1

Number of Online Controls 1

Number of Time/Area Diagrams 0

Number of Offline Controls 0

Number of Real Time Controls 0

Synthetic Rainfall Details

Rainfall Model FSR

Ratio R 0.300

Region Scotland and Ireland Cv (Summer) 0.750

M5-60 (mm) 16.500 Cv (Winter) 0.840

Margin for Flood Risk Warning (mm) 300.0

DVD Status OFF

Analysis Timestep Fine

Inertia Status OFF

DTS Status ON

Profile(s) Summer and Winter

Duration(s) (mins) 15, 30, 60, 120, 240, 360, 480, 960, 1440

Return Period(s) (years) 1, 30, 100

Climate Change (%) 10, 10, 10

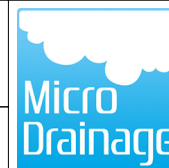
|       | US/MH  |            | Return | Climate | First (X)     | First (Y) | First (Z) | Overflow | Water  |
|-------|--------|------------|--------|---------|---------------|-----------|-----------|----------|--------|
| PN    | Name   | Storm      | Period | Change  | Surcharge     | Flood     | Overflow  | Act.     | Level  |
| 1.000 | S 1.0  | 15 Winter  | 30     | +10%    |               |           |           |          | 78.681 |
| 1.001 | S 1.1  | 15 Winter  | 30     | +10%    |               |           |           |          | 78.635 |
| 1.002 | S 1.2  | 15 Winter  | 30     | +10%    | 100/15 Winter |           |           |          | 78.511 |
| 1.003 | S 1.3  | 15 Winter  | 30     | +10%    | 100/15 Summer |           |           |          | 78.453 |
| 1.004 | S 1.4  | 15 Winter  | 30     | +10%    | 100/15 Summer |           |           |          | 78.408 |
| 2.000 | S 2.0  | 15 Winter  | 30     | +10%    | 100/15 Summer |           |           |          | 78.325 |
| 1.005 | S 1.5  | 960 Winter | 30     | +10%    | 100/15 Summer |           |           |          | 78.311 |
| 1.006 | S 1.6  | 960 Winter | 30     | +10%    | 30/15 Winter  |           |           |          | 78.312 |
| 1.007 | S 1.7  | 960 Winter | 30     | +10%    | 30/15 Winter  |           |           |          | 78.311 |
| 1.008 | S 1.8  | 960 Winter | 30     | +10%    | 30/15 Summer  |           |           |          | 78.310 |
| 3.000 | S 3.0  | 15 Winter  | 30     | +10%    | 30/15 Summer  |           |           |          | 78.317 |
| 1.009 | S 1.9  | 960 Winter | 30     | +10%    | 30/15 Summer  |           |           |          | 78.309 |
| 1.010 | S 1.10 | 960 Winter | 30     | +10%    | 30/15 Summer  |           |           |          | 78.307 |
| 1.011 | S 1.11 | 960 Winter | 30     | +10%    | 30/60 Summer  |           |           |          | 78.305 |
| 1.012 | S 1.12 | 960 Winter | 30     | +10%    | 30/30 Winter  |           |           |          | 78.304 |
| 1.013 | S 1.13 | 960 Winter | 30     | +10%    | 30/30 Winter  |           |           |          | 78.303 |
| 4.000 | S 4.0  | 960 Winter | 30     | +10%    | 30/60 Summer  |           |           |          | 78.301 |
| 1.014 | S 1.14 | 960 Winter | 30     | +10%    | 1/120 Summer  |           |           |          | 78.301 |
| 5.000 | S 5.0  | 15 Winter  | 30     | +10%    | 30/15 Summer  |           |           |          | 78.766 |
| 5.001 | S 5.1  | 15 Winter  | 30     | +10%    | 30/15 Summer  |           |           |          | 78.728 |
| 5.002 | S 5.2  | 15 Winter  | 30     | +10%    | 30/15 Summer  |           |           |          | 78.593 |

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Network 2020.1.3

30 year Return Period Summary of Critical Results by Maximum Level (Rank 1)  
for Network 1


| PN    | US/MH<br>Name | Surcharged   | Flooded        | Flow /<br>Cap. | Overflow<br>(l/s) | Half Drain     | Pipe          | Status     | Level<br>Exceeded |
|-------|---------------|--------------|----------------|----------------|-------------------|----------------|---------------|------------|-------------------|
|       |               | Depth<br>(m) | Volume<br>(m³) |                |                   | Time<br>(mins) | Flow<br>(l/s) |            |                   |
| 1.000 | S 1.0         | -0.168       | 0.000          | 0.14           |                   |                | 4.7           |            | OK                |
| 1.001 | S 1.1         | -0.129       | 0.000          | 0.37           |                   |                | 11.8          |            | OK                |
| 1.002 | S 1.2         | -0.185       | 0.000          | 0.27           |                   |                | 16.0          |            | OK                |
| 1.003 | S 1.3         | -0.088       | 0.000          | 0.83           |                   |                | 43.0          |            | OK                |
| 1.004 | S 1.4         | -0.091       | 0.000          | 0.80           |                   |                | 47.5          |            | OK                |
| 2.000 | S 2.0         | -0.148       | 0.000          | 0.25           |                   |                | 8.3           |            | OK                |
| 1.005 | S 1.5         | -0.052       | 0.000          | 0.04           |                   |                | 6.1           |            | OK                |
| 1.006 | S 1.6         | 0.051        | 0.000          | 0.06           |                   |                | 8.4           | SURCHARGED |                   |
| 1.007 | S 1.7         | 0.100        | 0.000          | 0.07           |                   |                | 10.0          | SURCHARGED |                   |
| 1.008 | S 1.8         | 0.183        | 0.000          | 0.10           |                   |                | 14.9          | SURCHARGED |                   |
| 3.000 | S 3.0         | 0.133        | 0.000          | 1.07           |                   |                | 37.2          | SURCHARGED |                   |
| 1.009 | S 1.9         | 0.315        | 0.000          | 0.15           |                   |                | 22.7          | SURCHARGED |                   |
| 1.010 | S 1.10        | 0.474        | 0.000          | 0.17           |                   |                | 23.6          | SURCHARGED |                   |
| 1.011 | S 1.11        | 0.572        | 0.000          | 0.12           |                   |                | 28.4          | SURCHARGED |                   |
| 1.012 | S 1.12        | 0.620        | 0.000          | 0.11           |                   |                | 27.8          | SURCHARGED |                   |
| 1.013 | S 1.13        | 0.678        | 0.000          | 0.11           |                   |                | 31.2          | SURCHARGED |                   |
| 4.000 | S 4.0         | 0.620        | 0.000          | 0.02           |                   |                | 1.2           | SURCHARGED |                   |
| 1.014 | S 1.14        | 0.920        | 0.000          | 0.21           |                   |                | 34.5          | SURCHARGED |                   |
| 5.000 | S 5.0         | 0.100        | 0.000          | 0.47           |                   |                | 27.8          | SURCHARGED |                   |
| 5.001 | S 5.1         | 0.197        | 0.000          | 0.92           |                   |                | 55.0          | SURCHARGED |                   |
| 5.002 | S 5.2         | 0.208        | 0.000          | 1.37           |                   |                | 82.6          | SURCHARGED |                   |









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| Clifton Scannell Emerson Associates                                |                                 | Page 1  |
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### STORM SEWER DESIGN by the Modified Rational Method

#### Design Criteria for Network 2

Pipe Sizes STANDARD Manhole Sizes STANDARD

FSR Rainfall Model - Scotland and Ireland

|                                      |        |                                       |       |
|--------------------------------------|--------|---------------------------------------|-------|
| Return Period (years)                | 25     | PIMP (%)                              | 100   |
| M5-60 (mm)                           | 16.500 | Add Flow / Climate Change (%)         | 0     |
| Ratio R                              | 0.300  | Minimum Backdrop Height (m)           | 0.200 |
| Maximum Rainfall (mm/hr)             | 50     | Maximum Backdrop Height (m)           | 1.500 |
| Maximum Time of Concentration (mins) | 30     | Min Design Depth for Optimisation (m) | 1.200 |
| Foul Sewage (l/s/ha)                 | 0.000  | Min Vel for Auto Design only (m/s)    | 1.00  |
| Volumetric Runoff Coeff.             | 0.750  | Min Slope for Optimisation (1:X)      | 500   |

Designed with Level Soffits

#### Time Area Diagram for Network 2






| Time<br>(mins) | Area<br>(ha) | Time<br>(mins) | Area<br>(ha) | Time<br>(mins) | Area<br>(ha) | Time<br>(mins) | Area<br>(ha) |
|----------------|--------------|----------------|--------------|----------------|--------------|----------------|--------------|
| 0-4            | 1.175        | 4-8            | 3.082        | 8-12           | 0.741        | 12-16          | 0.008        |

Total Area Contributing (ha) = 5.006

Total Pipe Volume (m³) = 199.417

#### Network Design Table for Network 2

« - Indicates pipe capacity < flow

| PN    | Length<br>(m) | Fall<br>(m) | Slope<br>(1:X) | I.Area<br>(ha) | T.E.<br>(mins) | Base<br>Flow (l/s) | k<br>(mm) | HYD<br>SECT | DIA<br>(mm) | Section Type | Auto<br>Design  |
|-------|---------------|-------------|----------------|----------------|----------------|--------------------|-----------|-------------|-------------|--------------|---|
| 7.000 | 41.093        | 0.137       | 299.9          | 0.120          | 5.00           | 0.0                | 0.600     | o           | 300         | Pipe/Conduit |  |
| 7.001 | 43.607        | 0.145       | 300.7          | 0.186          | 0.00           | 0.0                | 0.600     | o           | 300         | Pipe/Conduit |  |
| 7.002 | 49.818        | 0.142       | 350.8          | 0.155          | 0.00           | 0.0                | 0.600     | o           | 375         | Pipe/Conduit |  |
| 7.003 | 31.126        | 0.089       | 349.7          | 0.103          | 0.00           | 0.0                | 0.600     | o           | 375         | Pipe/Conduit |  |
| 7.004 | 69.850        | 0.200       | 349.3          | 0.071          | 0.00           | 0.0                | 0.600     | o           | 375         | Pipe/Conduit |  |

#### Network Results Table

| PN    | Rain<br>(mm/hr) | T.C.<br>(mins) | US/IL<br>(m) | E I.Area<br>(ha) | E Base<br>Flow (l/s) | Foul<br>(l/s) | Add Flow<br>(l/s) | Vel<br>(m/s) | Cap<br>(l/s) | Flow<br>(l/s) |
|-------|-----------------|----------------|--------------|------------------|----------------------|---------------|-------------------|--------------|--------------|---------------|
| 7.000 | 50.00           | 5.76           | 77.889       | 0.120            | 0.0                  | 0.0           | 0.0               | 0.90         | 63.8         | 16.3          |
| 7.001 | 50.00           | 6.57           | 77.752       | 0.307            | 0.0                  | 0.0           | 0.0               | 0.90         | 63.7         | 41.5          |
| 7.002 | 50.00           | 7.43           | 77.532       | 0.462            | 0.0                  | 0.0           | 0.0               | 0.96         | 106.2        | 62.6          |
| 7.003 | 50.00           | 7.97           | 77.390       | 0.565            | 0.0                  | 0.0           | 0.0               | 0.96         | 106.4        | 76.5          |
| 7.004 | 50.00           | 9.18           | 77.301       | 0.636            | 0.0                  | 0.0           | 0.0               | 0.96         | 106.4        | 86.1          |








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|--|---------------------------------|
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Manhole Schedules for Network 2

| MH Name | MH CL (m) | MH Depth (m) | MH Connection | MH Diam., L*W (mm) | PN     | Pipe Out Invert Level (m) | Diameter (mm) | PN     | Pipes In Invert Level (m) | Diameter (mm) | Backdrop (mm) |
|---------|-----------|--------------|---------------|--------------------|--------|---------------------------|---------------|--------|---------------------------|---------------|---------------|
| S 7.0   | 79.389    | 1.500        | Open Manhole  | 1200               | 7.000  | 77.889                    | 300           |        |                           |               |               |
| S 7.1   | 79.374    | 1.622        | Open Manhole  | 1200               | 7.001  | 77.752                    | 300           | 7.000  | 77.752                    | 300           |               |
| S 7.2   | 79.362    | 1.830        | Open Manhole  | 1200               | 7.002  | 77.532                    | 375           | 7.001  | 77.607                    | 300           |               |
| S 7.3   | 79.349    | 1.959        | Open Manhole  | 1200               | 7.003  | 77.390                    | 375           | 7.002  | 77.390                    | 375           |               |
| S 7.4   | 79.146    | 1.845        | Open Manhole  | 1200               | 7.004  | 77.301                    | 375           | 7.003  | 77.301                    | 375           |               |
| S 8.0   | 79.333    | 1.643        | Open Manhole  | 1200               | 8.000  | 77.690                    | 300           |        |                           |               |               |
| S 8.1   | 79.331    | 1.776        | Open Manhole  | 1200               | 8.001  | 77.555                    | 300           | 8.000  | 77.555                    | 300           |               |
| S 8.2   | 79.331    | 1.998        | Open Manhole  | 1200               | 8.002  | 77.333                    | 375           | 8.001  | 77.408                    | 300           |               |
| S 8.3   | 79.332    | 2.139        | Open Manhole  | 1200               | 8.003  | 77.193                    | 375           | 8.002  | 77.193                    | 375           |               |
| S 7.5   | 79.142    | 2.266        | Open Manhole  | 1200               | 7.005  | 76.876                    | 600           | 7.004  | 77.101                    | 375           |               |
|         |           |              |               |                    |        |                           |               | 8.003  | 77.102                    | 375           |               |
| S 7.6   | 78.684    | 1.866        | Open Manhole  | 1200               | 7.006  | 76.818                    | 600           | 7.005  | 76.818                    | 600           |               |
| S 7.7   | 78.757    | 1.967        | Open Manhole  | 1200               | 7.007  | 76.790                    | 600           | 7.006  | 76.790                    | 600           |               |
| S 9.0   | 79.116    | 2.082        | Open Manhole  | 1200               | 9.000  | 77.034                    | 300           |        |                           |               |               |
| S 9.1   | 79.192    | 2.278        | Open Manhole  | 1200               | 9.001  | 76.914                    | 300           | 9.000  | 76.914                    | 300           |               |
| S 9.2   | 79.154    | 2.435        | Open Manhole  | 1350               | 9.002  | 76.719                    | 375           | 9.001  | 76.794                    | 300           |               |
| S 9.3   | 79.127    | 2.559        | Open Manhole  | 1350               | 9.003  | 76.568                    | 450           | 9.002  | 76.643                    | 375           |               |
| S 9.4   | 79.080    | 2.626        | Open Manhole  | 1350               | 9.004  | 76.454                    | 450           | 9.003  | 76.454                    | 450           |               |
| S 9.5   | 79.001    | 2.775        | Open Manhole  | 1500               | 9.005  | 76.226                    | 600           | 9.004  | 76.376                    | 450           |               |
| S 9.6   | 78.955    | 2.767        | Open Manhole  | 1200               | 9.006  | 76.188                    | 600           | 9.005  | 76.188                    | 600           |               |
| S 9.7   | 78.842    | 2.745        | Open Manhole  | 1350               | 9.007  | 76.097                    | 600           | 9.006  | 76.097                    | 600           |               |
| S 9.8   | 78.406    | 2.441        | Open Manhole  | 1500               | 9.008  | 75.965                    | 600           | 9.007  | 75.965                    | 600           |               |
| S 10.0  | 79.326    | 2.035        | Open Manhole  | 1200               | 10.000 | 77.291                    | 300           |        |                           |               |               |
| S 10.1  | 79.230    | 2.037        | Open Manhole  | 1200               | 10.001 | 77.193                    | 300           | 10.000 | 77.193                    | 300           |               |
| S 10.2  | 79.228    | 2.241        | Open Manhole  | 1200               | 10.002 | 76.987                    | 375           | 10.001 | 77.062                    | 300           |               |
| S 10.3  | 79.162    | 2.274        | Open Manhole  | 1200               | 10.003 | 76.888                    | 375           | 10.002 | 76.888                    | 375           |               |
| S 10.4  | 78.778    | 2.038        | Open Manhole  | 1200               | 10.004 | 76.740                    | 375           | 10.003 | 76.740                    | 375           |               |
| S 10.5  | 78.977    | 2.363        | Open Manhole  | 1200               | 10.005 | 76.614                    | 375           | 10.004 | 76.614                    | 375           |               |
| S 10.6  | 78.610    | 2.147        | Open Manhole  | 1200               | 10.006 | 76.463                    | 450           | 10.005 | 76.538                    | 375           |               |
| S 11.0  | 79.073    | 1.870        | Open Manhole  | 1200               | 11.000 | 77.203                    | 300           |        |                           |               |               |
| S 12.0  | 78.732    | 1.425        | Open Manhole  | 1200               | 12.000 | 77.307                    | 225           |        |                           |               |               |
| S 11.1  | 78.976    | 1.829        | Open Manhole  | 1200               | 11.001 | 77.147                    | 300           | 11.000 | 77.147                    | 300           |               |
|         |           |              |               |                    |        |                           |               | 12.000 | 77.222                    | 225           |               |
| S 11.2  | 78.643    | 1.724        | Open Manhole  | 1200               | 11.002 | 76.919                    | 300           | 11.001 | 76.919                    | 300           |               |
| S 11.3  | 78.553    | 1.696        | Open Manhole  | 1200               | 11.003 | 76.857                    | 300           | 11.002 | 76.857                    | 300           |               |
| S 10.7  | 78.671    | 2.250        | Open Manhole  | 1200               | 10.007 | 76.421                    | 450           | 10.006 | 76.421                    | 450           |               |
|         |           |              |               |                    |        |                           |               | 11.003 | 76.795                    | 300           |               |
| S 10.8  | 78.697    | 2.373        | Open Manhole  | 1200               | 10.008 | 76.324                    | 450           | 10.007 | 76.324                    | 450           |               |

|  |                                 |   |
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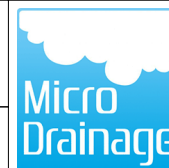
Manhole Schedules for Network 2

| MH Name | MH CL (m) | MH Depth (m) | MH Connection | MH Diam., L*W (mm) | PN     | Pipe Out Invert Level (m) | Diameter (mm) | PN     | Pipes In Invert Level (m) | Diameter (mm) | Backdrop (mm) |
|---------|-----------|--------------|---------------|--------------------|--------|---------------------------|---------------|--------|---------------------------|---------------|---------------|
| S 10.9  | 78.705    | 2.626        | Open Manhole  | 1200               | 10.009 | 76.079                    | 600           | 10.008 | 76.229                    | 450           |               |
| S 10.10 | 78.672    | 2.667        | Open Manhole  | 1200               | 10.010 | 76.005                    | 600           | 10.009 | 76.005                    | 600           |               |
| S 9.9   | 78.721    | 2.798        | Open Manhole  | 1200               | 9.009  | 75.925                    | 600           | 9.008  | 75.923                    | 600           |               |
|         |           |              |               |                    |        |                           |               | 10.010 | 75.925                    | 600           |               |
| S 13.0  | 79.000    | 3.014        | Open Manhole  | 2550               | 13.000 | 75.986                    | 450           |        |                           |               |               |
| S 7.8   | 77.600    | 1.800        | Open Manhole  | 1200               | 7.008  | 75.800                    | 300           | 7.007  | 76.760                    | 600           | 1260          |
|         |           |              |               |                    |        |                           |               | 9.009  | 75.900                    | 600           | 400           |
|         |           |              |               |                    |        |                           |               | 13.000 | 75.900                    | 450           | 250           |
| MH145   | 77.000    | 1.350        | Open Manhole  | 1800               |        | OUTFALL                   |               | 7.008  | 75.650                    | 300           |               |

| MH Name | Manhole Easting (m) | Manhole Northing (m) | Intersection Easting (m) | Intersection Northing (m) | Manhole Access | Layout (North)  |
|---------|---------------------|----------------------|--------------------------|---------------------------|----------------|---|
| S 7.0   | 711621.162          | 741339.449           | 711621.162               | 741339.449                | Required       |  |
| S 7.1   | 711621.162          | 741380.541           | 711621.162               | 741380.541                | Required       |  |
| S 7.2   | 711621.162          | 741424.149           | 711621.162               | 741424.149                | Required       |  |
| S 7.3   | 711621.162          | 741473.966           | 711621.162               | 741473.966                | Required       |  |
| S 7.4   | 711621.189          | 741505.093           | 711621.189               | 741505.093                | Required       |  |
| S 8.0   | 711551.339          | 741339.449           | 711551.339               | 741339.449                | Required       |  |
| S 8.1   | 711551.339          | 741380.036           | 711551.339               | 741380.036                | Required       |  |
| S 8.2   | 711551.339          | 741424.149           | 711551.339               | 741424.149                | Required       |  |
| S 8.3   | 711551.339          | 741473.298           | 711551.339               | 741473.298                | Required       |  |

Seefort Lodge  
Castledawson Avenue, Blackrock  
Dublin, Ireland

|                                |
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## Manhole Schedules for Network 2

| MH Name | Manhole Easting (m) | Manhole Northing (m) | Intersection Easting (m) | Intersection Northing (m) | Manhole Access | Layout (North) |
|---------|---------------------|----------------------|--------------------------|---------------------------|----------------|----------------|
| S 7.5   | 711551.339          | 741505.093           | 711551.339               | 741505.093                | Required       |                |
| S 7.6   | 711522.236          | 741505.093           | 711522.236               | 741505.093                | Required       |                |
| S 7.7   | 711522.236          | 741490.889           | 711522.236               | 741490.889                | Required       |                |
| S 9.0   | 711648.669          | 741325.241           | 711648.669               | 741325.241                | Required       |                |
| S 9.1   | 711648.669          | 741361.241           | 711648.669               | 741361.241                | Required       |                |
| S 9.2   | 711648.669          | 741397.241           | 711648.669               | 741397.241                | Required       |                |
| S 9.3   | 711648.669          | 741423.795           | 711648.669               | 741423.795                | Required       |                |
| S 9.4   | 711648.669          | 741469.241           | 711648.669               | 741469.241                | Required       |                |
| S 9.5   | 711648.669          | 741500.366           | 711648.669               | 741500.366                | Required       |                |
| S 9.6   | 711631.390          | 741507.644           | 711631.390               | 741507.644                | Required       |                |
| S 9.7   | 711585.803          | 741507.644           | 711585.803               | 741507.644                | Required       |                |
| S 9.8   | 711519.992          | 741507.644           | 711519.992               | 741507.644                | Required       |                |
| S 10.0  | 711758.694          | 741294.046           | 711758.694               | 741294.046                | Required       |                |
| S 10.1  | 711729.411          | 741294.046           | 711729.411               | 741294.046                | Required       |                |
| S 10.2  | 711690.208          | 741294.046           | 711690.208               | 741294.046                | Required       |                |





|  |                                 |   |
|--|---------------------------------|---|
| Clifton Scannell Emerson Associates                                |                                 | Page 10   |
| Seefort Lodge<br>Castledawson Avenue, Blackrock<br>Dublin, Ireland | Huntstown data centre facility  |  |
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PIPELINE SCHEDULES for Network 2

Upstream Manhole

| PN    | Hyd<br>Sect | Diam<br>(mm) | MH<br>Name | C.Level<br>(m) | I.Level<br>(m) | D.Depth<br>(m) | MH<br>Connection | MH DIAM., L*W<br>(mm) |
|-------|-------------|--------------|------------|----------------|----------------|----------------|------------------|-----------------------|
| 7.000 | o           | 300          | S 7.0      | 79.389         | 77.889         | 1.200          | Open Manhole     | 1200                  |
| 7.001 | o           | 300          | S 7.1      | 79.374         | 77.752         | 1.322          | Open Manhole     | 1200                  |
| 7.002 | o           | 375          | S 7.2      | 79.362         | 77.532         | 1.455          | Open Manhole     | 1200                  |
| 7.003 | o           | 375          | S 7.3      | 79.349         | 77.390         | 1.584          | Open Manhole     | 1200                  |
| 7.004 | o           | 375          | S 7.4      | 79.146         | 77.301         | 1.470          | Open Manhole     | 1200                  |
| 8.000 | o           | 300          | S 8.0      | 79.333         | 77.690         | 1.343          | Open Manhole     | 1200                  |
| 8.001 | o           | 300          | S 8.1      | 79.331         | 77.555         | 1.476          | Open Manhole     | 1200                  |
| 8.002 | o           | 375          | S 8.2      | 79.331         | 77.333         | 1.623          | Open Manhole     | 1200                  |
| 8.003 | o           | 375          | S 8.3      | 79.332         | 77.193         | 1.764          | Open Manhole     | 1200                  |
| 7.005 | o           | 600          | S 7.5      | 79.142         | 76.876         | 1.666          | Open Manhole     | 1200                  |
| 7.006 | o           | 600          | S 7.6      | 78.684         | 76.818         | 1.266          | Open Manhole     | 1200                  |
| 7.007 | o           | 600          | S 7.7      | 78.757         | 76.790         | 1.367          | Open Manhole     | 1200                  |
| 9.000 | o           | 300          | S 9.0      | 79.116         | 77.034         | 1.782          | Open Manhole     | 1200                  |
| 9.001 | o           | 300          | S 9.1      | 79.192         | 76.914         | 1.978          | Open Manhole     | 1200                  |
| 9.002 | o           | 375          | S 9.2      | 79.154         | 76.719         | 2.060          | Open Manhole     | 1350                  |
| 9.003 | o           | 450          | S 9.3      | 79.127         | 76.568         | 2.109          | Open Manhole     | 1350                  |
| 9.004 | o           | 450          | S 9.4      | 79.080         | 76.454         | 2.176          | Open Manhole     | 1350                  |
| 9.005 | o           | 600          | S 9.5      | 79.001         | 76.226         | 2.175          | Open Manhole     | 1500                  |

Downstream Manhole

| PN    | Length<br>(m) | Slope<br>(1:X) | MH<br>Name | C.Level<br>(m) | I.Level<br>(m) | D.Depth<br>(m) | MH<br>Connection | MH DIAM., L*W<br>(mm) |
|-------|---------------|----------------|------------|----------------|----------------|----------------|------------------|-----------------------|
| 7.000 | 41.093        | 299.9          | S 7.1      | 79.374         | 77.752         | 1.322          | Open Manhole     | 1200                  |
| 7.001 | 43.607        | 300.7          | S 7.2      | 79.362         | 77.607         | 1.455          | Open Manhole     | 1200                  |
| 7.002 | 49.818        | 350.8          | S 7.3      | 79.349         | 77.390         | 1.584          | Open Manhole     | 1200                  |
| 7.003 | 31.126        | 349.7          | S 7.4      | 79.146         | 77.301         | 1.470          | Open Manhole     | 1200                  |
| 7.004 | 69.850        | 349.3          | S 7.5      | 79.142         | 77.101         | 1.666          | Open Manhole     | 1200                  |
| 8.000 | 40.587        | 300.6          | S 8.1      | 79.331         | 77.555         | 1.476          | Open Manhole     | 1200                  |
| 8.001 | 44.112        | 300.1          | S 8.2      | 79.331         | 77.408         | 1.623          | Open Manhole     | 1200                  |
| 8.002 | 49.149        | 351.1          | S 8.3      | 79.332         | 77.193         | 1.764          | Open Manhole     | 1200                  |
| 8.003 | 31.795        | 349.4          | S 7.5      | 79.142         | 77.102         | 1.665          | Open Manhole     | 1200                  |
| 7.005 | 29.103        | 501.8          | S 7.6      | 78.684         | 76.818         | 1.266          | Open Manhole     | 1200                  |
| 7.006 | 14.203        | 507.3          | S 7.7      | 78.757         | 76.790         | 1.367          | Open Manhole     | 1200                  |
| 7.007 | 14.976        | 499.2          | S 7.8      | 77.600         | 76.760         | 0.240          | Open Manhole     | 1200                  |
| 9.000 | 36.000        | 300.0          | S 9.1      | 79.192         | 76.914         | 1.978          | Open Manhole     | 1200                  |
| 9.001 | 36.000        | 300.0          | S 9.2      | 79.154         | 76.794         | 2.060          | Open Manhole     | 1350                  |
| 9.002 | 26.554        | 349.4          | S 9.3      | 79.127         | 76.643         | 2.109          | Open Manhole     | 1350                  |
| 9.003 | 45.446        | 398.6          | S 9.4      | 79.080         | 76.454         | 2.176          | Open Manhole     | 1350                  |
| 9.004 | 31.125        | 399.0          | S 9.5      | 79.001         | 76.376         | 2.175          | Open Manhole     | 1500                  |
| 9.005 | 18.750        | 493.4          | S 9.6      | 78.955         | 76.188         | 2.167          | Open Manhole     | 1200                  |

|  |                                 |   |
|--|---------------------------------|---|
| Clifton Scannell Emerson Associates                                |                                 | Page 11   |
| Seefort Lodge<br>Castledawson Avenue, Blackrock<br>Dublin, Ireland | Huntstown data centre facility  |  |
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PIPELINE SCHEDULES for Network 2


Upstream Manhole

| PN     | Hyd<br>Sect | Diam<br>(mm) | MH<br>Name | C.Level<br>(m) | I.Level<br>(m) | D.Depth<br>(m) | MH<br>Connection | MH DIAM., L*W<br>(mm) |
|--------|-------------|--------------|------------|----------------|----------------|----------------|------------------|-----------------------|
| 9.006  | o           | 600          | S 9.6      | 78.955         | 76.188         | 2.167          | Open Manhole     | 1200                  |
| 9.007  | o           | 600          | S 9.7      | 78.842         | 76.097         | 2.145          | Open Manhole     | 1350                  |
| 9.008  | o           | 600          | S 9.8      | 78.406         | 75.965         | 1.841          | Open Manhole     | 1500                  |
|        |             |              |            |                |                |                |                  |                       |
| 10.000 | o           | 300          | S 10.0     | 79.326         | 77.291         | 1.735          | Open Manhole     | 1200                  |
| 10.001 | o           | 300          | S 10.1     | 79.230         | 77.193         | 1.737          | Open Manhole     | 1200                  |
| 10.002 | o           | 375          | S 10.2     | 79.228         | 76.987         | 1.866          | Open Manhole     | 1200                  |
| 10.003 | o           | 375          | S 10.3     | 79.162         | 76.888         | 1.899          | Open Manhole     | 1200                  |
| 10.004 | o           | 375          | S 10.4     | 78.778         | 76.740         | 1.663          | Open Manhole     | 1200                  |
| 10.005 | o           | 375          | S 10.5     | 78.977         | 76.614         | 1.988          | Open Manhole     | 1200                  |
| 10.006 | o           | 450          | S 10.6     | 78.610         | 76.463         | 1.697          | Open Manhole     | 1200                  |
|        |             |              |            |                |                |                |                  |                       |
| 11.000 | o           | 300          | S 11.0     | 79.073         | 77.203         | 1.570          | Open Manhole     | 1200                  |
|        |             |              |            |                |                |                |                  |                       |
| 12.000 | o           | 225          | S 12.0     | 78.732         | 77.307         | 1.200          | Open Manhole     | 1200                  |
|        |             |              |            |                |                |                |                  |                       |
| 11.001 | o           | 300          | S 11.1     | 78.976         | 77.147         | 1.529          | Open Manhole     | 1200                  |
| 11.002 | o           | 300          | S 11.2     | 78.643         | 76.919         | 1.424          | Open Manhole     | 1200                  |
| 11.003 | o           | 300          | S 11.3     | 78.553         | 76.857         | 1.396          | Open Manhole     | 1200                  |
|        |             |              |            |                |                |                |                  |                       |
| 10.007 | o           | 450          | S 10.7     | 78.671         | 76.421         | 1.800          | Open Manhole     | 1200                  |

Downstream Manhole

| PN     | Length<br>(m) | Slope<br>(1:X) | MH<br>Name | C.Level<br>(m) | I.Level<br>(m) | D.Depth<br>(m) | MH<br>Connection | MH DIAM., L*W<br>(mm) |
|--------|---------------|----------------|------------|----------------|----------------|----------------|------------------|-----------------------|
| 9.006  | 45.587        | 501.0          | S 9.7      | 78.842         | 76.097         | 2.145          | Open Manhole     | 1350                  |
| 9.007  | 65.811        | 498.6          | S 9.8      | 78.406         | 75.965         | 1.841          | Open Manhole     | 1500                  |
| 9.008  | 20.815        | 495.6          | S 9.9      | 78.721         | 75.923         | 2.198          | Open Manhole     | 1200                  |
|        |               |                |            |                |                |                |                  |                       |
| 10.000 | 29.283        | 298.8          | S 10.1     | 79.230         | 77.193         | 1.737          | Open Manhole     | 1200                  |
| 10.001 | 39.204        | 299.3          | S 10.2     | 79.228         | 77.062         | 1.866          | Open Manhole     | 1200                  |
| 10.002 | 39.682        | 400.8          | S 10.3     | 79.162         | 76.888         | 1.899          | Open Manhole     | 1200                  |
| 10.003 | 59.279        | 400.5          | S 10.4     | 78.778         | 76.740         | 1.663          | Open Manhole     | 1200                  |
| 10.004 | 50.432        | 400.3          | S 10.5     | 78.977         | 76.614         | 1.988          | Open Manhole     | 1200                  |
| 10.005 | 30.298        | 398.7          | S 10.6     | 78.610         | 76.538         | 1.697          | Open Manhole     | 1200                  |
| 10.006 | 16.896        | 402.3          | S 10.7     | 78.671         | 76.421         | 1.800          | Open Manhole     | 1200                  |
|        |               |                |            |                |                |                |                  |                       |
| 11.000 | 16.777        | 299.6          | S 11.1     | 78.976         | 77.147         | 1.529          | Open Manhole     | 1200                  |
|        |               |                |            |                |                |                |                  |                       |
| 12.000 | 17.025        | 200.3          | S 11.1     | 78.976         | 77.222         | 1.529          | Open Manhole     | 1200                  |
|        |               |                |            |                |                |                |                  |                       |
| 11.001 | 68.443        | 300.2          | S 11.2     | 78.643         | 76.919         | 1.424          | Open Manhole     | 1200                  |
| 11.002 | 18.602        | 300.0          | S 11.3     | 78.553         | 76.857         | 1.396          | Open Manhole     | 1200                  |
| 11.003 | 18.450        | 297.6          | S 10.7     | 78.671         | 76.795         | 1.576          | Open Manhole     | 1200                  |
|        |               |                |            |                |                |                |                  |                       |
| 10.007 | 38.835        | 400.4          | S 10.8     | 78.697         | 76.324         | 1.923          | Open Manhole     | 1200                  |



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| Seefort Lodge<br>Castledawson Avenue, Blackrock<br>Dublin, Ireland | Huntstown data centre facility  |  |
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PIPELINE SCHEDULES for Network 2

Upstream Manhole


| PN     | Hyd<br>Sect | Diam<br>(mm) | MH<br>Name | C.Level<br>(m) | I.Level<br>(m) | D.Depth<br>(m) | MH<br>Connection | MH DIAM., L*W<br>(mm) |
|--------|-------------|--------------|------------|----------------|----------------|----------------|------------------|-----------------------|
| 10.008 | o           | 450          | S 10.8     | 78.697         | 76.324         | 1.923          | Open Manhole     | 1200                  |
| 10.009 | o           | 600          | S 10.9     | 78.705         | 76.079         | 2.026          | Open Manhole     | 1200                  |
| 10.010 | o           | 600          | S 10.10    | 78.672         | 76.005         | 2.067          | Open Manhole     | 1200                  |
| 9.009  | o           | 600          | S 9.9      | 78.721         | 75.925         | 2.196          | Open Manhole     | 1200                  |
| 13.000 | o           | 450          | S 13.0     | 79.000         | 75.986         | 2.564          | Open Manhole     | 2550                  |
| 7.008  | o           | 300          | S 7.8      | 77.600         | 75.800         | 1.500          | Open Manhole     | 1200                  |


Downstream Manhole

| PN     | Length<br>(m) | Slope<br>(1:X) | MH<br>Name | C.Level<br>(m) | I.Level<br>(m) | D.Depth<br>(m) | MH<br>Connection | MH DIAM., L*W<br>(mm) |
|--------|---------------|----------------|------------|----------------|----------------|----------------|------------------|-----------------------|
| 10.008 | 38.104        | 401.1          | S 10.9     | 78.705         | 76.229         | 2.026          | Open Manhole     | 1200                  |
| 10.009 | 37.063        | 500.9          | S 10.10    | 78.672         | 76.005         | 2.067          | Open Manhole     | 1200                  |
| 10.010 | 39.876        | 498.5          | S 9.9      | 78.721         | 75.925         | 2.196          | Open Manhole     | 1200                  |
| 9.009  | 12.624        | 505.0          | S 7.8      | 77.600         | 75.900         | 1.100          | Open Manhole     | 1200                  |
| 13.000 | 34.249        | 398.2          | S 7.8      | 77.600         | 75.900         | 1.250          | Open Manhole     | 1200                  |
| 7.008  | 39.382        | 262.5          | MH145      | 77.000         | 75.650         | 1.050          | Open Manhole     | 1800                  |





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|--|---------------------------------|---|
| Clifton Scannell Emerson Associates  |                                 | Page 15   |
| Seefort Lodge<br>Castledawson Avenue, Blackrock<br>Dublin, Ireland   | Huntstown data centre facility  |  |
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| Innovyze Network 2020.1.3  |                                 |   |
| <p align="center"><u>Simulation Criteria for Network 2</u></p> <p> Volumetric Runoff Coeff 0.750    Additional Flow - % of Total Flow 0.000<br/> Areal Reduction Factor 1.000    MADD Factor * 10m³/ha Storage 2.000<br/> Hot Start (mins) 0    Inlet Coefficient 0.800<br/> Hot Start Level (mm) 0    Flow per Person per Day (l/per/day) 0.000<br/> Manhole Headloss Coeff (Global) 0.500    Run Time (mins) 60<br/> Foul Sewage per hectare (l/s) 0.000    Output Interval (mins) 1 </p> <p> Number of Input Hydrographs 0    Number of Storage Structures 1<br/> Number of Online Controls 1    Number of Time/Area Diagrams 0<br/> Number of Offline Controls 0    Number of Real Time Controls 0 </p> <p align="center"><u>Synthetic Rainfall Details</u></p> <p> Rainfall Model    FSR    Profile Type Summer<br/> Return Period (years) 25    Cv (Summer) 0.750<br/> Region Scotland and Ireland    Cv (Winter) 0.840<br/> M5-60 (mm) 16.500    Storm Duration (mins) 30<br/> Ratio R 0.300 </p> |                                 |   |
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Online Controls for Network 2

Hydro-Brake® Optimum Manhole: S 7.8, DS/PN: 7.008, Volume (m³): 14.3


|                                   |                            |
|-----------------------------------|----------------------------|
| Unit Reference                    | MD-SHE-0173-1600-1500-1600 |
| Design Head (m)                   | 1.500                      |
| Design Flow (l/s)                 | 16.0                       |
| Flush-Flo™                        | Calculated                 |
| Objective                         | Minimise upstream storage  |
| Application                       | Surface                    |
| Sump Available                    | Yes                        |
| Diameter (mm)                     | 173                        |
| Invert Level (m)                  | 75.800                     |
| Minimum Outlet Pipe Diameter (mm) | 225                        |
| Suggested Manhole Diameter (mm)   | 1500                       |

| Control Points            | Head (m) | Flow (l/s) |
|---------------------------|----------|------------|
| Design Point (Calculated) | 1.500    | 16.0       |
| Flush-Flo™                | 0.442    | 16.0       |
| Kick-Flo®                 | 0.961    | 13.0       |
| Mean Flow over Head Range | -        | 13.9       |

The hydrological calculations have been based on the Head/Discharge relationship for the Hydro-Brake® Optimum as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated


| Depth (m) | Flow (l/s) | Depth (m) | Flow (l/s) | Depth (m) | Flow (l/s) | Depth (m) | Flow (l/s) |
|-----------|------------|-----------|------------|-----------|------------|-----------|------------|
| 0.100     | 6.1        | 1.200     | 14.4       | 3.000     | 22.3       | 7.000     | 33.5       |
| 0.200     | 14.4       | 1.400     | 15.5       | 3.500     | 24.0       | 7.500     | 34.6       |
| 0.300     | 15.6       | 1.600     | 16.5       | 4.000     | 25.6       | 8.000     | 35.7       |
| 0.400     | 16.0       | 1.800     | 17.4       | 4.500     | 27.0       | 8.500     | 36.7       |
| 0.500     | 15.9       | 2.000     | 18.3       | 5.000     | 28.4       | 9.000     | 37.8       |
| 0.600     | 15.7       | 2.200     | 19.2       | 5.500     | 29.8       | 9.500     | 38.8       |
| 0.800     | 14.9       | 2.400     | 20.0       | 6.000     | 31.1       |           |            |
| 1.000     | 13.2       | 2.600     | 20.8       | 6.500     | 32.3       |           |            |



| Clifton Scannell Emerson Associates   |                                 | Page 18   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
|---|---------------------------------|---|----|---------------|-------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--------|--------|-------|--------|--------|-------|--------|--------|-------|--------|--------|-------|--------|--------|-------|--------|--------|-------|--------|--------|-------|--------|--------|-------|--------|--------|-------|--------|--------|-------|--------|--------|-------|--------|--------|-------|--------|--------|-------|--------|--------|-------|--------|--------|-------|--------|---------|-------|-------|-------|-------|--------|--------|-------|-------|-------|-------|
| Seefort Lodge<br>Castledawson Avenue, Blackrock<br>Dublin, Ireland  | Huntstown data centre facility  |  |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| Date 06/05/2021<br>File DUB040 SW Network-2.mdx   | Designed by ZS<br>Checked by CD |   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| Innovyze  | Network 2020.1.3                |   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| <p style="text-align: center;"><u>Manhole Headloss for Network 2</u></p> <table><thead><tr><th>PN</th><th>US/MH<br/>Name</th><th>US/MH<br/>Headloss</th></tr></thead><tbody><tr><td>7.000</td><td>S 7.0</td><td>0.500</td></tr><tr><td>7.001</td><td>S 7.1</td><td>0.500</td></tr><tr><td>7.002</td><td>S 7.2</td><td>0.500</td></tr><tr><td>7.003</td><td>S 7.3</td><td>0.500</td></tr><tr><td>7.004</td><td>S 7.4</td><td>0.500</td></tr><tr><td>8.000</td><td>S 8.0</td><td>0.500</td></tr><tr><td>8.001</td><td>S 8.1</td><td>0.500</td></tr><tr><td>8.002</td><td>S 8.2</td><td>0.500</td></tr><tr><td>8.003</td><td>S 8.3</td><td>0.500</td></tr><tr><td>7.005</td><td>S 7.5</td><td>0.500</td></tr><tr><td>7.006</td><td>S 7.6</td><td>0.500</td></tr><tr><td>7.007</td><td>S 7.7</td><td>0.500</td></tr><tr><td>9.000</td><td>S 9.0</td><td>0.500</td></tr><tr><td>9.001</td><td>S 9.1</td><td>0.500</td></tr><tr><td>9.002</td><td>S 9.2</td><td>0.500</td></tr><tr><td>9.003</td><td>S 9.3</td><td>0.500</td></tr><tr><td>9.004</td><td>S 9.4</td><td>0.500</td></tr><tr><td>9.005</td><td>S 9.5</td><td>0.500</td></tr><tr><td>9.006</td><td>S 9.6</td><td>0.500</td></tr><tr><td>9.007</td><td>S 9.7</td><td>0.500</td></tr><tr><td>9.008</td><td>S 9.8</td><td>0.500</td></tr><tr><td>10.000</td><td>S 10.0</td><td>0.500</td></tr><tr><td>10.001</td><td>S 10.1</td><td>0.500</td></tr><tr><td>10.002</td><td>S 10.2</td><td>0.500</td></tr><tr><td>10.003</td><td>S 10.3</td><td>0.500</td></tr><tr><td>10.004</td><td>S 10.4</td><td>0.500</td></tr><tr><td>10.005</td><td>S 10.5</td><td>0.500</td></tr><tr><td>10.006</td><td>S 10.6</td><td>0.500</td></tr><tr><td>11.000</td><td>S 11.0</td><td>0.500</td></tr><tr><td>12.000</td><td>S 12.0</td><td>0.500</td></tr><tr><td>11.001</td><td>S 11.1</td><td>0.500</td></tr><tr><td>11.002</td><td>S 11.2</td><td>0.500</td></tr><tr><td>11.003</td><td>S 11.3</td><td>0.500</td></tr><tr><td>10.007</td><td>S 10.7</td><td>0.500</td></tr><tr><td>10.008</td><td>S 10.8</td><td>0.500</td></tr><tr><td>10.009</td><td>S 10.9</td><td>0.500</td></tr><tr><td>10.010</td><td>S 10.10</td><td>0.500</td></tr><tr><td>9.009</td><td>S 9.9</td><td>0.500</td></tr><tr><td>13.000</td><td>S 13.0</td><td>0.500</td></tr><tr><td>7.008</td><td>S 7.8</td><td>0.500</td></tr></tbody></table> |                                 |   | PN | US/MH<br>Name | US/MH<br>Headloss | 7.000 | S 7.0 | 0.500 | 7.001 | S 7.1 | 0.500 | 7.002 | S 7.2 | 0.500 | 7.003 | S 7.3 | 0.500 | 7.004 | S 7.4 | 0.500 | 8.000 | S 8.0 | 0.500 | 8.001 | S 8.1 | 0.500 | 8.002 | S 8.2 | 0.500 | 8.003 | S 8.3 | 0.500 | 7.005 | S 7.5 | 0.500 | 7.006 | S 7.6 | 0.500 | 7.007 | S 7.7 | 0.500 | 9.000 | S 9.0 | 0.500 | 9.001 | S 9.1 | 0.500 | 9.002 | S 9.2 | 0.500 | 9.003 | S 9.3 | 0.500 | 9.004 | S 9.4 | 0.500 | 9.005 | S 9.5 | 0.500 | 9.006 | S 9.6 | 0.500 | 9.007 | S 9.7 | 0.500 | 9.008 | S 9.8 | 0.500 | 10.000 | S 10.0 | 0.500 | 10.001 | S 10.1 | 0.500 | 10.002 | S 10.2 | 0.500 | 10.003 | S 10.3 | 0.500 | 10.004 | S 10.4 | 0.500 | 10.005 | S 10.5 | 0.500 | 10.006 | S 10.6 | 0.500 | 11.000 | S 11.0 | 0.500 | 12.000 | S 12.0 | 0.500 | 11.001 | S 11.1 | 0.500 | 11.002 | S 11.2 | 0.500 | 11.003 | S 11.3 | 0.500 | 10.007 | S 10.7 | 0.500 | 10.008 | S 10.8 | 0.500 | 10.009 | S 10.9 | 0.500 | 10.010 | S 10.10 | 0.500 | 9.009 | S 9.9 | 0.500 | 13.000 | S 13.0 | 0.500 | 7.008 | S 7.8 | 0.500 |
| PN  | US/MH<br>Name                   | US/MH<br>Headloss   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 7.000   | S 7.0                           | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 7.001   | S 7.1                           | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 7.002   | S 7.2                           | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 7.003   | S 7.3                           | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 7.004   | S 7.4                           | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 8.000   | S 8.0                           | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 8.001   | S 8.1                           | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 8.002   | S 8.2                           | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 8.003   | S 8.3                           | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 7.005   | S 7.5                           | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 7.006   | S 7.6                           | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 7.007   | S 7.7                           | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 9.000   | S 9.0                           | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 9.001   | S 9.1                           | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 9.002   | S 9.2                           | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 9.003   | S 9.3                           | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 9.004   | S 9.4                           | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 9.005   | S 9.5                           | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 9.006   | S 9.6                           | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 9.007   | S 9.7                           | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 9.008   | S 9.8                           | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 10.000  | S 10.0                          | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 10.001  | S 10.1                          | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 10.002  | S 10.2                          | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 10.003  | S 10.3                          | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 10.004  | S 10.4                          | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 10.005  | S 10.5                          | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 10.006  | S 10.6                          | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 11.000  | S 11.0                          | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 12.000  | S 12.0                          | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 11.001  | S 11.1                          | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 11.002  | S 11.2                          | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 11.003  | S 11.3                          | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 10.007  | S 10.7                          | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 10.008  | S 10.8                          | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 10.009  | S 10.9                          | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 10.010  | S 10.10                         | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 9.009   | S 9.9                           | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 13.000  | S 13.0                          | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| 7.008   | S 7.8                           | 0.500   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |
| ©1982-2020 Innovyze   |                                 |   |    |               |                   |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |        |       |        |         |       |       |       |       |        |        |       |       |       |       |






|  |                                 |   |
|--|---------------------------------|---|
| Clifton Scannell Emerson Associates                                |                                 | Page 20   |
| Seefort Lodge<br>Castledawson Avenue, Blackrock<br>Dublin, Ireland | Huntstown data centre facility  |  |
| Date 06/05/2021<br>File DUB040 SW Network-2.mdx                    | Designed by ZS<br>Checked by CD |   |
| Innovyze   | Network 2020.1.3                |   |

1 year Return Period Summary of Critical Results by Maximum Level (Rank 1)  
for Network 2

| PN    | US/MH<br>Name | Surcharged Flooded |                | Flow /<br>Cap. | Overflow<br>(l/s) | Half Drain<br>Time<br>(mins) | Pipe<br>Flow<br>(l/s) | Status | Level<br>Exceeded |
|-------|---------------|--------------------|----------------|----------------|-------------------|------------------------------|-----------------------|--------|-------------------|
|       |               | Depth<br>(m)       | Volume<br>(m³) |                |                   |                              |                       |        |                   |
| 7.000 | S 7.0         | -0.196             | 0.000          | 0.25           |                   |                              | 14.8                  | OK     |                   |
| 7.001 | S 7.1         | -0.137             | 0.000          | 0.56           |                   |                              | 33.3                  | OK     |                   |
| 7.002 | S 7.2         | -0.188             | 0.000          | 0.48           |                   |                              | 47.0                  | OK     |                   |
| 7.003 | S 7.3         | -0.168             | 0.000          | 0.58           |                   |                              | 54.9                  | OK     |                   |
| 7.004 | S 7.4         | -0.165             | 0.000          | 0.58           |                   |                              | 58.4                  | OK     |                   |
| 8.000 | S 8.0         | -0.196             | 0.000          | 0.25           |                   |                              | 14.9                  | OK     |                   |
| 8.001 | S 8.1         | -0.137             | 0.000          | 0.56           |                   |                              | 33.3                  | OK     |                   |
| 8.002 | S 8.2         | -0.188             | 0.000          | 0.48           |                   |                              | 47.1                  | OK     |                   |
| 8.003 | S 8.3         | -0.168             | 0.000          | 0.58           |                   |                              | 55.0                  | OK     |                   |
| 7.005 | S 7.5         | -0.242             | 0.000          | 0.45           |                   |                              | 112.6                 | OK     |                   |
| 7.006 | S 7.6         | -0.228             | 0.000          | 0.68           |                   |                              | 110.5                 | OK     |                   |
| 7.007 | S 7.7         | -0.244             | 0.000          | 0.66           |                   |                              | 109.9                 | OK     |                   |
| 9.000 | S 9.0         | -0.149             | 0.000          | 0.46           |                   |                              | 27.0                  | OK     |                   |
| 9.001 | S 9.1         | -0.084             | 0.000          | 0.84           |                   |                              | 49.7                  | OK     |                   |
| 9.002 | S 9.2         | -0.134             | 0.000          | 0.73           |                   |                              | 67.6                  | OK     |                   |
| 9.003 | S 9.3         | -0.186             | 0.000          | 0.60           |                   |                              | 86.3                  | OK     |                   |
| 9.004 | S 9.4         | -0.157             | 0.000          | 0.75           |                   |                              | 104.0                 | OK     |                   |
| 9.005 | S 9.5         | -0.264             | 0.000          | 0.52           |                   |                              | 104.4                 | OK     |                   |
| 9.006 | S 9.6         | -0.260             | 0.000          | 0.40           |                   |                              | 104.8                 | OK     |                   |
| 9.007 | S 9.7         | -0.200             | 0.000          | 0.36           |                   |                              | 100.6                 | OK     |                   |
| 9.008 | S 9.8         | -0.093             | 0.000          | 0.43           |                   |                              | 92.0                  | OK     |                   |



|   |  |   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
|---|--|---|-------|-------|----|------|----------|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|---------|--|-------|-------|--|--------|--------|--|-------|-------|--|--|
| Clifton Scannell Emerson Associates   |  | Page 22   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| Seefort Lodge<br>Castledawson Avenue, Blackrock<br>Dublin, Ireland  | Huntstown data centre facility   |  |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| Date 06/05/2021<br>File DUB040 SW Network-2.mdx   | Designed by ZS<br>Checked by CD  |   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| Innovyze  | Network 2020.1.3   |   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| <u>1 year Return Period Summary of Critical Results by Maximum Level (Rank 1)</u><br><u>for Network 2</u> |  |   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
|   | <table><tr><td></td><td>US/MH</td><td>Level</td></tr><tr><td>PN</td><td>Name</td><td>Exceeded</td></tr><tr><td>10.000</td><td>S 10.0</td><td></td></tr><tr><td>10.001</td><td>S 10.1</td><td></td></tr><tr><td>10.002</td><td>S 10.2</td><td></td></tr><tr><td>10.003</td><td>S 10.3</td><td></td></tr><tr><td>10.004</td><td>S 10.4</td><td></td></tr><tr><td>10.005</td><td>S 10.5</td><td></td></tr><tr><td>10.006</td><td>S 10.6</td><td></td></tr><tr><td>11.000</td><td>S 11.0</td><td></td></tr><tr><td>12.000</td><td>S 12.0</td><td></td></tr><tr><td>11.001</td><td>S 11.1</td><td></td></tr><tr><td>11.002</td><td>S 11.2</td><td></td></tr><tr><td>11.003</td><td>S 11.3</td><td></td></tr><tr><td>10.007</td><td>S 10.7</td><td></td></tr><tr><td>10.008</td><td>S 10.8</td><td></td></tr><tr><td>10.009</td><td>S 10.9</td><td></td></tr><tr><td>10.010</td><td>S 10.10</td><td></td></tr><tr><td>9.009</td><td>S 9.9</td><td></td></tr><tr><td>13.000</td><td>S 13.0</td><td></td></tr><tr><td>7.008</td><td>S 7.8</td><td></td></tr></table> |   | US/MH | Level | PN | Name | Exceeded | 10.000 | S 10.0 |  | 10.001 | S 10.1 |  | 10.002 | S 10.2 |  | 10.003 | S 10.3 |  | 10.004 | S 10.4 |  | 10.005 | S 10.5 |  | 10.006 | S 10.6 |  | 11.000 | S 11.0 |  | 12.000 | S 12.0 |  | 11.001 | S 11.1 |  | 11.002 | S 11.2 |  | 11.003 | S 11.3 |  | 10.007 | S 10.7 |  | 10.008 | S 10.8 |  | 10.009 | S 10.9 |  | 10.010 | S 10.10 |  | 9.009 | S 9.9 |  | 13.000 | S 13.0 |  | 7.008 | S 7.8 |  |  |
|   | US/MH  | Level   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| PN  | Name   | Exceeded  |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.000  | S 10.0   |   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.001  | S 10.1   |   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.002  | S 10.2   |   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.003  | S 10.3   |   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.004  | S 10.4   |   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.005  | S 10.5   |   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.006  | S 10.6   |   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 11.000  | S 11.0   |   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 12.000  | S 12.0   |   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 11.001  | S 11.1   |   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 11.002  | S 11.2   |   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 11.003  | S 11.3   |   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.007  | S 10.7   |   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.008  | S 10.8   |   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.009  | S 10.9   |   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.010  | S 10.10  |   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 9.009   | S 9.9  |   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 13.000  | S 13.0   |   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 7.008   | S 7.8  |   |       |       |    |      |          |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
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Clifton Scannell Emerson Associates

Page 23

Seefort Lodge  
Castledawson Avenue, Blackrock  
Dublin, Ireland

Date 06/05/2021  
File DUB040 SW Network-2.mdx

Innovyze

Huntstown data centre facility

Designed by ZS  
Checked by CD

Network 2020.1.3

Micro  
Drainage

30 year Return Period Summary of Critical Results by Maximum Level (Rank 1)  
for Network 2

Simulation Criteria

Areal Reduction Factor 1.000

Additional Flow - % of Total Flow 0.000

Hot Start (mins) 0

MADD Factor \* 10m³/ha Storage 2.000

Hot Start Level (mm) 0

Inlet Coefficient 0.800

Manhole Headloss Coeff (Global) 0.500

Flow per Person per Day (l/per/day) 0.000

Foul Sewage per hectare (l/s) 0.000

Number of Input Hydrographs 0

Number of Storage Structures 1

Number of Online Controls 1

Number of Time/Area Diagrams 0

Number of Offline Controls 0

Number of Real Time Controls 0

Synthetic Rainfall Details

Rainfall Model

FSR

Ratio R 0.300

Region Scotland and Ireland Cv (Summer) 0.750

M5-60 (mm)

16.500 Cv (Winter) 0.840

Margin for Flood Risk Warning (mm) 300.0

DVD Status OFF

Analysis Timestep

Fine Inertia Status OFF

DTS Status

ON

Profile(s)

Summer and Winter

Duration(s) (mins) 15, 30, 60, 120, 240, 360, 480, 960, 1440

Return Period(s) (years) 1, 30, 100


Climate Change (%) 10, 10, 10

| PN    | US/MH Name | Storm       | Return Period | Climate Change | First (X) Surchage | First (Y) Flood | First (Z) Overflow | Overflow Act. | Water Level (m) |
|-------|------------|-------------|---------------|----------------|--------------------|-----------------|--------------------|---------------|-----------------|
| 7.000 | S 7.0      | 15 Winter   | 30            | +10%           | 30/15 Summer       |                 |                    |               | 78.257          |
| 7.001 | S 7.1      | 15 Winter   | 30            | +10%           | 30/15 Summer       |                 |                    |               | 78.218          |
| 7.002 | S 7.2      | 15 Winter   | 30            | +10%           | 30/15 Summer       |                 |                    |               | 78.030          |
| 7.003 | S 7.3      | 15 Winter   | 30            | +10%           | 30/15 Summer       |                 |                    |               | 77.896          |
| 7.004 | S 7.4      | 15 Winter   | 30            | +10%           | 30/15 Summer       |                 |                    |               | 77.770          |
| 8.000 | S 8.0      | 15 Winter   | 30            | +10%           | 30/15 Summer       |                 |                    |               | 78.055          |
| 8.001 | S 8.1      | 15 Winter   | 30            | +10%           | 30/15 Summer       |                 |                    |               | 78.014          |
| 8.002 | S 8.2      | 15 Winter   | 30            | +10%           | 30/15 Summer       |                 |                    |               | 77.782          |
| 8.003 | S 8.3      | 15 Winter   | 30            | +10%           | 30/15 Summer       |                 |                    |               | 77.615          |
| 7.005 | S 7.5      | 15 Winter   | 30            | +10%           | 30/15 Winter       |                 |                    |               | 77.481          |
| 7.006 | S 7.6      | 15 Winter   | 30            | +10%           | 30/15 Summer       |                 |                    |               | 77.430          |
| 7.007 | S 7.7      | 30 Summer   | 30            | +10%           | 100/15 Winter      |                 |                    |               | 77.390          |
| 9.000 | S 9.0      | 15 Winter   | 30            | +10%           | 30/15 Summer       |                 |                    |               | 77.999          |
| 9.001 | S 9.1      | 15 Winter   | 30            | +10%           | 30/15 Summer       |                 |                    |               | 77.900          |
| 9.002 | S 9.2      | 15 Winter   | 30            | +10%           | 30/15 Summer       |                 |                    |               | 77.510          |
| 9.003 | S 9.3      | 15 Winter   | 30            | +10%           | 30/15 Summer       |                 |                    |               | 77.308          |
| 9.004 | S 9.4      | 15 Winter   | 30            | +10%           | 30/15 Summer       |                 |                    |               | 77.083          |
| 9.005 | S 9.5      | 960 Winter  | 30            | +10%           | 30/15 Winter       |                 |                    |               | 77.067          |
| 9.006 | S 9.6      | 960 Winter  | 30            | +10%           | 30/15 Winter       |                 |                    |               | 77.066          |
| 9.007 | S 9.7      | 960 Winter  | 30            | +10%           | 30/15 Summer       |                 |                    |               | 77.065          |
| 9.008 | S 9.8      | 1440 Winter | 30            | +10%           | 30/15 Summer       |                 |                    |               | 77.064          |

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|  |   |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
|--|---|---|--------------|--------------|-----------|-------------|-----------------|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|---------|--|-------|-------|--|--------|--------|--|-------|-------|--|--|
| Clifton Scannell Emerson Associates  |   | Page 26   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| Seefort Lodge<br>Castledawson Avenue, Blackrock<br>Dublin, Ireland   | Huntstown data centre facility  |  |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| Date 06/05/2021<br>File DUB040 SW Network-2.mdx  | Designed by ZS<br>Checked by CD   |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| Innovyze   | Network 2020.1.3  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| <u>30 year Return Period Summary of Critical Results by Maximum Level (Rank 1)</u><br><u>for Network 2</u> |   |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
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|  | <b>US/MH</b>  | <b>Level</b>  |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| <b>PN</b>  | <b>Name</b>   | <b>Exceeded</b>   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.000   | S 10.0  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.001   | S 10.1  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.002   | S 10.2  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.003   | S 10.3  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.004   | S 10.4  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.005   | S 10.5  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.006   | S 10.6  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 11.000   | S 11.0  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 12.000   | S 12.0  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 11.001   | S 11.1  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 11.002   | S 11.2  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 11.003   | S 11.3  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.007   | S 10.7  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.008   | S 10.8  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.009   | S 10.9  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.010   | S 10.10   |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 9.009  | S 9.9   |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 13.000   | S 13.0  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 7.008  | S 7.8   |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
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Clifton Scannell Emerson Associates

Page 27

Seefort Lodge  
Castledawson Avenue, Blackrock  
Dublin, Ireland

Date 06/05/2021  
File DUB040 SW Network-2.mdx

Huntstown data centre facility

Designed by ZS  
Checked by CD

Micro Drainage

Innovyze

Network 2020.1.3

100 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for Network 2

Simulation Criteria

Areal Reduction Factor 1.000

Additional Flow - % of Total Flow 0.000

Hot Start (mins) 0

MADD Factor \* 10m³/ha Storage 2.000

Hot Start Level (mm) 0

Inlet Coeffiecient 0.800

Manhole Headloss Coeff (Global) 0.500

Flow per Person per Day (l/per/day) 0.000

Foul Sewage per hectare (l/s) 0.000

Number of Input Hydrographs 0

Number of Storage Structures 1

Number of Online Controls 1

Number of Time/Area Diagrams 0

Number of Offline Controls 0

Number of Real Time Controls 0

Synthetic Rainfall Details

Rainfall Model

FSR

Ratio R 0.300

Region Scotland and Ireland Cv (Summer) 0.750

M5-60 (mm)

16.500 Cv (Winter) 0.840

Margin for Flood Risk Warning (mm) 300.0

DVD Status OFF

Analysis Timestep

Fine Inertia Status OFF

DTS Status

ON

Profile(s)

Summer and Winter

Duration(s) (mins) 15, 30, 60, 120, 240, 360, 480, 960, 1440

Return Period(s) (years)

1, 30, 100

Climate Change (%)

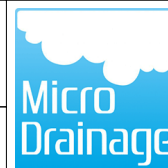
10, 10, 10

|       | US/MH |             | Return | Climate | First (X)     | First (Y) | First (Z) | Overflow | Water  |
|-------|-------|-------------|--------|---------|---------------|-----------|-----------|----------|--------|
| PN    | Name  | Storm       | Period | Change  | Surcharge     | Flood     | Overflow  | Act.     | Level  |
| 7.000 | S 7.0 | 15 Winter   | 100    | +10%    | 30/15 Summer  |           |           |          | 78.801 |
| 7.001 | S 7.1 | 15 Winter   | 100    | +10%    | 30/15 Summer  |           |           |          | 78.755 |
| 7.002 | S 7.2 | 15 Winter   | 100    | +10%    | 30/15 Summer  |           |           |          | 78.476 |
| 7.003 | S 7.3 | 15 Winter   | 100    | +10%    | 30/15 Summer  |           |           |          | 78.268 |
| 7.004 | S 7.4 | 15 Winter   | 100    | +10%    | 30/15 Summer  |           |           |          | 78.058 |
| 8.000 | S 8.0 | 15 Winter   | 100    | +10%    | 30/15 Summer  |           |           |          | 78.467 |
| 8.001 | S 8.1 | 15 Winter   | 100    | +10%    | 30/15 Summer  |           |           |          | 78.414 |
| 8.002 | S 8.2 | 15 Winter   | 100    | +10%    | 30/15 Summer  |           |           |          | 78.057 |
| 8.003 | S 8.3 | 15 Winter   | 100    | +10%    | 30/15 Summer  |           |           |          | 77.788 |
| 7.005 | S 7.5 | 15 Winter   | 100    | +10%    | 30/15 Winter  |           |           |          | 77.545 |
| 7.006 | S 7.6 | 15 Winter   | 100    | +10%    | 30/15 Summer  |           |           |          | 77.453 |
| 7.007 | S 7.7 | 15 Winter   | 100    | +10%    | 100/15 Winter |           |           |          | 77.392 |
| 9.000 | S 9.0 | 15 Winter   | 100    | +10%    | 30/15 Summer  |           |           |          | 78.720 |
| 9.001 | S 9.1 | 15 Winter   | 100    | +10%    | 30/15 Summer  |           |           |          | 78.570 |
| 9.002 | S 9.2 | 15 Winter   | 100    | +10%    | 30/15 Summer  |           |           |          | 78.026 |
| 9.003 | S 9.3 | 15 Winter   | 100    | +10%    | 30/15 Summer  |           |           |          | 77.776 |
| 9.004 | S 9.4 | 15 Winter   | 100    | +10%    | 30/15 Summer  |           |           |          | 77.511 |
| 9.005 | S 9.5 | 1440 Winter | 100    | +10%    | 30/15 Winter  |           |           |          | 77.396 |
| 9.006 | S 9.6 | 1440 Winter | 100    | +10%    | 30/15 Winter  |           |           |          | 77.395 |
| 9.007 | S 9.7 | 1440 Winter | 100    | +10%    | 30/15 Summer  |           |           |          | 77.394 |
| 9.008 | S 9.8 | 1440 Winter | 100    | +10%    | 30/15 Summer  |           |           |          | 77.392 |

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|                                |
|--------------------------------|
| Huntstown data centre facility |
|--------------------------------|



Designed by ZS


Checked by CD

Network 2020.1.3

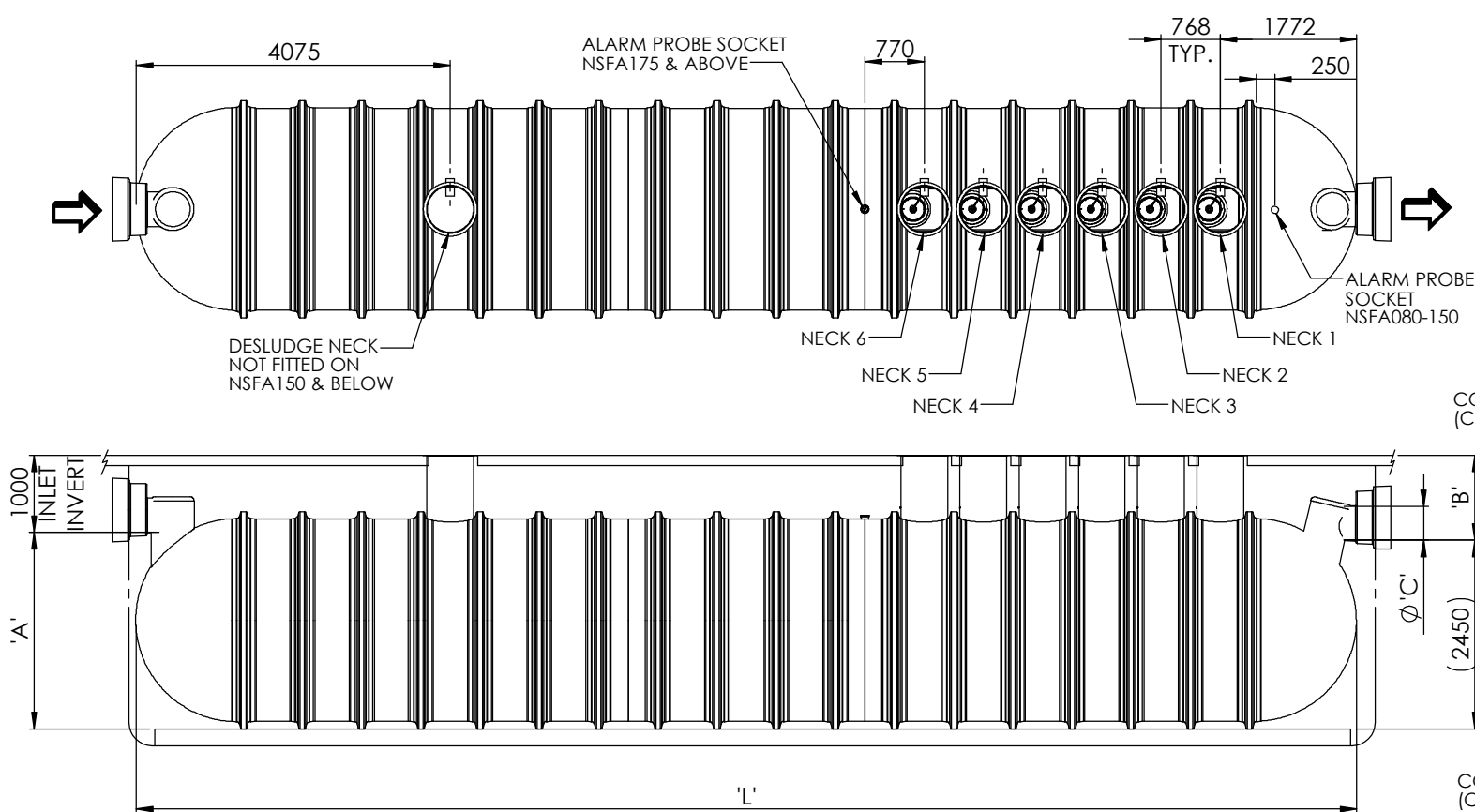
1) for Network 2

| PN    | US/MH<br>Name | Surcharged   | Flooded        | Flow /<br>Cap. | Overflow<br>(l/s) | Half Drain     | Pipe          | Status     | Level    |
|-------|---------------|--------------|----------------|----------------|-------------------|----------------|---------------|------------|----------|
|       |               | Depth<br>(m) | Volume<br>(m³) |                |                   | Time<br>(mins) | Flow<br>(l/s) |            | Exceeded |
| 7.000 | S 7.0         | 0.612        | 0.000          | 0.59           |                   |                | 35.0          | SURCHARGED |          |
| 7.001 | S 7.1         | 0.703        | 0.000          | 1.38           |                   |                | 82.4          | SURCHARGED |          |
| 7.002 | S 7.2         | 0.569        | 0.000          | 1.24           |                   |                | 121.7         | SURCHARGED |          |
| 7.003 | S 7.3         | 0.503        | 0.000          | 1.54           |                   |                | 145.2         | SURCHARGED |          |
| 7.004 | S 7.4         | 0.382        | 0.000          | 1.51           |                   |                | 152.0         | SURCHARGED |          |
| 8.000 | S 8.0         | 0.477        | 0.000          | 0.65           |                   |                | 38.4          | SURCHARGED |          |
| 8.001 | S 8.1         | 0.559        | 0.000          | 1.53           |                   |                | 91.5          | SURCHARGED |          |
| 8.002 | S 8.2         | 0.349        | 0.000          | 1.36           |                   |                | 133.1         | SURCHARGED |          |
| 8.003 | S 8.3         | 0.220        | 0.000          | 1.66           |                   |                | 157.2         | SURCHARGED |          |
| 7.005 | S 7.5         | 0.069        | 0.000          | 1.25           |                   |                | 309.1         | SURCHARGED |          |
| 7.006 | S 7.6         | 0.035        | 0.000          | 1.91           |                   |                | 310.1         | SURCHARGED |          |
| 7.007 | S 7.7         | 0.002        | 0.000          | 1.85           |                   |                | 310.0         | SURCHARGED |          |
| 9.000 | S 9.0         | 1.386        | 0.000          | 1.12           |                   |                | 65.9          | SURCHARGED |          |
| 9.001 | S 9.1         | 1.356        | 0.000          | 2.14           |                   |                | 126.0         | SURCHARGED |          |
| 9.002 | S 9.2         | 0.932        | 0.000          | 1.92           |                   |                | 178.0         | SURCHARGED |          |
| 9.003 | S 9.3         | 0.758        | 0.000          | 1.63           |                   |                | 236.3         | SURCHARGED |          |
| 9.004 | S 9.4         | 0.607        | 0.000          | 2.13           |                   |                | 295.5         | SURCHARGED |          |
| 9.005 | S 9.5         | 0.570        | 0.000          | 0.12           |                   |                | 24.2          | SURCHARGED |          |
| 9.006 | S 9.6         | 0.607        | 0.000          | 0.09           |                   |                | 24.8          | SURCHARGED |          |
| 9.007 | S 9.7         | 0.697        | 0.000          | 0.10           |                   |                | 26.3          | SURCHARGED |          |
| 9.008 | S 9.8         | 0.827        | 0.000          | 0.13           |                   |                | 27.9          | SURCHARGED |          |



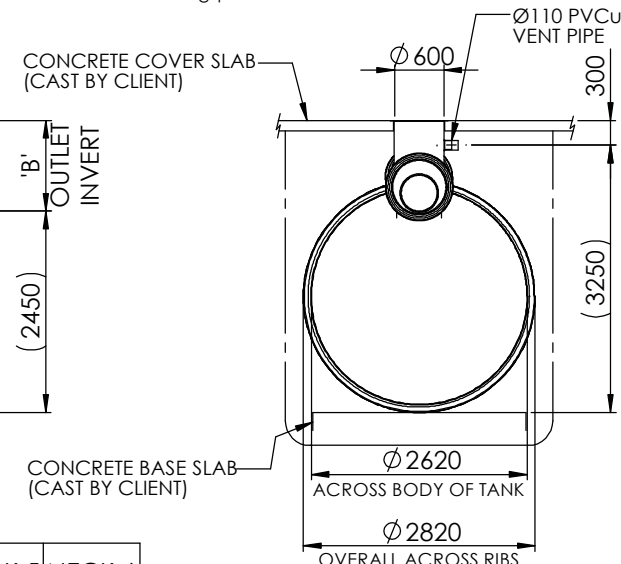
|   |   |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
|---|---|---|--------------|--------------|-----------|-------------|-----------------|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|--------|--|--------|---------|--|-------|-------|--|--------|--------|--|-------|-------|--|--|
| Clifton Scannell Emerson Associates   |   | Page 30   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| Seefort Lodge<br>Castledawson Avenue, Blackrock<br>Dublin, Ireland                                | Huntstown data centre facility  |  |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| Date 06/05/2021<br>File DUB040 SW Network-2.mdx   | Designed by ZS<br>Checked by CD   |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| Innovyze  | Network 2020.1.3  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| <u>100 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for Network 2</u> |   |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
|   | <table><tr><td></td><td><b>US/MH</b></td><td><b>Level</b></td></tr><tr><td><b>PN</b></td><td><b>Name</b></td><td><b>Exceeded</b></td></tr><tr><td>10.000</td><td>S 10.0</td><td></td></tr><tr><td>10.001</td><td>S 10.1</td><td></td></tr><tr><td>10.002</td><td>S 10.2</td><td></td></tr><tr><td>10.003</td><td>S 10.3</td><td></td></tr><tr><td>10.004</td><td>S 10.4</td><td></td></tr><tr><td>10.005</td><td>S 10.5</td><td></td></tr><tr><td>10.006</td><td>S 10.6</td><td></td></tr><tr><td>11.000</td><td>S 11.0</td><td></td></tr><tr><td>12.000</td><td>S 12.0</td><td></td></tr><tr><td>11.001</td><td>S 11.1</td><td></td></tr><tr><td>11.002</td><td>S 11.2</td><td></td></tr><tr><td>11.003</td><td>S 11.3</td><td></td></tr><tr><td>10.007</td><td>S 10.7</td><td></td></tr><tr><td>10.008</td><td>S 10.8</td><td></td></tr><tr><td>10.009</td><td>S 10.9</td><td></td></tr><tr><td>10.010</td><td>S 10.10</td><td></td></tr><tr><td>9.009</td><td>S 9.9</td><td></td></tr><tr><td>13.000</td><td>S 13.0</td><td></td></tr><tr><td>7.008</td><td>S 7.8</td><td></td></tr></table> |   | <b>US/MH</b> | <b>Level</b> | <b>PN</b> | <b>Name</b> | <b>Exceeded</b> | 10.000 | S 10.0 |  | 10.001 | S 10.1 |  | 10.002 | S 10.2 |  | 10.003 | S 10.3 |  | 10.004 | S 10.4 |  | 10.005 | S 10.5 |  | 10.006 | S 10.6 |  | 11.000 | S 11.0 |  | 12.000 | S 12.0 |  | 11.001 | S 11.1 |  | 11.002 | S 11.2 |  | 11.003 | S 11.3 |  | 10.007 | S 10.7 |  | 10.008 | S 10.8 |  | 10.009 | S 10.9 |  | 10.010 | S 10.10 |  | 9.009 | S 9.9 |  | 13.000 | S 13.0 |  | 7.008 | S 7.8 |  |  |
|   | <b>US/MH</b>  | <b>Level</b>  |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| <b>PN</b>   | <b>Name</b>   | <b>Exceeded</b>   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.000  | S 10.0  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.001  | S 10.1  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.002  | S 10.2  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.003  | S 10.3  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.004  | S 10.4  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.005  | S 10.5  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.006  | S 10.6  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 11.000  | S 11.0  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 12.000  | S 12.0  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 11.001  | S 11.1  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 11.002  | S 11.2  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 11.003  | S 11.3  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.007  | S 10.7  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.008  | S 10.8  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.009  | S 10.9  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 10.010  | S 10.10   |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 9.009   | S 9.9   |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 13.000  | S 13.0  |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| 7.008   | S 7.8   |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |
| ©1982-2020 Innovyze   |   |   |              |              |           |             |                 |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |        |  |        |         |  |       |       |  |        |        |  |       |       |  |  |

## **Appendix B – Hydrocarbon Interceptor Details**



#### NOTES

1. BS EN 858 STATES MINIMUM CONNECTION SIZES, UNITS ORDERED WITH DIFFERENT SIZE CONNECTIONS ARE NOT FULLY COMPLIANT WITH THE STANDARD. ALTERNATIVE CONNECTORS MAY BE ORDERED.
2. EXTENSION NECKS FOR DEEPER INVERTS CAN BE PROVIDED IN 0.5m INCREMENTS FOR ON SITE ASSEMBLY. MAX 2.0m INVERT RECOMMENDED.
3. ALL UNITS REQUIRE APPROPRIATE COVER & FRAME TO SUIT APPLIED LOADINGS.
4. THIS DRAWING SHOULD BE USED FOR DIMENSIONAL INFORMATION ONLY. IT IS ESSENTIAL THAT THIS DRAWING IS READ IN CONJUNCTION WITH INSTALLATION GUIDELINES SUPPLIED WITH THE UNIT (COPIES ARE AVAILABLE FROM OUR SALES DEPT.).
5. STANDARD PIPE ORIENTATION SHOWN. FOR OTHER AVAILABLE OPTIONS SEE TDS0033.
6. THIS DRAWING IS ALSO AVAILABLE ON OUR WEBSITE [www.kingspanenv.com](http://www.kingspanenv.com)



| UNIT REF. | UNIT CLASS | NOMINAL FLOW RATE (L/s) | APPROX. EMPTY WEIGHT (kg) | 'L' OVERALL LENGTH | 'A' BASE TO INLET INVERT | 'B' OUTLET INVERT | 'C' STD. PIPE DIA. (GRP) | NECK 1 FITTED | NECK 2 FITTED | NECK 3 FITTED | NECK 4 FITTED | NECK 5 FITTED | NECK 6 FITTED |
|-----------|------------|-------------------------|---------------------------|--------------------|--------------------------|-------------------|--------------------------|---------------|---------------|---------------|---------------|---------------|---------------|
| NSFA080   | 1          | 80                      | 1250                      | 5744               | 2500                     | 1050              | 300                      | ✓             | ✓             |               |               |               |               |
| NSFA100   | 1          | 100                     | 1350                      | 6200               | 2500                     | 1050              | 375/400                  | ✓             | ✓             |               |               |               |               |
| NSFA125   | 1          | 125                     | 1700                      | 7365               | 2500                     | 1050              | 450                      | ✓             | ✓             | ✓             |               |               |               |
| NSFA150   | 1          | 150                     | 2000                      | 8675               | 2550                     | 1100              | 500/525                  | ✓             | ✓             | ✓             |               |               |               |
| NSFA175   | 1          | 175                     | 2400                      | 9975               | 2550                     | 1100              | 500/525                  | ✓             | ✓             | ✓             | ✓             |               |               |
| NSFA200   | 1          | 200                     | 2700                      | 11280              | 2550                     | 1100              | 600                      | ✓             | ✓             | ✓             | ✓             |               |               |
| NSFA210   | 1          | 210                     | 2900                      | 11994              | 2550                     | 1100              | 600                      | ✓             | ✓             | ✓             | ✓             | ✓             |               |
| NSFA225   | 1          | 225                     | 3100                      | 12766              | 2550                     | 1100              | 600                      | ✓             | ✓             | ✓             | ✓             | ✓             |               |
| NSFA240   | 1          | 240                     | 3300                      | 13582              | 2550                     | 1100              | 600                      | ✓             | ✓             | ✓             | ✓             | ✓             |               |
| NSFA255   | 1          | 255                     | 3450                      | 14300              | 2550                     | 1100              | 600                      | ✓             | ✓             | ✓             | ✓             | ✓             | ✓             |
| NSFA270   | 1          | 270                     | 3600                      | 15071              | 2550                     | 1100              | 600                      | ✓             | ✓             | ✓             | ✓             | ✓             | ✓             |
| NSFA285   | 1          | 285                     | 3800                      | 15833              | 2550                     | 1100              | 600                      | ✓             | ✓             | ✓             | ✓             | ✓             | ✓             |

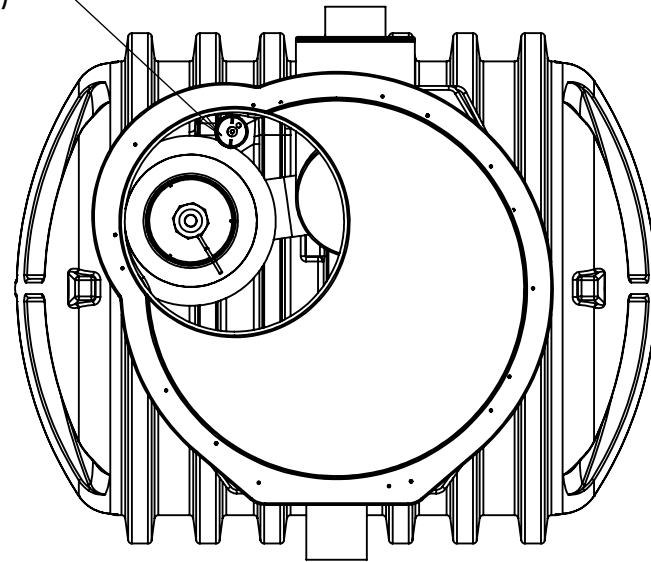
|   |          |          |   |
|---|----------|----------|---|
| Please check with Kingspan Environmental For The Latest Issue Of This Drawing |          |          |   |
| Issue   | Date     | Drawn by | Description   |
| 04  | 11.03.19 | T.Kelly  | CC1444 - Units now built to 1.0m Invert First Fix           |
| 03  | 03.04.18 | T.Kelly  | CC1425 - Units 210 to 285 Added : Class 2 Reference Deleted |

|                |                    |
|----------------|--------------------|
| Material : n/a | Tolerance : n/a    |
| Finish : n/a   | Thickness : n/a    |
| Weight : n/a   | Surface Area : n/a |

|   |             |
|---|-------------|
| Drawing : DS0896P                           | Page 1 of 1 |
| NSFA080 - NSFA285 Full Retention Separators |             |

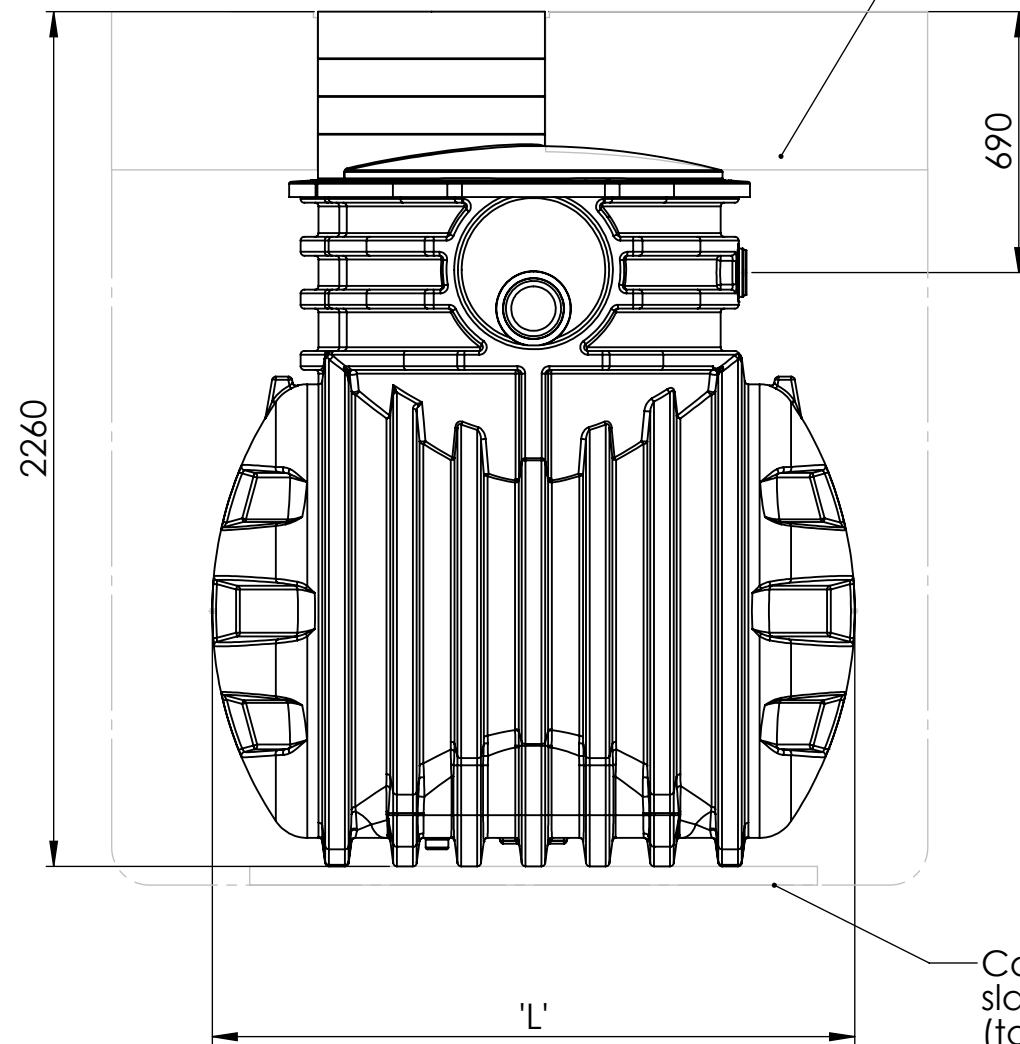
|                      |                     |   |
|----------------------|---------------------|---|
| All dimensions in mm | Scale: Not to scale | Kingspan reserve the right to alter the details of this drawing without prior notice. This drawing is copyright and may not be reproduced or used without the written permission of Kingspan. |
|----------------------|---------------------|---|

Alarm Probe Tube  
(see note 7)

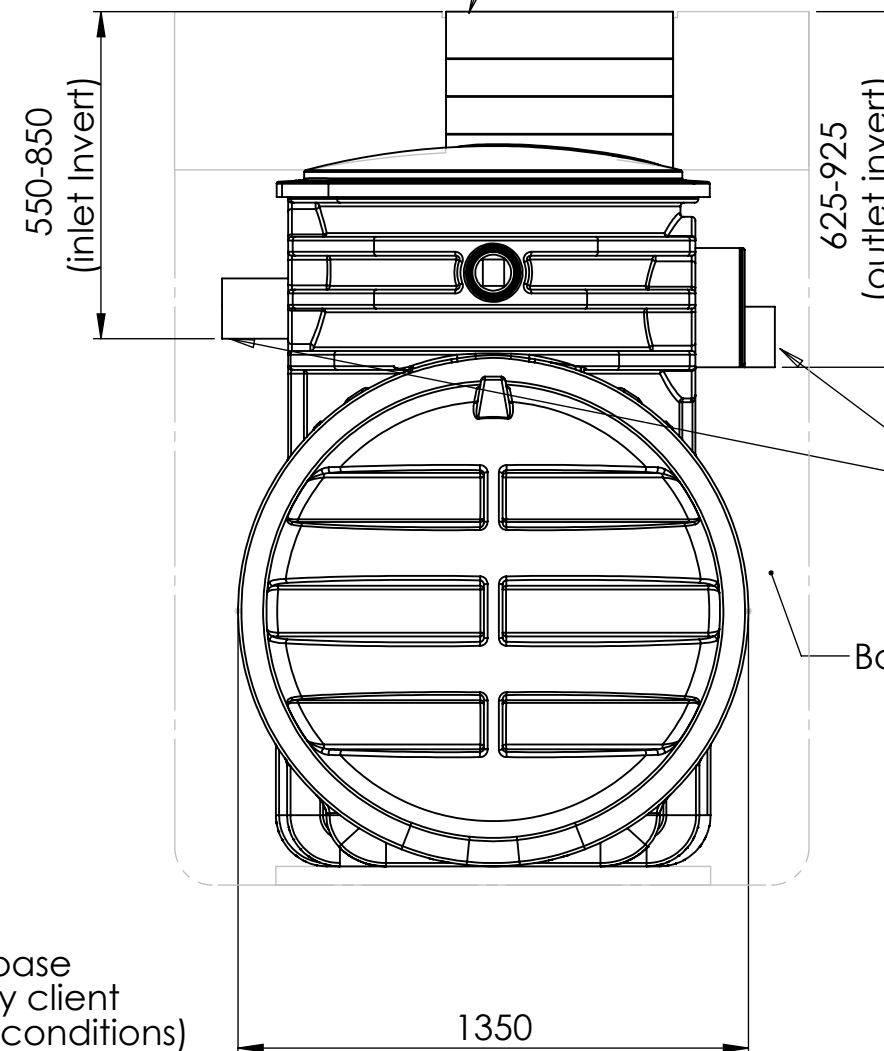


Concrete cover slab cast by client  
(to suit wet site conditions)

Neck can be trimmed  
down to required invert



Concrete base  
slab cast by client  
(to suit site conditions)



Ø160 mm inlet/outlet plain pipe

Backfill (see note 8)

| Unit Ref No | Nominal Flow | Dim L (mm) | Approx Empty Weight (kgs) | Fall across unit |
|-------------|--------------|------------|---------------------------|------------------|
| NSFP003     | 3 L/s        | 1700       | 180                       | 75               |
| NSFP006     | 6 L/s        | 1700       | 180                       | 75               |

Notes:-

1. Inlet/Outlet pipes are plain pipe  $\varnothing 160$  mm PVCu. The standard EN 858 states minimum connection sizes, units ordered with different sized connections are not fully compliant with the standard.

2. Extension necks for deeper inverts can be provided. These can be cut in 200 mm sections. Max 2.0m Invert recommended. Please ask our sales department for further details.

3. All units require appropriate cover and frame to suit applied loadings.

4. This drawing should be used for dimensional information only. It is essential that this drawing is read in conjunction with the installation guidelines supplied with the unit. (Copies are available from our sales dept.).

5. This drawing is also available on our website [www.kingspanenv.com](http://www.kingspanenv.com).

6. A  $\varnothing 76$  mm tube (internal) is supplied to house an oil alarm probe.

7. Wet site conditions - Concrete Backfill  
Dry site conditions - Pea Shingle Backfill

Please refer to installation manual for details of correct backfilling.

Please check with Kingspan Environmental that this drawing is the latest issue

| Issue | Date     | Drawn by | Approved by | Description                                 |
|-------|----------|----------|-------------|---|
| 04    | 15/12/10 | S.Gill   |             | CC934                                       |
| 03    | 24/02/10 | S. Gill  |             | CC794                                       |
| 02    | 23/09/09 | S.Gill   |             | Drawing Description Changed/Table Corrected |
| 01    | 19/03/09 | S.Gill   |             | Initial Release                             |

Material : n/a  
Finish : n/a  
Weight : Kgs n/a

Tolerance : n/a  
Thickness : n/a  
Surface Area : n/a

Drawing : NSFP 003-006 Sales Drawing

Page 1 of 1

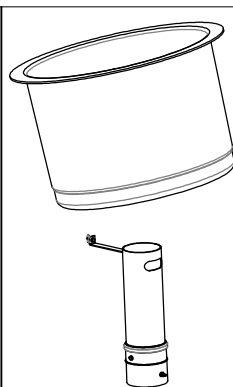
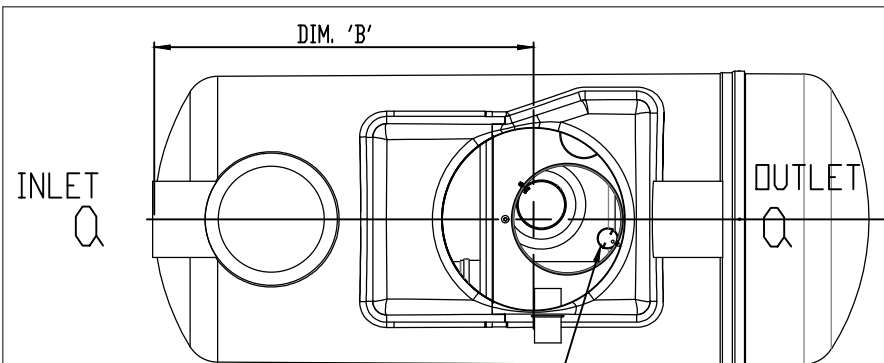
Drg No - DSO992

All dimensions in mm

Scale: Not to scale

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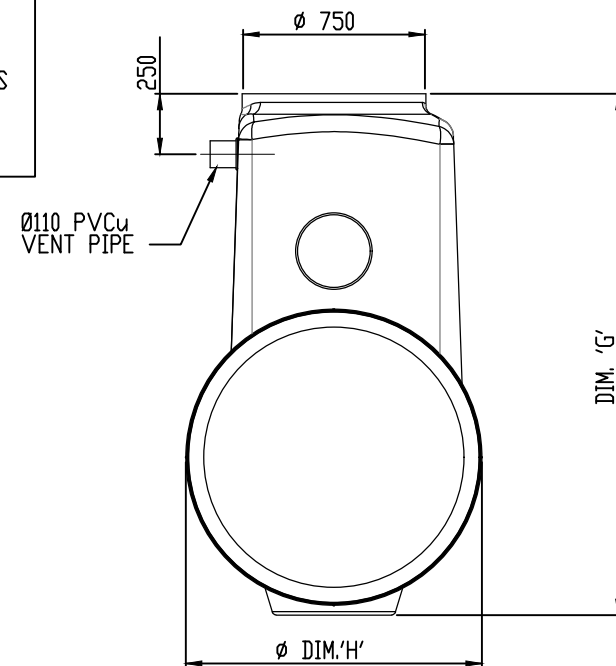
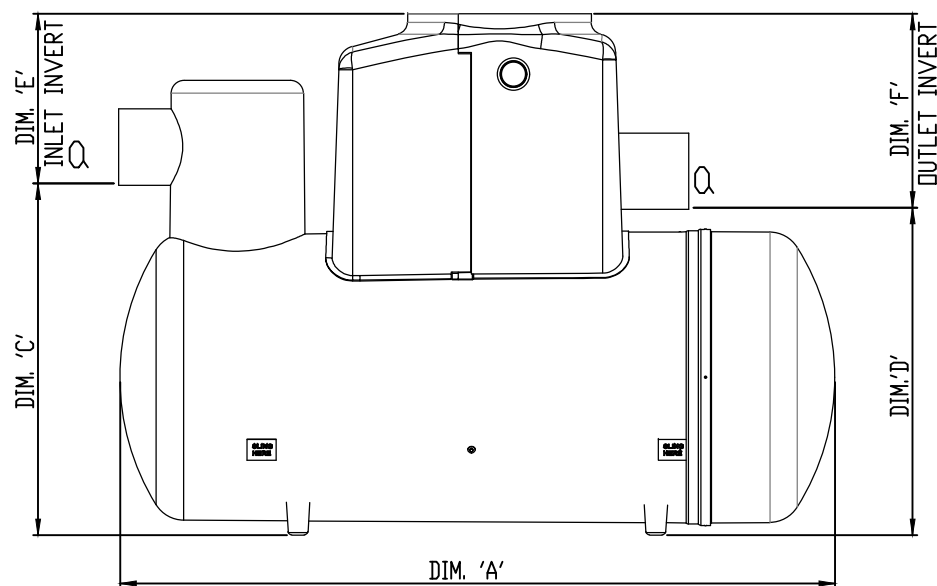




EXTENSION PARTS  
(IF REQUIRED)  
INCLUDED IN  
PRODUCT CODE

#### NOTES

1. UNITS ARE SUPPLIED WITH THE STANDARD (MINIMUM) PIPEWORK SIZE, AND ORIENTATION SHOWN ON THE DRAWING. THE STANDARD EN858-1 STATES MINIMUM CONNECTION SIZES, UNITS ORDERED WITH DIFFERENT SIZE CONNECTIONS MAY NOT BE FULLY COMPLIANT WITH THE STANDARD. PLEASE CONSULT OUR SALES DEPARTMENT FOR DETAILS OF AVAILABLE OPTIONS, BUT PLEASE NOTE WE DO NOT ALTER INTERNAL PIPEWORK.
2. ALL UNITS SUPPLIED ARE CLASS 1 AND INCLUDE A COALESCER.
3. EXTENSION PARTS FOR DEEPER INVERTS CAN BE PROVIDED FOR ON SITE ASSEMBLY.
4. ALL UNITS REQUIRE APPROPRIATE CONCRETE BASE, COVER AND FRAME TO SUIT APPLIED LOADINGS.
5. THIS DRAWING SHOULD BE USED FOR DIMENSIONAL INFORMATION ONLY.
6. A Ø76mm TUBE IS SUPPLIED TO HOUSE AN OIL ALARM PROBE.



| UNIT    | NOMINAL FLOW (l/sec.) | DIM.'A' | DIM.'B' | DIM.'C' | DIM.'D' | DIM.'E' | DIM.'F' | DIM.'G' | DIM.'H' | STD. PIPE Ø | APPROX. EMPTY WEIGHT (kg) | FALL ACROSS UNIT |
|---------|-----------------------|---------|---------|---------|---------|---------|---------|---------|---------|-------------|---------------------------|------------------|
| NSBE010 | 10.0                  | 2069    | 1096    | 1450    | 1350    | 700     | 800     | 2150    | 1220    | 315         | 160                       | 100              |
| NSBE015 | 15.0                  | 2947    | 1560    | 1450    | 1350    | 700     | 800     | 2150    | 1220    | 315         | 200                       | 100              |
| NSBE020 | 20.0                  | 3893    | 2016    | 1450    | 1350    | 700     | 800     | 2150    | 1220    | 375         | 220                       | 100              |

Please check with Kingspan Environmental that this drawing is the latest issue

| Issue | Date     | Drawn by | Approved by | Description  | Material : Various | Tolerance : | Thickness : n/a | Surface Area : | Drawing : DS1155                    | Page 1 of 2 |
|-------|----------|----------|-------------|--|--------------------|-------------|-----------------|----------------|-------------------------------------|-------------|
| 03    | 14.09.12 | T.Kelly  |             | CC1081 - Inlet neck added & Std pipe for NSBE020 375 was 315 | Finish :           |             |                 |                |                                     |             |
| 02    | 20.08.12 | CS       |             | CC981 - Pipe work up date from 160 & 200 to 315dia.          | Weight :           |             |                 |                |                                     |             |
| 01    | 27.07.11 | T.Kelly  |             | CC981 - Initial Release                                      |                    |             |                 |                | NSBE010 - NSBE020 Bypass Separators |             |

All dimensions in mm

Scale: Not to scale

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## **Appendix C – Solid Separator Details**



CDS Dimensions (mm)

|         | CDS10404 | CDS0604 | CDS0606 | CDS0804 | CDS0806 | CDS0808 | CDS1010 | CDS1012 | CDS1015 |
|---------|----------|---------|---------|---------|---------|---------|---------|---------|---------|
| A       | 370      | 370     | 370     | 370     | 370     | 370     | 500     | 500     | 500     |
| B       | 444      | 815     | 615     | 810     | 830     | 810     | 800     | 800     | 830     |
| C       | 1250     | 1985    | 1985    | 2080    | 2300    | 2480    | 2800    | 3000    | 3330    |
| D       | 800      | 1200    | 200     | 1500    | 1500    | 1500    | 2000    | 2000    | 2000    |
| E       | 1112     | 1665    | 1665    | 1966    | 1966    | 1966    | 2475    | 2475    | 2475    |
| F       | 400      | 700     | 700     | 700     | 700     | 800     | 1000    | 1000    | 1000    |
| G (dia) | 400      | 600     | 600     | 800     | 800     | 800     | 1000    | 1000    | 1000    |
| H       | 400      | 400     | 600     | 400     | 600     | 800     | 1000    | 1200    | 1500    |

## Selection Table — CDS Polypropylene Manhole Units

| Model Reference | Hydraulic Peak Flow Rate l/s | Treatment Flow Rate l/s | Drainage Area — Impermeable m <sup>2</sup> | Chamber Diameter (mm) | Internal Pipe Diameter (mm) |
|-----------------|------------------------------|-------------------------|--|-----------------------|-----------------------------|
| CDS 0404        | 30                           | 12.5                    | 2,000                                      | 900                   | 150/225                     |
| CDS 0604        | 70                           | 23                      | 5,000                                      | 1200                  | 225                         |
| CDS 0606/01     | 140                          | 38                      | 10,000                                     | 1200                  | 225-375                     |
| CDS 0606/02     | 200                          | 38                      | 15,000                                     | 1200                  | 225-375                     |
| CDS 0806        | 350                          | 49                      | 25,000                                     | 1500                  | 450                         |
| CDS 0808        | 400                          | 72                      | 30,000                                     | 1500                  | 450                         |
| CDS 1010        | 480                          | 116                     | 35,000                                     | 2000                  | 450                         |
| CDS 1012        | 550                          | 157                     | 40,000                                     | 2000                  | 450/750                     |
| CDS 1015        | 700                          | 211                     | 50,000                                     | 2000                  | 450/750                     |
| CDS 0804        | 275                          | 31                      | 20,000                                     | 1500                  | 300                         |

Proposed Peak Flow Rate for each model calculated using Rational Lloyd Davis with a rainfall intensity of 50mm/hr. For greater flows — special design/ construction required.

### In-Line CDS

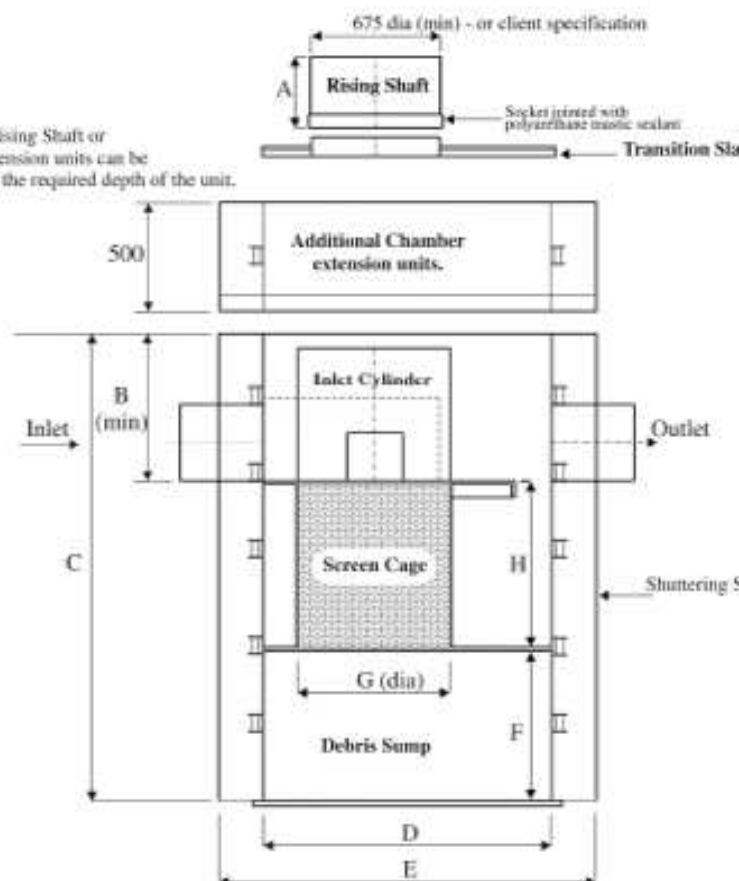
For small catchment, these units are used within the drainage system in-line and are supplied as BBA Approved\* complete manhole polypropylene units from the selection table above.

### Off-Line CDS

Larger catchment areas and retrofit projects designed with larger surface runoff conveyance capacity can receive treatment using a CDS unit placed adjacent to the storm pipeline. Water is channeled to these offline CDS configurations using a diversion structure. The diversion structure and its weir send the water quality flow to the offline CDS unit and also ensure larger flow events from less frequent storm events properly bypass the offline unit without cause flooding upstream of the unit.



Note:  
Additional Rising Shaft or Chamber extension units can be added to suit the required depth of the unit.



### Model Designation

A four digit number representing the screen diameter and screen height then follows to give the standard model designation for a CDS screen for installation into standard commercially available pre-fabricated manhole chambers. Example: CDS 0806 designates a separation screen dia. 0.8 m and screen height of 0.6m.

### Support

- Drawings and specifications are available at [contechstormwater.com](http://contechstormwater.com).
- Site-specific design support is available from our engineers.

800.338.1122

[contechstormwater.com](http://contechstormwater.com)
**CONTECH**

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CDS is a trademark of CONTECH Construction Products Inc.

## **Appendix D – QBAR Calculations**

# Greenfield runoff rate estimation for sites

www.uksuds.com | Greenfield runoff tool

|                |               |
|----------------|---------------|
| Calculated by: | Conor Doherty |
| Site name:     | DUB 40        |
| Site location: | Huntstown     |

This is an estimation of the greenfield runoff rates that are used to meet normal best practice criteria in line with Environment Agency guidance "Rainfall runoff management for developments", SC030219 (2013), the SuDS Manual C753 (Ciria, 2015) and the non-statutory standards for SuDS (Defra, 2015). This information on greenfield runoff rates may be the basis for setting consents for the drainage of surface water runoff from sites.

## Site Details

|            |                   |
|------------|-------------------|
| Latitude:  | 53.41135° N       |
| Longitude: | 6.32112° W        |
| Reference: | 1307439049        |
| Date:      | Feb 23 2021 14:37 |

## Runoff estimation approach

IH124

## Site characteristics

|                       |       |
|-----------------------|-------|
| Total site area (ha): | 12.85 |
|-----------------------|-------|

## Methodology

|                                     |                             |
|-------------------------------------|-----------------------------|
| Q <sub>BAR</sub> estimation method: | Calculate from SPR and SAAR |
| SPR estimation method:              | Calculate from SOIL type    |

## Soil characteristics

|              | Default | Edited |
|--------------|---------|--------|
| SOIL type:   | 2       | 2      |
| HOST class:  | N/A     | N/A    |
| SPR/SPRHOST: | 0.3     | 0.3    |

## Hydrological characteristics

|                                | Default | Edited |
|--------------------------------|---------|--------|
| SAAR (mm):                     | 935     | 822    |
| Hydrological region:           | 12      | 12     |
| Growth curve factor 1 year:    | 0.85    | 0.85   |
| Growth curve factor 30 years:  | 2.13    | 2.13   |
| Growth curve factor 100 years: | 2.61    | 2.61   |
| Growth curve factor 200 years: | 2.86    | 2.86   |

## Notes

### (1) Is Q<sub>BAR</sub> < 2.0 l/s/ha?

When Q<sub>BAR</sub> is < 2.0 l/s/ha then limiting discharge rates are set at 2.0 l/s/ha.

### (2) Are flow rates < 5.0 l/s?

Where flow rates are less than 5.0 l/s consent for discharge is usually set at 5.0 l/s if blockage from vegetation and other materials is possible. Lower consent flow rates may be set where the blockage risk is addressed by using appropriate drainage elements.

### (3) Is SPR/SPRHOST ≤ 0.3?

Where groundwater levels are low enough the use of soakaways to avoid discharge offsite would normally be preferred for disposal of surface water runoff.

## Greenfield runoff rates

|                         | Default | Edited |
|-------------------------|---------|--------|
| Q <sub>BAR</sub> (l/s): | 32.86   | 28.26  |
| 1 in 1 year (l/s):      | 27.93   | 24.02  |
| 1 in 30 years (l/s):    | 69.99   | 60.2   |
| 1 in 100 year (l/s):    | 85.76   | 73.76  |
| 1 in 200 years (l/s):   | 93.97   | 80.83  |

This report was produced using the greenfield runoff tool developed by HR Wallingford and available at [www.uksuds.com](http://www.uksuds.com). The use of this tool is subject to the UK SuDS terms and conditions and licence agreement, which can both be found at [www.uksuds.com/terms-and-conditions.htm](http://www.uksuds.com/terms-and-conditions.htm). The outputs from this tool are estimates of greenfield runoff rates. The use of these results is the responsibility of the users of this tool. No liability will be accepted by HR Wallingford, the Environment Agency, CEH, Hydrosolutions or any other organisation for the use of this data in the design or operational characteristics of any drainage scheme.

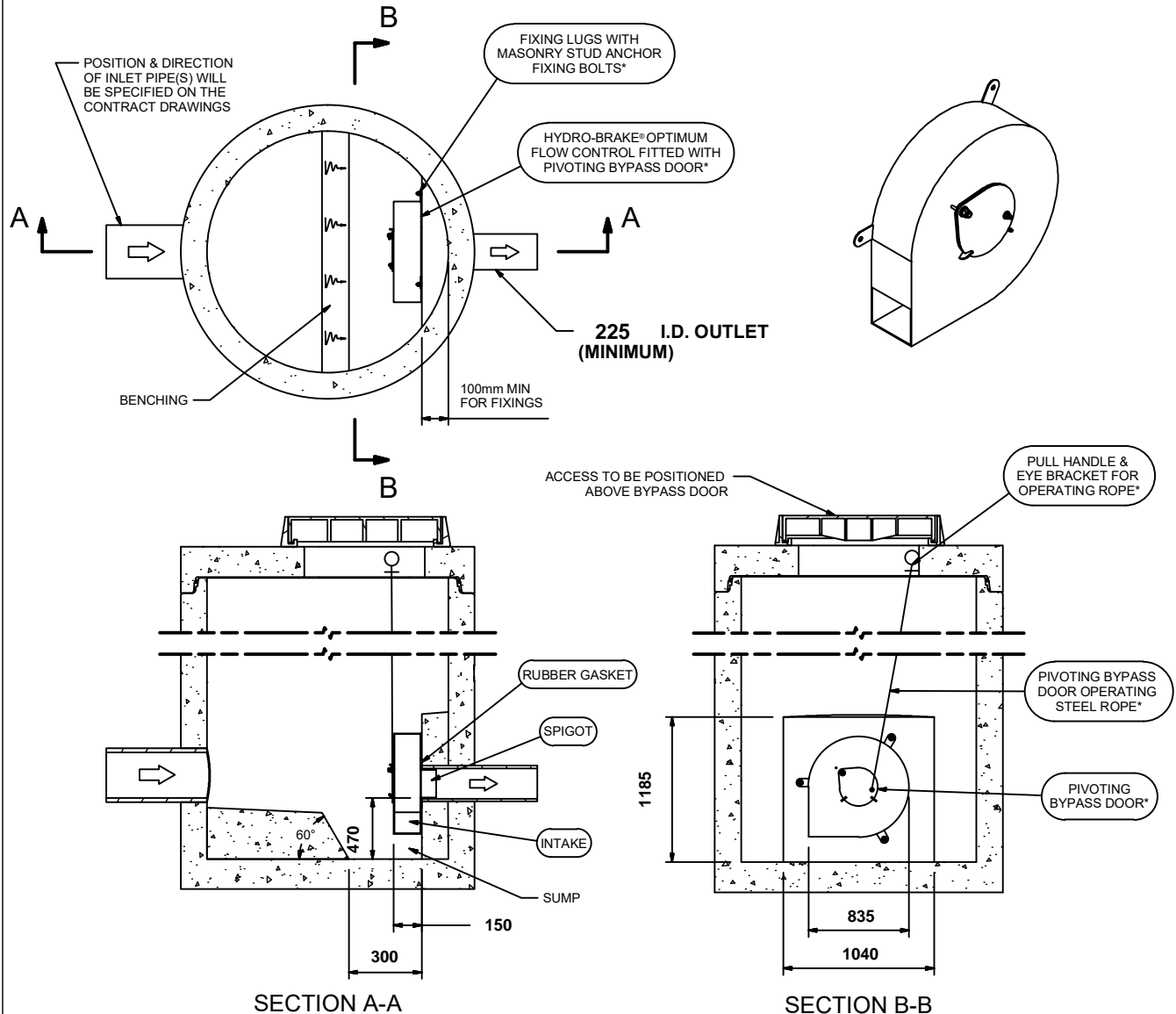
## **Appendix E – Flow Control Devise Details**

## Technical Specification

| Control Point  | Head (m) | Flow (l/s) |
|----------------|----------|------------|
| Primary Design | 2.000    | 11.988     |
| Flush-Flo™     | 0.583    | 11.986     |
| Kick-Flo®      | 1.209    | 9.456      |
| Mean Flow      |          | 10.499     |

Hydro-Brake® Optimum Flow Control including:

- 5 mm grade 304L stainless steel
- Integral stainless steel pivoting by-pass door allowing clear line of sight through to outlet, c/w stainless steel operating rope
- Beed blasted finish to maximise corrosion resistance
- Stainless steel fixings
- Rubber gasket to seal outlet



**IMPORTANT:** ○ LIMIT OF HYDRO INTERNATIONAL SUPPLY  
 THE DEVICE WILL BE HANDED TO SUIT SITE CONDITIONS  
 FOR SITE SPECIFIC DETAILS AND MINIMUM CHAMBER SIZE REFER TO HYDRO INTERNATIONAL  
 ALL CIVIL AND INSTALLATION WORK BY OTHERS  
 \* WHERE SUPPLIED  
 HYDRO-BRAKE® FLOW CONTROL & HYDRO-BRAKE® OPTIMUM FLOW CONTROL ARE REGISTERED TRADEMARKS FOR FLOW  
 CONTROLS DESIGNED AND MANUFACTURED EXCLUSIVELY BY HYDRO INTERNATIONAL

**THIS DESIGN LAYOUT IS FOR ILLUSTRATIVE PURPOSES ONLY. NOT TO SCALE.**

### DESIGN ADVICE



The head/flow characteristics of this SHE-0143-1200-2000-1200 Hydro-Brake® Optimum Flow Control are unique. Dynamic hydraulic modelling evaluates the full head/flow characteristic curve.  
**The use of any other flow control will invalidate any design based on this data and could constitute a flood risk.**

**Hydro**  
International®

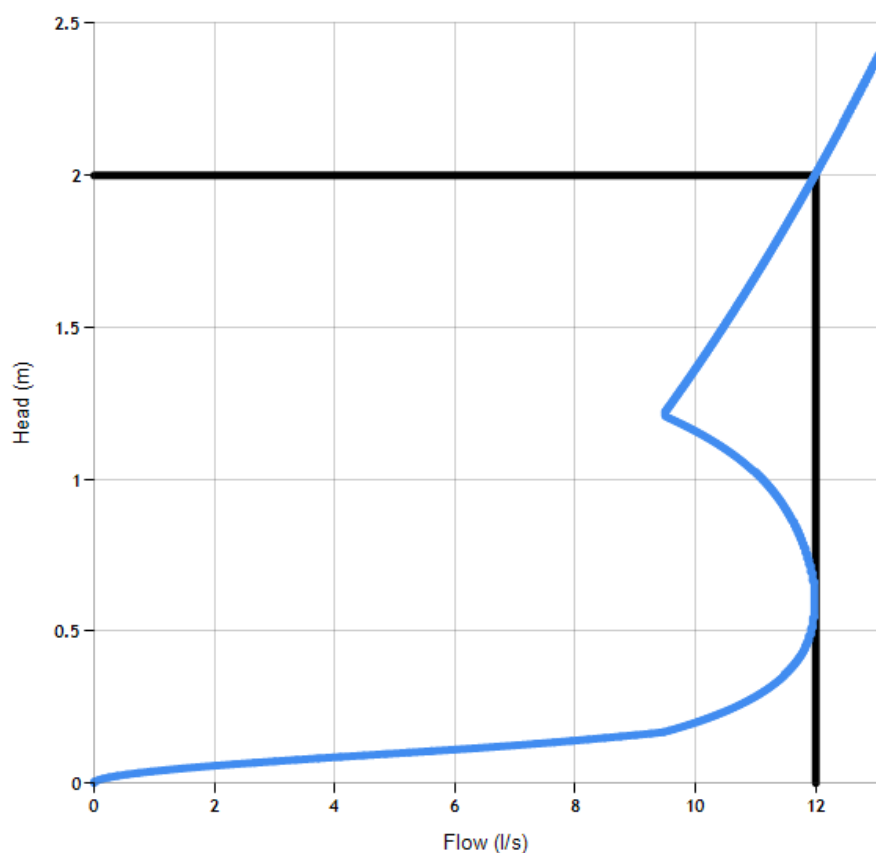
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|----------|---------------------|---|
| DATE     | 04/03/2021 09:26:45 | SHE-0143-1200-2000-1200<br>Hydro-Brake® Optimum |
| SITE     |                     |   |
| DESIGNER | Debbie Henry        |   |
| REF      | Hydrobrake 1        |   |

## Technical Specification

| Control Point  | Head (m) | Flow (l/s) |
|----------------|----------|------------|
| Primary Design | 2.000    | 11.988     |
| Flush-Flo™     | 0.583    | 11.986     |
| Kick-Flo®      | 1.209    | 9.456      |
| Mean Flow      |          | 10.499     |



PT/329/0412



| Head (m) | Flow (l/s) |
|----------|------------|
| 0.000    | 0.000      |
| 0.069    | 2.789      |
| 0.138    | 7.861      |
| 0.207    | 10.108     |
| 0.276    | 10.912     |
| 0.345    | 11.425     |
| 0.414    | 11.738     |
| 0.483    | 11.909     |
| 0.552    | 11.979     |
| 0.621    | 11.978     |
| 0.690    | 11.924     |
| 0.759    | 11.829     |
| 0.828    | 11.693     |
| 0.897    | 11.509     |
| 0.966    | 11.259     |
| 1.034    | 10.921     |
| 1.103    | 10.466     |
| 1.172    | 9.864      |
| 1.241    | 9.575      |
| 1.310    | 9.821      |
| 1.379    | 10.061     |
| 1.448    | 10.294     |
| 1.517    | 10.522     |
| 1.586    | 10.745     |
| 1.655    | 10.963     |
| 1.724    | 11.176     |
| 1.793    | 11.385     |
| 1.862    | 11.589     |
| 1.931    | 11.790     |
| 2.000    | 11.988     |

### DESIGN ADVICE



The head/flow characteristics of this SHE-0143-1200-2000-1200 Hydro-Brake Optimum® Flow Control are unique. Dynamic hydraulic modelling evaluates the full head/flow characteristic curve.

**The use of any other flow control will invalidate any design based on this data and could constitute a flood risk.**



DATE 04/03/2021 09:26:45

SITE

DESIGNER Debbie Henry

REF Hydrobrake 1

SHE-0143-1200-2000-1200

Hydro-Brake Optimum®

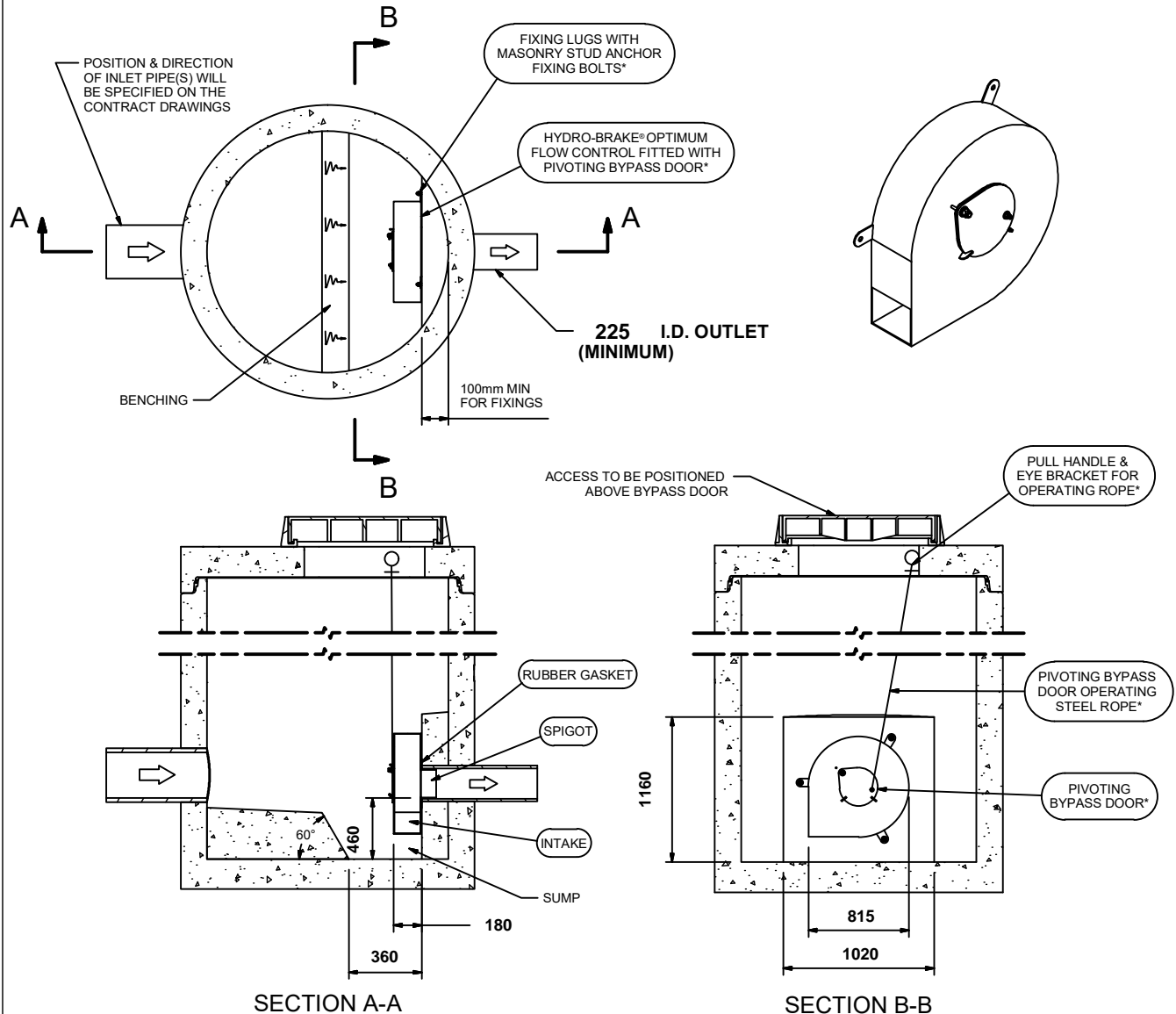


## Technical Specification

| Control Point  | Head (m) | Flow (l/s) |
|----------------|----------|------------|
| Primary Design | 1.600    | 16.456     |
| Flush-Flo™     | 0.474    | 16.466     |
| Kick-Flo®      | 1.020    | 13.299     |
| Mean Flow      |          | 14.303     |

Hydro-Brake® Optimum Flow Control including:

- 5 mm grade 304L stainless steel
- Integral stainless steel pivoting by-pass door allowing clear line of sight through to outlet, c/w stainless steel operating rope
- Beed blasted finish to maximise corrosion resistance
- Stainless steel fixings
- Rubber gasket to seal outlet



**IMPORTANT:** ○ LIMIT OF HYDRO INTERNATIONAL SUPPLY  
 THE DEVICE WILL BE HANDED TO SUIT SITE CONDITIONS  
 FOR SITE SPECIFIC DETAILS AND MINIMUM CHAMBER SIZE REFER TO HYDRO INTERNATIONAL  
 ALL CIVIL AND INSTALLATION WORK BY OTHERS  
 \* WHERE SUPPLIED  
 HYDRO-BRAKE® FLOW CONTROL & HYDRO-BRAKE® OPTIMUM FLOW CONTROL ARE REGISTERED TRADEMARKS FOR FLOW  
 CONTROLS DESIGNED AND MANUFACTURED EXCLUSIVELY BY HYDRO INTERNATIONAL

**THIS DESIGN LAYOUT IS FOR ILLUSTRATIVE PURPOSES ONLY. NOT TO SCALE.**

### DESIGN ADVICE



The head/flow characteristics of this SHE-0174-1650-1600-1650 Hydro-Brake® Optimum Flow Control are unique. Dynamic hydraulic modelling evaluates the full head/flow characteristic curve.  
**The use of any other flow control will invalidate any design based on this data and could constitute a flood risk.**

**Hydro**  
International®

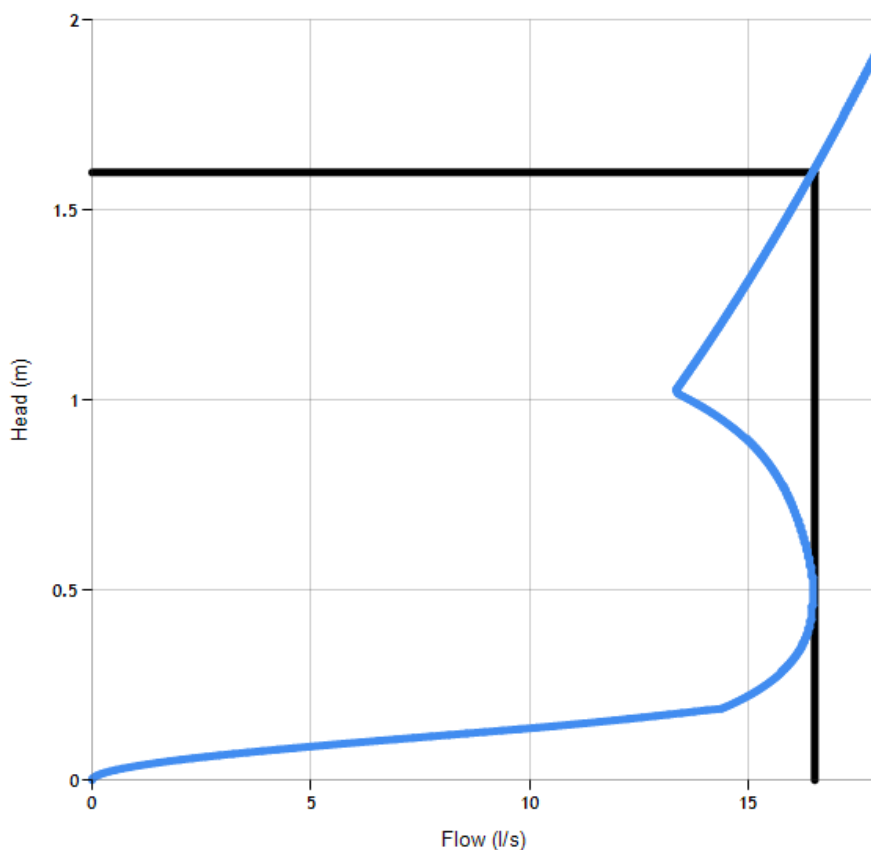
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|----------|---------------------|---|
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| SITE     |                     |   |
| DESIGNER | Debbie Henry        |   |
| REF      | Hydrobrake 2        |   |

## Technical Specification

| Control Point  | Head (m) | Flow (l/s) |
|----------------|----------|------------|
| Primary Design | 1.600    | 16.456     |
| Flush-Flo™     | 0.474    | 16.466     |
| Kick-Flo®      | 1.020    | 13.299     |
| Mean Flow      |          | 14.303     |



PT/329/0412



| Head (m) | Flow (l/s) |
|----------|------------|
| 0.000    | 0.000      |
| 0.055    | 2.122      |
| 0.110    | 7.230      |
| 0.166    | 12.589     |
| 0.221    | 14.961     |
| 0.276    | 15.666     |
| 0.331    | 16.101     |
| 0.386    | 16.344     |
| 0.441    | 16.450     |
| 0.497    | 16.460     |
| 0.552    | 16.404     |
| 0.607    | 16.303     |
| 0.662    | 16.165     |
| 0.717    | 15.990     |
| 0.772    | 15.766     |
| 0.828    | 15.468     |
| 0.883    | 15.065     |
| 0.938    | 14.514     |
| 0.993    | 13.774     |
| 1.048    | 13.471     |
| 1.103    | 13.801     |
| 1.159    | 14.123     |
| 1.214    | 14.437     |
| 1.269    | 14.743     |
| 1.324    | 15.043     |
| 1.379    | 15.337     |
| 1.434    | 15.625     |
| 1.490    | 15.907     |
| 1.545    | 16.184     |
| 1.600    | 16.456     |

### DESIGN ADVICE



The head/flow characteristics of this SHE-0174-1650-1600-1650 Hydro-Brake Optimum® Flow Control are unique. Dynamic hydraulic modelling evaluates the full head/flow characteristic curve.

**The use of any other flow control will invalidate any design based on this data and could constitute a flood risk.**



DATE 04/03/2021 09:28:21

SITE

DESIGNER Debbie Henry

REF Hydrobrake 2

SHE-0174-1650-1600-1650

Hydro-Brake Optimum®



## **Appendix F – Irish Water Confirmation of Feasibility**

Philip Corr

Seafort Lodge  
Castledawson Avenue  
Blackrock  
Co. Dublin  
A94P768

**Uisce Éireann**  
Bosca OP 448  
Oifig Sheachadta na  
Cathrach Theas  
Cathair Chorcaí

**Irish Water**  
PO Box 448,  
South City  
Delivery Office,  
Cork City.

[www.water.ie](http://www.water.ie)

31 March 2021

**Re: CDS20004468 pre-connection enquiry - Subject to contract Contract denied**

**Connection for Business Connection of 3 units at Huntstown, Dublin, Co. Dublin**

Dear Sir/Madam,

Irish Water has reviewed your pre-connection enquiry in relation to a Water & Wastewater connection at Huntstown, Dublin, Co. Dublin (the **Premises**). Based upon the details you have provided with your pre-connection enquiry and on our desk top analysis of the capacity currently available in the Irish Water network(s) as assessed by Irish Water, we wish to advise you that your proposed connection to the Irish Water network(s) can be facilitated at this moment in time.

| SER ICE                | <b>OUTCOME OF PRE-CONNECTION ENQUIR</b><br><b><u>THIS IS NOT A CONNECTION OFFER. OU MUST APPL FOR A CONNECTION(S) TO THE IRISH WATER NETWORK(S) IF OU WISH TO PROCEED.</u></b>                  |
|------------------------|---|
| Water Connection       | Feasible Subject to upgrades  |
| Wastewater Connection  | Feasible without infrastructure upgrade by Irish Water  |
| SITE SPECIFIC COMMENTS |   |
| Water Connection       | Approx. 1500m of new 450mm ID pipe main to replace the existing 6" uPVC main as shown below (red dashed line) will be required. This new 450mm will be connected to the existing 450mm DI main. |



Upgrade of pumps at Balleycoolen Highlands Tower will be required.

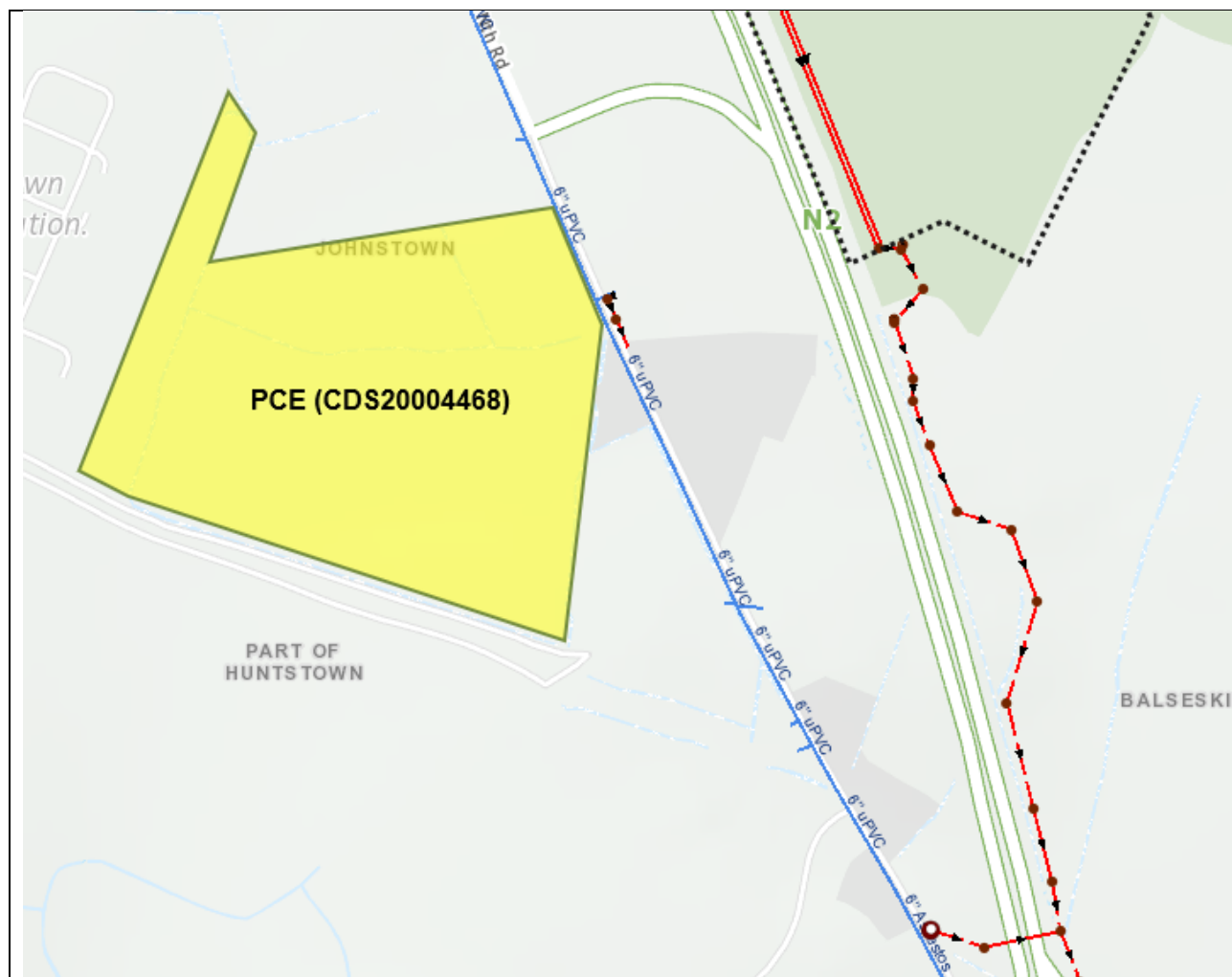
The Developer has to fund a portion of the upgrade works. That will be determined at a connection application stage, based on the peak flow and other connection applications in Hunstown SDZ at that time.

On-site water storage will be required for the average day peak week demand rate of the commercial section for 24-hour period with a re-fill time of 12 hours.

New bulk meter and associated telemetry system will be required to be installed along this connection main.

The design and construction of the Water & Wastewater pipes and related infrastructure to be installed in this development shall comply with the Irish Water Connections and Developer Services Standard Details and Codes of Practice that are available on the Irish Water website. Irish Water reserves the right to supplement these requirements with Codes of Practice and these will be issued with the connection agreement.

The map included below outlines the current Irish Water infrastructure adjacent to your site:



Reproduced from the Ordnance Survey of Ireland by Permission of the Government. License No. 3-3-34

Whilst every care has been taken in its compilation Irish Water gives this information as to the position of its underground network as a general guide only on the strict understanding that it is based on the best available information provided by each Local Authority in Ireland to Irish Water. Irish Water can assume no responsibility for and give no guarantees, undertakings or warranties concerning the accuracy, completeness or up to date nature of the information provided and does not accept any liability whatsoever arising from any errors or omissions. This information should not be relied upon in the event of excavations or any other works being carried out in the vicinity of the Irish Water underground network. The onus is on the parties carrying out excavations or any other works to ensure the exact location of the Irish Water underground network is identified prior to excavations or any other works being carried out. Service connection pipes are not generally shown but their presence should be anticipated.


#### General Notes:

- 1) The initial assessment referred to above is carried out taking into account water demand and wastewater discharge volumes and infrastructure details on the date of the assessment. **The availability of capacity may change at any date after this assessment.**
- 2) This feedback does not constitute a contract in whole or in part to provide a connection to any Irish Water infrastructure. All feasibility assessments are subject to the constraints of the Irish Water Capital Investment Plan.

- 3) The feedback provided is subject to a Connection Agreement/contract being signed at a later date.
- 4) A Connection Agreement will be required to commencing the connection works associated with the enquiry this can be applied for at <https://www.water.ie/connections/get-connected/>
- 5) A Connection Agreement cannot be issued until all statutory approvals are successfully in place.
- 6) Irish Water Connection Policy/ Charges can be found at <https://www.water.ie/connections/information/connection-charges/>
- 7) Please note the Confirmation of Feasibility does not extend to your fire flow requirements.
- 8) Irish Water is not responsible for the management or disposal of storm water or ground waters. You are advised to contact the relevant Local Authority to discuss the management or disposal of proposed storm water or ground water discharges
- 9) To access Irish Water Maps email [datarequests@water.ie](mailto:datarequests@water.ie)
- 10) All works to the Irish Water infrastructure, including works in the Public Space, shall have to be carried out by Irish Water.

If you have any further questions, please contact Marina Byrne from the design team via email [mzbyrne@water.ie](mailto:mzbyrne@water.ie) For further information, visit **[www.water.ie/connections](https://www.water.ie/connections)**.

Yours sincerely,




**Yvonne Harris**

**Head of Customer Operations**

## **Appendix G – Foul Drainage Calculations**

| TITLE   |                          |       |          |          |         |            |           | Project Number     |           |                |           |           |                | Revision | Date       |
|---|--------------------------|-------|----------|----------|---------|------------|-----------|--------------------|-----------|----------------|-----------|-----------|----------------|----------|------------|
| Project   | Data Centre at Huntstown |       |          |          |         |            |           | 20_099             |           |                |           |           |                | Planning | 07/05/2021 |
| SUBJECT   |                          |       |          |          |         |            |           |                    |           |                |           |           |                |          |            |
| Public Gravity Sewer Capacity Check   |                          |       |          |          |         |            |           |                    |           |                |           |           |                |          |            |
| Irish Water Code of Practice for Wastewater Infrastrurcture (IW_CDS-5030-03)  |                          |       |          |          |         |            |           |                    |           |                |           |           |                |          |            |
| Note:   |                          |       |          |          |         |            |           |                    |           |                |           |           |                |          |            |
| k <sub>s</sub> =  | 0.0015                   | m     |          |          |         |            |           |                    |           |                |           |           |                |          |            |
| Pipe  | Dist                     | Slope | Piezo    | Pipe     | Pipe    |            | Full      |                    | Full      | Prop Discharge | Prop      | Actual    | Self Cleansing |          | Notes      |
| Section   | (m)                      | (1/X) | Gradient | Dia (mm) | Dia (m) | Flow (l/s) | Cap (l/s) | Adequate Capacity? | Vel (m/s) | <0.8           | Vel (m/s) | Vel (m/s) | >0.75m/s       |          |            |
| Domestic Foul   |                          |       |          |          |         |            |           |                    |           |                |           |           |                |          |            |
| F1.1-F1.3   | 135.0                    | 80.0  | 0.013    | 150.0    | 0.150   | 3.70       | 17.309    | ✓                  | 0.98      | 0.21           | 0.77      | 0.76      | ✓              |          |            |
| F1.3-F1.4   | 76.0                     | 100.0 | 0.010    | 150.0    | 0.150   | 5.32       | 15.470    | ✓                  | 0.88      | 0.34           | 0.90      | 0.79      | ✓              |          |            |
| F2.0-F2.5   | 50.0                     | 80.0  | 0.013    | 100.0    | 0.100   | 4.75       | 5.839     | ✓                  | 0.74      | 0.81           | 1.10      | 0.82      | ✓              | **       |            |
| CWD Drainage  |                          |       |          |          |         |            |           |                    |           |                |           |           |                |          |            |
| CWD   | 76.0                     | 200.0 | 0.005    | 225.0    | 0.225   | 19.00      | 32.193    | ✓                  | 0.81      | 0.59           | 1.04      | 0.84      | ✓              |          |            |
| Notes:  |                          |       |          |          |         |            |           |                    |           |                |           |           |                |          |            |
| Proportional Discharge = Actual Discharge/Full Bore Discharge                 |                          |       |          |          |         |            |           |                    |           |                |           |           |                |          |            |
| Proportional Velocity = Actual Velocity/Full Bore Velocity                    |                          |       |          |          |         |            |           |                    |           |                |           |           |                |          |            |
| k <sub>s</sub> = Pipe Roughness Factor  |                          |       |          |          |         |            |           |                    |           |                |           |           |                |          |            |
| Design Flow based on Equation 2 of Sectio 2.2 of Appendix B to IW-CDS-5030-03 |                          |       |          |          |         |            |           |                    |           |                |           |           |                |          |            |
| ** As per Section 3.6.6 of IW-CDS-5030-03)                                    |                          |       |          |          |         |            |           |                    |           |                |           |           |                |          |            |



CLIFTON SCANNELL EMERSON ASSOCIATES  
Consulting Engineers  
E-mail: info@csea.ie      Web: www.csea.ie



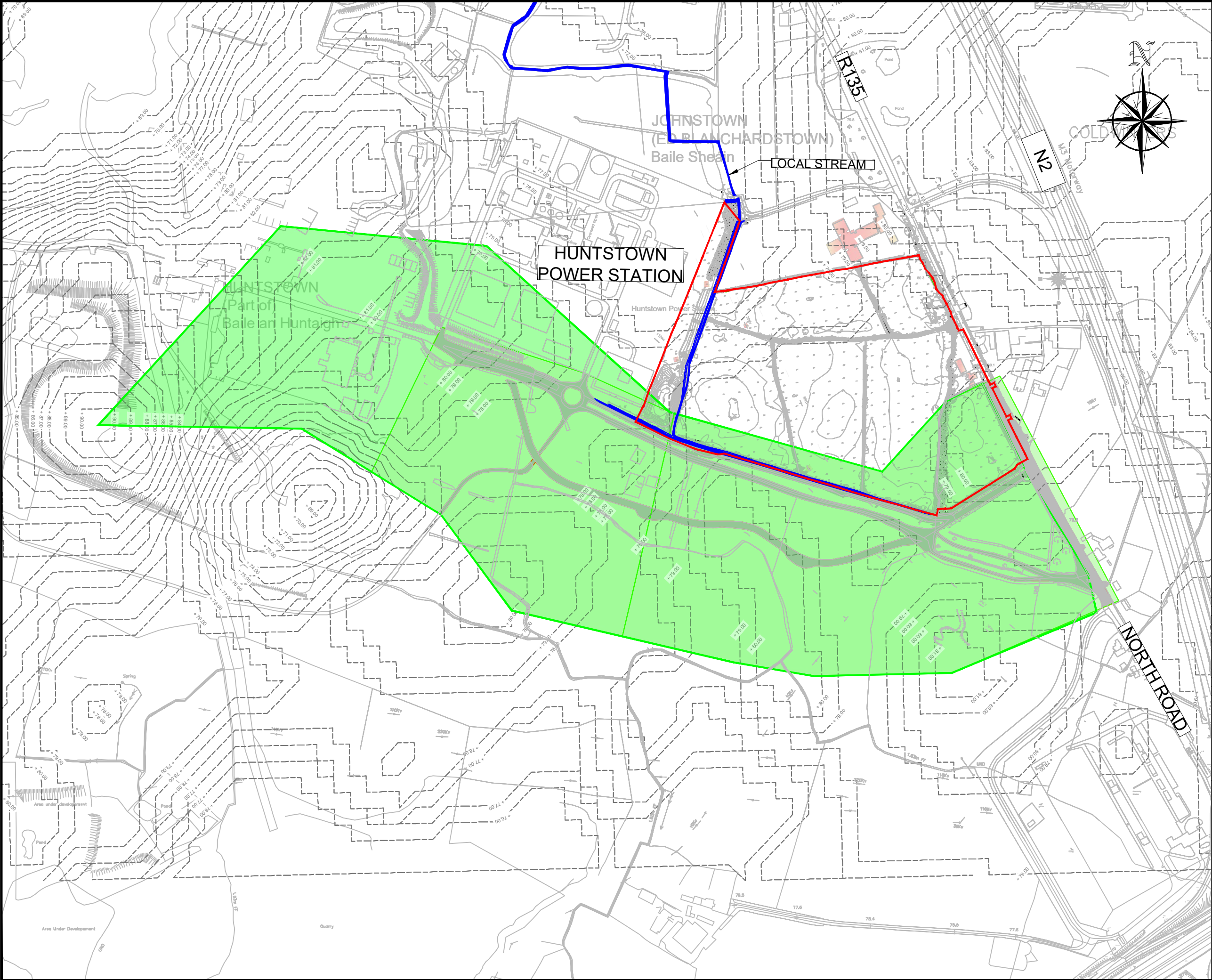
**CLIFTON SCANNELL EMERSON ASSOCIATES**  
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## **Appendix H – Ditch Diversion Catchment Map**





**LEGEND:**

- OUTLINE OF SITE SUBJECT TO THIS APPLICATION
- EXISTING CONTOURS
- EXISTING LEVELS
- CATCHMENT AREA
- ROAD AREA
- EXISTING DRAINS

|  |  |  |  |  |  |
|--|--|--|--|--|--|
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|     |                     |       |         |            |
|-----|---------------------|-------|---------|------------|
| P02 | ISSUED FOR PLANNING | DM    | CD      | 04-08-2021 |
| P01 | FOR INFORMATION     | PH    | CD      | 08-04-2021 |
| Rev | Description         | Drawn | Checked | Date       |

Clifton Scannell Emerson Associates Limited  
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Seafort Lodge,  
Castledawson Avenue,  
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W: www.csea.ie

HUNTSTOWN POWER COMPANY LTD

HUNTSTOWN DATA CENTRE FACILITY

PROPOSED DITCH DIVERSION CATCHMENT AREA

Client

Project

Dwg. Title

Drawn By PH Date 08-04-2021

Checked By CD Scale 1:500 @ A3

Project Code Originator Zone/Phase Level Type Role Dwg. No.

20\_099

CSEA Job No.


S2 FOR INFORMATION

Status Code Suitability Description

P02 PLANNING

Revision Project Status

## **Appendix I – Ditch Diversion Calculations**

|  |  |   |
|--|--|---|
| Clifton Scannell Emerson Associates                                |  | Page 1  |
| Seefort Lodge<br>Castledawson Avenue, Blackrock<br>Dublin, Ireland | Project:<br>Huntstown data centre facility |  |
| Date 06/05/2021<br>File Existing watercourse.MDX                   | Designed by ZS<br>Checked by CD            |   |
| Innovyze   | Network 2020.1.3                           |   |

### STORM SEWER DESIGN by the Modified Rational Method

#### Design Criteria for Storm

Pipe Sizes STANDARD Manhole Sizes STANDARD

FSR Rainfall Model - Scotland and Ireland

|                                      |        |                                       |       |
|--------------------------------------|--------|---------------------------------------|-------|
| Return Period (years)                | 1      | PIMP (%)                              | 10    |
| M5-60 (mm)                           | 16.500 | Add Flow / Climate Change (%)         | 0     |
| Ratio R                              | 0.300  | Minimum Backdrop Height (m)           | 0.175 |
| Maximum Rainfall (mm/hr)             | 50     | Maximum Backdrop Height (m)           | 1.500 |
| Maximum Time of Concentration (mins) | 30     | Min Design Depth for Optimisation (m) | 1.200 |
| Foul Sewage (l/s/ha)                 | 0.000  | Min Vel for Auto Design only (m/s)    | 1.00  |
| Volumetric Runoff Coeff.             | 0.480  | Min Slope for Optimisation (1:X)      | 500   |

Designed with Level Soffits





#### Time Area Diagram for Storm

| Time<br>(mins) | Area<br>(ha) | Time<br>(mins) | Area<br>(ha) | Time<br>(mins) | Area<br>(ha) | Time<br>(mins) | Area<br>(ha) | Time<br>(mins) | Area<br>(ha) |
|----------------|--------------|----------------|--------------|----------------|--------------|----------------|--------------|----------------|--------------|
| 0-4            | 0.653        | 8-12           | 2.042        | 16-20          | 5.595        | 24-28          | 3.921        | 32-36          | 1.984        |
| 4-8            | 2.042        | 12-16          | 5.387        | 20-24          | 5.595        | 28-32          | 3.553        |                |              |

Total Area Contributing (ha) = 30.770


Total Pipe Volume (m³) = 3252.257

#### Network Design Table for Storm

| PN    | Length<br>(m) | Fall<br>(m) | Slope<br>(1:X) | I.Area<br>(ha) | T.E.<br>(mins) | Base<br>Flow (l/s) | n     | HYD<br>SECT | DIA<br>(mm) | Section Type | Auto<br>Design  |
|-------|---------------|-------------|----------------|----------------|----------------|--------------------|-------|-------------|-------------|--------------|---|
| 1.000 | 233.000       | 0.110       | 2118.2         | 1.954          | 22.00          | 0.0                | 0.030 | \           | -1          | Pipe/Conduit |  |
| 1.001 | 136.000       | 0.059       | 2305.1         | 0.000          | 0.00           | 0.0                | 0.030 | \           | -1          | Pipe/Conduit |  |
| 2.000 | 99.000        | 0.560       | 176.8          | 1.123          | 22.00          | 0.0                | 0.030 | \           | -3          | Pipe/Conduit |  |
| 1.002 | 224.000       | 0.910       | 246.2          | 0.000          | 0.00           | 0.0                | 0.030 | \           | -2          | Pipe/Conduit |  |

#### Network Results Table

| PN    | Rain<br>(mm/hr) | T.C.<br>(mins) | US/IL<br>(m) | Σ I.Area<br>(ha) | Σ Base<br>Flow (l/s) | Foul<br>(l/s) | Add Flow<br>(l/s) | Vel<br>(m/s) | Cap<br>(l/s) | Flow<br>(l/s) |
|-------|-----------------|----------------|--------------|------------------|----------------------|---------------|-------------------|--------------|--------------|---------------|
| 1.000 | 17.99           | 28.48          | 77.110       | 1.954            | 0.0                  | 0.0           | 0.0               | 0.60         | 2367.2       | 60.9          |
| 1.001 | 17.44           | 30.00          | 77.000       | 1.954            | 0.0                  | 0.0           | 0.0               | 0.57         | 2269.2       | 60.9          |
| 2.000 | 20.40           | 22.91          | 77.120       | 1.123            | 0.0                  | 0.0           | 0.0               | 1.81         | 4855.2       | 39.7          |
| 1.002 | 17.44           | 30.00          | 76.560       | 3.077            | 0.0                  | 0.0           | 0.0               | 2.06         | 14083.3      | 93.0          |


|  |  |   |
|--|--|---|
| Clifton Scannell Emerson Associates                                |  | Page 2  |
| Seefort Lodge<br>Castledawson Avenue, Blackrock<br>Dublin, Ireland | Project:<br>Huntstown data centre facility |  |
| Date 06/05/2021<br>File Existing watercourse.MDX                   | Designed by ZS<br>Checked by CD            |   |
| Innovyze   | Network 2020.1.3                           |   |

### Conduit Sections for Storm

NOTE: Diameters less than 66 refer to section numbers of hydraulic conduits. These conduits are marked by the symbols:- [] box culvert, \ / open channel, oo dual pipe, ooo triple pipe, O egg.






Section numbers < 0 are taken from user conduit table


| Section<br>Number | Conduit<br>Type | Major<br>Dimn.<br>(mm) | Minor<br>Dimn.<br>(mm) | Side<br>Slope<br>(Deg) | Corner<br>Splay<br>(mm) | 4*Hyd<br>Radius<br>(m) | XSect<br>Area<br>(m <sup>2</sup> ) |
|-------------------|-----------------|------------------------|------------------------|------------------------|-------------------------|------------------------|------------------------------------|
| -1                | \ /             | 3368                   | 1626                   |                        |                         | 3.012                  | 3.949                              |
| -2                | \ /             | 3800                   | 2572                   |                        |                         | 3.825                  | 6.829                              |
| -3                | \ /             | 2681                   | 1456                   |                        |                         | 2.457                  | 2.680                              |

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| Clifton Scannell Emerson Associates                                |  | Page 3  |
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| Date 06/05/2021<br>File Existing watercourse.MDX                   | Designed by ZS<br>Checked by CD            |   |
| Innovyze   | Network 2020.1.3                           |   |

Manhole Schedules for Storm

| MH Name | MH CL (m) | MH Depth (m) | MH Connection | MH Diam., L*W (mm) | PN    | Pipe Out Invert Level (m) | Diameter (mm) | PN    | Pipes In Invert Level (m) | Diameter (mm) | Backdrop (mm) |
|---------|-----------|--------------|---------------|--------------------|-------|---------------------------|---------------|-------|---------------------------|---------------|---------------|
| 1       | 78.950    | 1.840        | Junction      |                    | 1.000 | 77.110                    | -1            |       |                           |               |               |
| ST2     | 78.575    | 1.575        | Junction      |                    | 1.001 | 77.000                    | -1            | 1.000 | 77.000                    | -1            |               |
| 2       | 78.650    | 1.530        | Junction      |                    | 2.000 | 77.120                    | -3            |       |                           |               |               |
| ST1     | 78.200    | 1.640        | Junction      |                    | 1.002 | 76.560                    | -2            | 1.001 | 76.941                    | -1            | 1907          |
|         |           |              |               |                    |       |                           |               | 2.000 | 76.560                    | -3            |               |
|         | 77.300    | 1.650        | Open Manhole  | 0                  |       | OUTFALL                   |               | 1.002 | 75.650                    | -2            |               |

| MH Name | Manhole Easting (m) | Manhole Northing (m) | Intersection Easting (m) | Intersection Northing (m) | Manhole Access | Layout (North)  |
|---------|---------------------|----------------------|--------------------------|---------------------------|----------------|---|
| 1       | -363.296            | 185.463              |                          |                           | No Entry       |  |
| ST2     | -586.420            | 118.347              |                          |                           | No Entry       |  |
| 2       | -814.011            | 60.037               |                          |                           | No Entry       |  |
| ST1     | -717.705            | 82.977               |                          |                           | No Entry       |  |
|         | -778.113            | 298.678              |                          |                           | No Entry       |  |

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| Seefort Lodge<br>Castledawson Avenue, Blackrock<br>Dublin, Ireland | Project:<br>Huntstown data centre facility |  |
| Date 06/05/2021<br>File Existing watercourse.MDX                   | Designed by ZS<br>Checked by CD            |   |
| Innovyze   | Network 2020.1.3                           |   |


PIPELINE SCHEDULES for Storm

Upstream Manhole

| PN    | Hyd<br>Sect | Diam<br>(mm) | MH<br>Name | C.Level<br>(m) | I.Level<br>(m) | D.Depth<br>(m) | MH<br>Connection | MH DIAM., L*W<br>(mm) |
|-------|-------------|--------------|------------|----------------|----------------|----------------|------------------|-----------------------|
| 1.000 | \/          | -1           | 1          | 78.950         | 77.110         | 1.740          | Junction         |                       |
| 1.001 | \/          | -1           | ST2        | 78.575         | 77.000         | -0.051         | Junction         |                       |
| 2.000 | \/          | -3           | 2          | 78.650         | 77.120         | 1.430          | Junction         |                       |
| 1.002 | \/          | -2           | ST1        | 78.200         | 76.560         | 1.540          | Junction         |                       |


Downstream Manhole

| PN    | Length<br>(m) | Slope<br>(1:X) | MH<br>Name | C.Level<br>(m) | I.Level<br>(m) | D.Depth<br>(m) | MH<br>Connection | MH DIAM., L*W<br>(mm) |
|-------|---------------|----------------|------------|----------------|----------------|----------------|------------------|-----------------------|
| 1.000 | 233.000       | 2118.2         | ST2        | 78.575         | 77.000         | 1.475          | Junction         |                       |
| 1.001 | 136.000       | 2305.1         | ST1        | 78.200         | 76.941         | -0.367         | Junction         |                       |
| 2.000 | 99.000        | 176.8          | ST1        | 78.200         | 76.560         | 1.540          | Junction         |                       |
| 1.002 | 224.000       | 246.2          |            | 77.300         | 75.650         | 1.550          | Open Manhole     | 0                     |

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| Seefort Lodge<br>Castledawson Avenue, Blackrock<br>Dublin, Ireland | Project:<br>Huntstown data centre facility |  |
| Date 06/05/2021<br>File Existing watercourse.MDX                   | Designed by ZS<br>Checked by CD            |   |
| Innovyze   | Network 2020.1.3                           |   |

Area Summary for Storm

| Pipe<br>Number | PIMP<br>Type | PIMP<br>Name | PIMP<br>(%) | Gross<br>Area (ha) | Imp.<br>Area (ha) | Pipe Total<br>(ha) |
|----------------|--------------|--------------|-------------|--------------------|-------------------|--------------------|
| 1.000          | -            | -            | 10          | 19.540             | 1.954             | 1.954              |
| 1.001          | -            | -            | 10          | 0.000              | 0.000             | 0.000              |
| 2.000          | -            | -            | 10          | 11.230             | 1.123             | 1.123              |
| 1.002          | -            | -            | 10          | 0.000              | 0.000             | 0.000              |
|                |              |              |             | Total              | Total             | Total              |
|                |              |              |             | 30.770             | 3.077             | 3.077              |

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| Seefort Lodge<br>Castledawson Avenue, Blackrock<br>Dublin, Ireland | Project:<br>Huntstown data centre facility |  |
| Date 06/05/2021<br>File Existing watercourse.MDX                   | Designed by ZS<br>Checked by CD            |   |
| Innovyze   | Network 2020.1.3                           |   |

#### Network Classifications for Storm

| PN    | USMH | Pipe | Min Cover | Max Cover | Pipe Type    | MH   | MH    | MH Ring | MH Type  |
|-------|------|------|-----------|-----------|--------------|------|-------|---------|----------|
|       | Name | Dia  | Depth     | Depth     |              | Dia  | Width | Depth   |          |
|       |      | (mm) | (m)       | (m)       |              | (mm) | (mm)  | (m)     |          |
| 1.000 | 1    | -1   | 1.475     | 1.740     | Unclassified |      |       |         | Junction |
| 1.001 | ST2  | -1   | -0.051    | -0.051    | Unclassified |      |       |         | Junction |
| 2.000 | 2    | -3   | 1.430     | 1.540     | Unclassified |      |       |         | Junction |
| 1.002 | ST1  | -2   | 1.540     | 1.550     | Unclassified |      |       |         | Junction |

#### Free Flowing Outfall Details for Storm

| Outfall     | Outfall C. Level | I. Level | Min | D,L           | W    |
|-------------|------------------|----------|-----|---------------|------|
| Pipe Number | Name             | (m)      | (m) | I. Level (mm) | (mm) |
|             |                  |          |     | (m)           |      |

|       |        |        |        |   |   |
|-------|--------|--------|--------|---|---|
| 1.002 | 77.300 | 75.650 | 75.650 | 0 | 0 |
|-------|--------|--------|--------|---|---|

#### Simulation Criteria for Storm

|                                 |       |  |        |
|---------------------------------|-------|--|--------|
| Volumetric Runoff Coeff         | 0.750 | Additional Flow - % of Total Flow          | 10.000 |
| Areal Reduction Factor          | 1.000 | MADD Factor * 10m <sup>3</sup> /ha Storage | 2.000  |
| Hot Start (mins)                | 0     | Inlet Coefficient                          | 0.800  |
| Hot Start Level (mm)            | 0     | Flow per Person per Day (l/per/day)        | 0.000  |
| Manhole Headloss Coeff (Global) | 0.500 | Run Time (mins)                            | 60     |
| Foul Sewage per hectare (l/s)   | 0.000 | Output Interval (mins)                     | 1      |

|                             |   |                              |   |
|-----------------------------|---|------------------------------|---|
| Number of Input Hydrographs | 0 | Number of Storage Structures | 0 |
| Number of Online Controls   | 0 | Number of Time/Area Diagrams | 0 |
| Number of Offline Controls  | 0 | Number of Real Time Controls | 0 |


#### Synthetic Rainfall Details


|                       |                      |                       |        |
|-----------------------|----------------------|-----------------------|--------|
| Rainfall Model        | FSR                  | Profile Type          | Summer |
| Return Period (years) | 100                  | Cv (Summer)           | 0.750  |
| Region                | Scotland and Ireland | Cv (Winter)           | 0.840  |
| M5-60 (mm)            | 16.500               | Storm Duration (mins) | 30     |
| Ratio R               | 0.300                |                       |        |

#### Manhole Headloss for Storm


| PN    | US/MH | US/MH    |
|-------|-------|----------|
|       | Name  | Headloss |
| 1.000 | 1     | 0.000    |
| 1.001 | ST2   | 0.000    |
| 2.000 | 2     | 0.000    |
| 1.002 | ST1   | 0.000    |



| Clifton Scannell Emerson Associates   |      |   |        |  |            |                | Page 7  |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
|---|------|---|--------|--|------------|----------------|---|--------|----------|----------------|--------|-----------|------------|-----------|----------|-------|----|------|-------|--------|--------|-----------|-------|----------|--------|----------|-------|---|-----------|---|------|-------|--------|-------|--|--------|-------|-----|-----------|-------|------|--|--|------|----|--------|-------|-----|-----------|-------|------|--|--|------|----|--------|-------|-----|-----------|-------|------|--|--|------|----|--------|-------|-----|--------|-------|------|--|--|------|----|--|
| Seefort Lodge<br>Castledawson Avenue, Blackrock<br>Dublin, Ireland  |      |   |        | Project:<br>Huntstown data centre facility |            |                |  |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| Date 06/05/2021<br>File Existing watercourse.MDX  |      |   |        | Designed by ZS<br>Checked by CD            |            |                |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| Innovyze  |      |   |        | Network 2020.1.3                           |            |                |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| <u>1 year Return Period Summary of Critical Results by Maximum Level (Rank 1)</u><br><u>for Storm</u>   |      |   |        |  |            |                |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| <u>Simulation Criteria</u>  |      |   |        |  |            |                |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| Areal Reduction Factor  |      | 1.000                                     |        | Additional Flow - % of Total Flow          |            | 10.000         |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| Hot Start (mins)  |      | 0   |        | MADD Factor * 10m³/ha Storage              |            | 2.000          |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| Hot Start Level (mm)  |      | 0   |        | Inlet Coeffiecient                         |            | 0.800          |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| Manhole Headloss Coeff (Global)   |      | 0.500                                     |        | Flow per Person per Day (l/per/day)        |            | 0.000          |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| Foul Sewage per hectare (l/s)   |      | 0.000                                     |        |  |            |                |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| Number of Input Hydrographs 0   |      |   |        | Number of Storage Structures 0             |            |                |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| Number of Online Controls 0   |      |   |        | Number of Time/Area Diagrams 0             |            |                |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| Number of Offline Controls 0  |      |   |        | Number of Real Time Controls 0             |            |                |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| <u>Synthetic Rainfall Details</u>   |      |   |        |  |            |                |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| Rainfall Model  |      | FSR                                       |        | Ratio R                                    |            | 0.300          |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| Region  |      | Scotland and Ireland                      |        | Cv (Summer)                                |            | 0.480          |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| M5-60 (mm)  |      | 16.500                                    |        | Cv (Winter)                                |            | 0.480          |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| Margin for Flood Risk Warning (mm)  |      |   |        | 300.0                                      |            | DVD Status OFF |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| Analysis Timestep   |      |   |        | Fine Inertia                               |            | Status OFF     |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| DTS Status  |      |   |        | ON   |            |                |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| Profile(s)  |      |   |        | Summer and Winter                          |            |                |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| Duration(s) (mins)  |      | 15, 30, 60, 120, 240, 360, 480, 960, 1440 |        |  |            |                |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| Return Period(s) (years)  |      | 1, 30, 100                                |        |  |            |                |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| Climate Change (%)  |      | 10, 10, 10                                |        |  |            |                |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
|   |      |   |        |  |            |                |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| <table><tr><th colspan="2">US/MH</th><th colspan="2">Return Climate</th><th>First (X)</th><th>First (Y)</th><th>First (Z)</th><th>Overflow</th><th>Water</th></tr><tr><th>PN</th><th>Name</th><th>Storm</th><th>Period</th><th>Change</th><th>Surcharge</th><th>Flood</th><th>Overflow</th><th>Act.</th><th>Level</th></tr><tr><td>1.000</td><td>1</td><td>60 Summer</td><td>1</td><td>+10%</td><td></td><td></td><td></td><td></td><td>77.289</td></tr><tr><td>1.001</td><td>ST2</td><td>60 Summer</td><td>1</td><td>+10%</td><td></td><td></td><td></td><td></td><td>77.148</td></tr><tr><td>2.000</td><td>2</td><td>60 Summer</td><td>1</td><td>+10%</td><td></td><td></td><td></td><td></td><td>77.182</td></tr><tr><td>1.002</td><td>ST1</td><td>60 Summer</td><td>1</td><td>+10%</td><td></td><td></td><td></td><td></td><td>76.644</td></tr></table>   |      |   |        |  |            |                |   | US/MH  |          | Return Climate |        | First (X) | First (Y)  | First (Z) | Overflow | Water | PN | Name | Storm | Period | Change | Surcharge | Flood | Overflow | Act.   | Level    | 1.000 | 1 | 60 Summer | 1 | +10% |       |        |       |  | 77.289 | 1.001 | ST2 | 60 Summer | 1     | +10% |  |  |      |    | 77.148 | 2.000 | 2   | 60 Summer | 1     | +10% |  |  |      |    | 77.182 | 1.002 | ST1 | 60 Summer | 1     | +10% |  |  |      |    | 76.644 |       |     |        |       |      |  |  |      |    |  |
| US/MH   |      | Return Climate                            |        | First (X)                                  | First (Y)  | First (Z)      | Overflow  | Water  |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| PN  | Name | Storm                                     | Period | Change                                     | Surcharge  | Flood          | Overflow  | Act.   | Level    |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| 1.000   | 1    | 60 Summer                                 | 1      | +10%                                       |            |                |   |        | 77.289   |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| 1.001   | ST2  | 60 Summer                                 | 1      | +10%                                       |            |                |   |        | 77.148   |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| 2.000   | 2    | 60 Summer                                 | 1      | +10%                                       |            |                |   |        | 77.182   |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| 1.002   | ST1  | 60 Summer                                 | 1      | +10%                                       |            |                |   |        | 76.644   |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
|   |      |   |        |  |            |                |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| <table><tr><th colspan="2">US/MH</th><th>Depth</th><th>Volume</th><th>Flow /</th><th>Half Drain</th><th>Pipe</th><th colspan="2">Level</th></tr><tr><th>PN</th><th>Name</th><th>(m)</th><th>(m³)</th><th>Cap.</th><th>Overflow</th><th>Time</th><th>Flow</th><th>Status</th><th>Exceeded</th></tr><tr><td></td><td></td><td></td><td></td><td></td><td>(l/s)</td><td>(mins)</td><td>(l/s)</td><td></td><td></td></tr><tr><td>1.000</td><td>1</td><td>-1.447</td><td>0.000</td><td>0.02</td><td></td><td></td><td>70.0</td><td>OK</td><td></td></tr><tr><td>1.001</td><td>ST2</td><td>-1.478</td><td>0.000</td><td>0.02</td><td></td><td></td><td>65.8</td><td>OK</td><td></td></tr><tr><td>2.000</td><td>2</td><td>-1.394</td><td>0.000</td><td>0.01</td><td></td><td></td><td>40.5</td><td>OK</td><td></td></tr><tr><td>1.002</td><td>ST1</td><td>-2.488</td><td>0.000</td><td>0.01</td><td></td><td></td><td>98.7</td><td>OK</td><td></td></tr></table> |      |   |        |  |            |                |   | US/MH  |          | Depth          | Volume | Flow /    | Half Drain | Pipe      | Level    |       | PN | Name | (m)   | (m³)   | Cap.   | Overflow  | Time  | Flow     | Status | Exceeded |       |   |           |   |      | (l/s) | (mins) | (l/s) |  |        | 1.000 | 1   | -1.447    | 0.000 | 0.02 |  |  | 70.0 | OK |        | 1.001 | ST2 | -1.478    | 0.000 | 0.02 |  |  | 65.8 | OK |        | 2.000 | 2   | -1.394    | 0.000 | 0.01 |  |  | 40.5 | OK |        | 1.002 | ST1 | -2.488 | 0.000 | 0.01 |  |  | 98.7 | OK |  |
| US/MH   |      | Depth                                     | Volume | Flow /                                     | Half Drain | Pipe           | Level   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| PN  | Name | (m)                                       | (m³)   | Cap.                                       | Overflow   | Time           | Flow  | Status | Exceeded |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
|   |      |   |        |  | (l/s)      | (mins)         | (l/s)   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| 1.000   | 1    | -1.447                                    | 0.000  | 0.02                                       |            |                | 70.0  | OK     |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| 1.001   | ST2  | -1.478                                    | 0.000  | 0.02                                       |            |                | 65.8  | OK     |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| 2.000   | 2    | -1.394                                    | 0.000  | 0.01                                       |            |                | 40.5  | OK     |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| 1.002   | ST1  | -2.488                                    | 0.000  | 0.01                                       |            |                | 98.7  | OK     |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
|   |      |   |        |  |            |                |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |
| ©1982-2020 Innovyze   |      |   |        |  |            |                |   |        |          |                |        |           |            |           |          |       |    |      |       |        |        |           |       |          |        |          |       |   |           |   |      |       |        |       |  |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |           |       |      |  |  |      |    |        |       |     |        |       |      |  |  |      |    |  |

|  |            |   |               |  |                 |                              |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
|--|------------|---|---------------|--|-----------------|------------------------------|---|---------------|----------|-----------|------------|--|---------|--|------------|--|------|--|-------|-------|------------|--------|---------------|----------------|-----------------|-----------------|--------------------|---------------|--|-----------|-------|------|-----------|------|------|-------|--------|-------|--------|----------|--------|-------|-----|-----------|-------|------|--|--|-------|----|--|--------|-------|-----|-----------|-------|------|--|--|-------|----|--|--------|-------|-----|-----------|-------|------|--|--|------|----|--|--------|-------|-----|--------|-------|------|--|--|-------|----|--|--|
| Clifton Scannell Emerson Associates  |            |   |               |  |                 |                              | Page 8  |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| Seefort Lodge<br>Castledawson Avenue, Blackrock<br>Dublin, Ireland   |            |   |               | Project:<br>Huntstown data centre facility |                 |                              |  |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| Date 06/05/2021  |            | Designed by ZS                            |               |  |                 |                              |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| File Existing watercourse.MDX  |            | Checked by CD                             |               |  |                 |                              |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| Innovyze   |            |   |               | Network 2020.1.3                           |                 |                              |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| <u>30 year Return Period Summary of Critical Results by Maximum Level (Rank 1)</u><br><u>for Storm</u>   |            |   |               |  |                 |                              |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| <u>Simulation Criteria</u>   |            |   |               |  |                 |                              |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| Areal Reduction Factor   |            | 1.000                                     |               | Additional Flow - % of Total Flow          |                 | 10.000                       |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| Hot Start (mins)   |            | 0   |               | MADD Factor * 10m³/ha Storage              |                 | 2.000                        |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| Hot Start Level (mm)   |            | 0   |               | Inlet Coeffiecient                         |                 | 0.800                        |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| Manhole Headloss Coeff (Global)  |            | 0.500                                     |               | Flow per Person per Day (l/per/day)        |                 | 0.000                        |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| Foul Sewage per hectare (l/s)  |            | 0.000                                     |               |  |                 |                              |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| Number of Input Hydrographs  |            |   |               | 0  |                 | Number of Storage Structures |   | 0             |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| Number of Online Controls  |            |   |               | 0  |                 | Number of Time/Area Diagrams |   | 0             |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| Number of Offline Controls   |            |   |               | 0  |                 | Number of Real Time Controls |   | 0             |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| <u>Synthetic Rainfall Details</u>  |            |   |               |  |                 |                              |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| Rainfall Model   |            | FSR                                       |               | Ratio R                                    |                 | 0.300                        |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| Region   |            | Scotland and Ireland                      |               | Cv (Summer)                                |                 | 0.480                        |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| M5-60 (mm)   |            | 16.500                                    |               | Cv (Winter)                                |                 | 0.480                        |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| Margin for Flood Risk Warning (mm)   |            |   |               | 300.0                                      |                 | DVD Status                   |   | OFF           |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| Analysis Timestep  |            |   |               | Fine                                       |                 | Inertia Status               |   | OFF           |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| DTS Status   |            |   |               | ON   |                 |                              |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| Profile(s)   |            |   |               | Summer and Winter                          |                 |                              |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| Duration(s) (mins)   |            | 15, 30, 60, 120, 240, 360, 480, 960, 1440 |               |  |                 |                              |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| Return Period(s) (years)   |            | 1, 30, 100                                |               |  |                 |                              |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| Climate Change (%)   |            | 10, 10, 10                                |               |  |                 |                              |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
|  |            |   |               |  |                 |                              |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| <table><tr><td colspan="2"></td><td colspan="2"></td><td colspan="2"></td><td colspan="2"></td><td colspan="2"></td><td>Water</td></tr><tr><td>PN</td><td>US/MH Name</td><td>Storm</td><td>Return Period</td><td>Climate Change</td><td>First (X) Surge</td><td>First (Y) Flood</td><td>First (Z) Overflow</td><td>Overflow Act.</td><td></td><td>Level (m)</td></tr><tr><td>1.000</td><td>1</td><td>60 Summer</td><td>30</td><td>+10%</td><td></td><td></td><td></td><td></td><td></td><td>77.388</td></tr><tr><td>1.001</td><td>ST2</td><td>60 Summer</td><td>30</td><td>+10%</td><td></td><td></td><td></td><td></td><td></td><td>77.238</td></tr><tr><td>2.000</td><td>2</td><td>60 Summer</td><td>30</td><td>+10%</td><td></td><td></td><td></td><td></td><td></td><td>77.255</td></tr><tr><td>1.002</td><td>ST1</td><td>60 Summer</td><td>30</td><td>+10%</td><td></td><td></td><td></td><td></td><td></td><td>76.742</td></tr></table>  |            |   |               |  |                 |                              |   |               |          |           |            |  |         |  |            |  |      |  | Water | PN    | US/MH Name | Storm  | Return Period | Climate Change | First (X) Surge | First (Y) Flood | First (Z) Overflow | Overflow Act. |  | Level (m) | 1.000 | 1    | 60 Summer | 30   | +10% |       |        |       |        |          | 77.388 | 1.001 | ST2 | 60 Summer | 30    | +10% |  |  |       |    |  | 77.238 | 2.000 | 2   | 60 Summer | 30    | +10% |  |  |       |    |  | 77.255 | 1.002 | ST1 | 60 Summer | 30    | +10% |  |  |      |    |  | 76.742 |       |     |        |       |      |  |  |       |    |  |  |
|  |            |   |               |  |                 |                              |   |               |          | Water     |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| PN   | US/MH Name | Storm                                     | Return Period | Climate Change                             | First (X) Surge | First (Y) Flood              | First (Z) Overflow  | Overflow Act. |          | Level (m) |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| 1.000  | 1          | 60 Summer                                 | 30            | +10%                                       |                 |                              |   |               |          | 77.388    |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| 1.001  | ST2        | 60 Summer                                 | 30            | +10%                                       |                 |                              |   |               |          | 77.238    |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| 2.000  | 2          | 60 Summer                                 | 30            | +10%                                       |                 |                              |   |               |          | 77.255    |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| 1.002  | ST1        | 60 Summer                                 | 30            | +10%                                       |                 |                              |   |               |          | 76.742    |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
|  |            |   |               |  |                 |                              |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| <table><tr><td colspan="2"></td><td colspan="2">Surcharged</td><td colspan="2">Flooded</td><td colspan="2">Half Drain</td><td colspan="2">Pipe</td><td></td></tr><tr><td>US/MH</td><td>Depth</td><td>Volume</td><td>Flow /</td><td>Overflow</td><td>Time</td><td>Flow</td><td>Level</td><td colspan="3"></td></tr><tr><td>PN</td><td>Name</td><td>(m)</td><td>(m³)</td><td>Cap.</td><td>(l/s)</td><td>(mins)</td><td>(l/s)</td><td>Status</td><td>Exceeded</td><td></td></tr><tr><td>1.000</td><td>1</td><td>-1.348</td><td>0.000</td><td>0.04</td><td></td><td></td><td>148.4</td><td>OK</td><td></td><td></td></tr><tr><td>1.001</td><td>ST2</td><td>-1.388</td><td>0.000</td><td>0.04</td><td></td><td></td><td>140.8</td><td>OK</td><td></td><td></td></tr><tr><td>2.000</td><td>2</td><td>-1.321</td><td>0.000</td><td>0.02</td><td></td><td></td><td>88.4</td><td>OK</td><td></td><td></td></tr><tr><td>1.002</td><td>ST1</td><td>-2.390</td><td>0.000</td><td>0.02</td><td></td><td></td><td>215.0</td><td>OK</td><td></td><td></td></tr></table> |            |   |               |  |                 |                              |   |               |          |           | Surcharged |  | Flooded |  | Half Drain |  | Pipe |  |       | US/MH | Depth      | Volume | Flow /        | Overflow       | Time            | Flow            | Level              |               |  |           | PN    | Name | (m)       | (m³) | Cap. | (l/s) | (mins) | (l/s) | Status | Exceeded |        | 1.000 | 1   | -1.348    | 0.000 | 0.04 |  |  | 148.4 | OK |  |        | 1.001 | ST2 | -1.388    | 0.000 | 0.04 |  |  | 140.8 | OK |  |        | 2.000 | 2   | -1.321    | 0.000 | 0.02 |  |  | 88.4 | OK |  |        | 1.002 | ST1 | -2.390 | 0.000 | 0.02 |  |  | 215.0 | OK |  |  |
|  |            | Surcharged                                |               | Flooded                                    |                 | Half Drain                   |   | Pipe          |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| US/MH  | Depth      | Volume                                    | Flow /        | Overflow                                   | Time            | Flow                         | Level   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| PN   | Name       | (m)                                       | (m³)          | Cap.                                       | (l/s)           | (mins)                       | (l/s)   | Status        | Exceeded |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| 1.000  | 1          | -1.348                                    | 0.000         | 0.04                                       |                 |                              | 148.4   | OK            |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| 1.001  | ST2        | -1.388                                    | 0.000         | 0.04                                       |                 |                              | 140.8   | OK            |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| 2.000  | 2          | -1.321                                    | 0.000         | 0.02                                       |                 |                              | 88.4  | OK            |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| 1.002  | ST1        | -2.390                                    | 0.000         | 0.02                                       |                 |                              | 215.0   | OK            |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
|  |            |   |               |  |                 |                              |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |
| ©1982-2020 Innovyze  |            |   |               |  |                 |                              |   |               |          |           |            |  |         |  |            |  |      |  |       |       |            |        |               |                |                 |                 |                    |               |  |           |       |      |           |      |      |       |        |       |        |          |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |       |    |  |        |       |     |           |       |      |  |  |      |    |  |        |       |     |        |       |      |  |  |       |    |  |  |



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|--|--|---|
| Clifton Scannell Emerson Associates                                |  | Page 1  |
| Seefort Lodge<br>Castledawson Avenue, Blackrock<br>Dublin, Ireland | Project:<br>Huntstown data centre facility |  |
| Date 06/05/2021<br>Proposed watercourse diversion                  | Designed by ZS<br>Checked by CD            |   |
| Innovyze   | Network 2020.1.3                           |   |

### STORM SEWER DESIGN by the Modified Rational Method

#### Design Criteria for Storm

Pipe Sizes STANDARD Manhole Sizes STANDARD

FSR Rainfall Model - Scotland and Ireland

|                                      |        |                                       |       |
|--------------------------------------|--------|---------------------------------------|-------|
| Return Period (years)                | 1      | PIMP (%)                              | 10    |
| M5-60 (mm)                           | 16.500 | Add Flow / Climate Change (%)         | 0     |
| Ratio R                              | 0.300  | Minimum Backdrop Height (m)           | 0.175 |
| Maximum Rainfall (mm/hr)             | 50     | Maximum Backdrop Height (m)           | 1.500 |
| Maximum Time of Concentration (mins) | 30     | Min Design Depth for Optimisation (m) | 1.200 |
| Foul Sewage (l/s/ha)                 | 0.000  | Min Vel for Auto Design only (m/s)    | 1.00  |
| Volumetric Runoff Coeff.             | 0.480  | Min Slope for Optimisation (1:X)      | 500   |

Designed with Level Soffits

#### Time Area Diagram for Storm

| Time<br>(mins) | Area<br>(ha) | Time<br>(mins) | Area<br>(ha) | Time<br>(mins) | Area<br>(ha) | Time<br>(mins) | Area<br>(ha) | Time<br>(mins) | Area<br>(ha) |
|----------------|--------------|----------------|--------------|----------------|--------------|----------------|--------------|----------------|--------------|
| 0-4            | 0.000        | 8-12           | 4.246        | 16-20          | 4.358        | 24-28          | 4.358        | 32-36          | 0.915        |
| 4-8            | 4.561        | 12-16          | 4.358        | 20-24          | 4.358        | 28-32          | 3.615        |                |              |

Total Area Contributing (ha) = 30.770

Total Pipe Volume (m³) = 1768.069


#### Network Design Table for Storm

| PN    | Length<br>(m) | Fall<br>(m) | Slope<br>(1:X) | I.Area<br>(ha) | T.E.<br>(mins) | Base<br>Flow (l/s) | k<br>(mm) | n     | HYD<br>SECT | DIA<br>(mm) | Section Type | Auto<br>Design |
|-------|---------------|-------------|----------------|----------------|----------------|--------------------|-----------|-------|-------------|-------------|--------------|----------------|
| 1.000 | 233.000       | 0.110       | 2118.2         | 1.954          | 22.00          | 0.0                |           | 0.030 | \           | -1          | Pipe/Conduit | ✓              |
| 1.001 | 65.000        | 0.540       | 120.4          | 0.000          | 0.00           | 0.0                |           | 0.030 | \           | -1          | Pipe/Conduit | ✓              |
| 2.000 | 67.000        | 0.339       | 197.6          | 0.443          | 22.00          | 0.0                |           | 0.030 | \           | -3          | Pipe/Conduit | ✓              |
| 2.001 | 25.000        | 0.126       | 198.4          | 0.165          | 0.00           | 0.0                | 0.600     |       | o           | -4          | Pipe/Conduit | ✓              |
| 2.002 | 7.000         | 0.095       | 73.7           | 0.515          | 0.00           | 0.0                |           | 0.030 | \           | -3          | Pipe/Conduit | ✓              |

#### Network Results Table









| PN    | Rain<br>(mm/hr) | T.C.<br>(mins) | US/IL<br>(m) | Σ I.Area<br>(ha) | Σ Base<br>Flow (l/s) | Foul<br>(l/s) | Add Flow<br>(l/s) | Vel<br>(m/s) | Cap<br>(l/s) | Flow<br>(l/s) |
|-------|-----------------|----------------|--------------|------------------|----------------------|---------------|-------------------|--------------|--------------|---------------|
| 1.000 | 17.99           | 28.48          | 77.110       | 1.954            | 0.0                  | 0.0           | 0.0               | 0.60         | 2367.2       | 60.9          |
| 1.001 | 17.83           | 28.91          | 77.000       | 1.954            | 0.0                  | 0.0           | 0.0               | 2.51         | 9930.3       | 60.9          |
| 2.000 | 20.53           | 22.65          | 77.120       | 0.443            | 0.0                  | 0.0           | 0.0               | 1.71         | 4591.9       | 15.8          |
| 2.001 | 20.43           | 22.84          | 76.781       | 0.608            | 0.0                  | 0.0           | 0.0               | 2.22         | 1412.9       | 21.5          |
| 2.002 | 20.41           | 22.88          | 76.655       | 1.123            | 0.0                  | 0.0           | 0.0               | 2.81         | 7520.5       | 39.7          |




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| Clifton Scannell Emerson Associates                                |  | Page 3  |
| Seefort Lodge<br>Castledawson Avenue, Blackrock<br>Dublin, Ireland | Project:<br>Huntstown data centre facility |  |
| Date 06/05/2021<br>File Proposed watercourse di...                 | Designed by ZS<br>Checked by CD            |   |
| Innovyze   | Network 2020.1.3                           |   |

Manhole Schedules for Storm

| MH Name | MH CL (m) | MH Depth (m) | MH Connection | MH Diam., L*W (mm) | PN    | Pipe Out Invert Level (m) | Diameter (mm) | PN    | Pipes In Invert Level (m) | Diameter (mm) | Backdrop (mm) |
|---------|-----------|--------------|---------------|--------------------|-------|---------------------------|---------------|-------|---------------------------|---------------|---------------|
| 1       | 78.950    | 1.840        | Junction      |                    | 1.000 | 77.110                    | -1            |       |                           |               |               |
| ST2     | 78.725    | 1.725        | Junction      |                    | 1.001 | 77.000                    | -1            | 1.000 | 77.000                    | -1            |               |
| 2       | 78.650    | 1.530        | Junction      |                    | 2.000 | 77.120                    | -3            |       |                           |               |               |
| HW-10   | 78.610    | 1.829        | Junction      |                    | 2.001 | 76.781                    | -4            | 2.000 | 76.781                    | -3            |               |
| HW-11   | 78.520    | 1.865        | Junction      |                    | 2.002 | 76.655                    | -3            | 2.001 | 76.655                    | -4            |               |
| ST1     | 78.510    | 1.950        | Junction      |                    | 2.003 | 76.560                    | -3            | 2.002 | 76.560                    | -3            |               |
| HW-8    | 78.500    | 2.040        | Junction      |                    | 1.002 | 76.460                    | -4            | 1.001 | 76.460                    | -1            |               |
|         |           |              |               |                    |       |                           |               | 2.003 | 76.460                    | -3            |               |
| DIV-01  | 78.441    | 2.191        | Open Manhole  | 3000               | 1.003 | 76.250                    | -4            | 1.002 | 76.450                    | -4            | 200           |
| DIV-02  | 77.550    | 1.624        | Open Manhole  | 3000               | 1.004 | 75.926                    | -4            | 1.003 | 75.926                    | -4            |               |
| DIV-03  | 77.702    | 1.902        | Open Manhole  | 3000               | 1.005 | 75.800                    | -4            | 1.004 | 75.800                    | -4            |               |
| DIV-04  | 77.629    | 1.900        | Open Manhole  | 3000               | 1.006 | 75.729                    | -4            | 1.005 | 75.729                    | -4            |               |
|         | 77.300    | 1.650        | Open Manhole  | 0                  |       | OUTFALL                   |               | 1.006 | 75.650                    | -4            |               |

| MH Name | Manhole Easting (m) | Manhole Northing (m) | Intersection Easting (m) | Intersection Northing (m) | Manhole Access | Layout (North)  |
|---------|---------------------|----------------------|--------------------------|---------------------------|----------------|---|
| 1       | -437.033            | 133.145              |                          |                           | No Entry       |  |
| ST2     | -669.625            | 146.923              |                          |                           | No Entry       |  |
| 2       | -903.933            | 150.334              |                          |                           | No Entry       |  |
| HW-10   | -836.933            | 150.204              |                          |                           | No Entry       |  |
| HW-11   | -811.937            | 149.812              |                          |                           | No Entry       |  |
| ST1     | -804.937            | 149.846              |                          |                           | No Entry       |  |
| HW-8    | -734.123            | 154.987              |                          |                           | No Entry       |  |
| DIV-01  | -735.111            | 160.905              | -735.111                 | 160.905                   | Required       |  |




|  |  |   |
|--|--|---|
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Area Summary for Storm

| Pipe<br>Number | PIMP<br>Type | PIMP<br>Name | PIMP<br>(%) | Gross<br>Area (ha) | Imp.<br>Area (ha) | Pipe Total<br>(ha) |
|----------------|--------------|--------------|-------------|--------------------|-------------------|--------------------|
| 1.000          | -            | -            | 10          | 19.540             | 1.954             | 1.954              |
| 1.001          | -            | -            | 10          | 0.000              | 0.000             | 0.000              |
| 2.000          | -            | -            | 10          | 4.430              | 0.443             | 0.443              |
| 2.001          | -            | -            | 10          | 1.650              | 0.165             | 0.165              |
| 2.002          | -            | -            | 10          | 5.150              | 0.515             | 0.515              |
| 2.003          | -            | -            | 10          | 0.000              | 0.000             | 0.000              |
| 1.002          | -            | -            | 10          | 0.000              | 0.000             | 0.000              |
| 1.003          | -            | -            | 10          | 0.000              | 0.000             | 0.000              |
| 1.004          | -            | -            | 10          | 0.000              | 0.000             | 0.000              |
| 1.005          | -            | -            | 10          | 0.000              | 0.000             | 0.000              |
| 1.006          | -            | -            | 10          | 0.000              | 0.000             | 0.000              |
|                |              |              |             | Total              | Total             | Total              |
|                |              |              |             | 30.770             | 3.077             | 3.077              |



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| Innovyze   |                          |                                     |                           |                           | Network 2020.1.3                           |                   |                     |                         |              |
| <u>Network Classifications for Storm</u>                           |                          |                                     |                           |                           |  |                   |                     |                         |              |
| PN   | USMH<br>Name             | Pipe<br>Dia<br>(mm)                 | Min Cover<br>Depth<br>(m) | Max Cover<br>Depth<br>(m) | Pipe Type                                  | MH<br>Dia<br>(mm) | MH<br>Width<br>(mm) | MH Ring<br>Depth<br>(m) | MH Type      |
| 1.000  | 1                        | -1                                  | 1.625                     | 1.740                     | Unclassified                               |                   |                     |                         | Junction     |
| 1.001  | ST2                      | -1                                  | 1.625                     | 1.940                     | Unclassified                               |                   |                     |                         | Junction     |
| 2.000  | 2                        | -3                                  | 1.430                     | 1.729                     | Unclassified                               |                   |                     |                         | Junction     |
| 2.001  | HW-10                    | -4                                  | 1.729                     | 1.765                     | Unclassified                               |                   |                     |                         | Junction     |
| 2.002  | HW-11                    | -3                                  | 1.765                     | 1.850                     | Unclassified                               |                   |                     |                         | Junction     |
| 2.003  | ST1                      | -3                                  | 1.850                     | 1.940                     | Unclassified                               |                   |                     |                         | Junction     |
| 1.002  | HW-8                     | -4                                  | 1.891                     | 1.940                     | Unclassified                               |                   |                     |                         | Junction     |
| 1.003  | DIV-01                   | -4                                  | 1.524                     | 2.091                     | Unclassified                               | 3000              | 0                   | 2.091                   | Unclassified |
| 1.004  | DIV-02                   | -4                                  | 1.524                     | 1.802                     | Unclassified                               | 3000              | 0                   | 1.524                   | Unclassified |
| 1.005  | DIV-03                   | -4                                  | 1.800                     | 1.802                     | Unclassified                               | 3000              | 0                   | 1.802                   | Unclassified |
| 1.006  | DIV-04                   | -4                                  | 1.550                     | 1.800                     | Unclassified                               | 3000              | 0                   | 1.800                   | Unclassified |
| <u>Free Flowing Outfall Details for Storm</u>                      |                          |                                     |                           |                           |  |                   |                     |                         |              |
| Outfall<br>Pipe Number   | Outfall C. Level<br>Name | I. Level<br>(m)                     | Min<br>I. Level<br>(m)    | D,L<br>(mm)               | W<br>(mm)                                  |                   |                     |                         |              |
| 1.006  | 77.300                   | 75.650                              | 75.650                    | 0                         | 0  |                   |                     |                         |              |
| <u>Simulation Criteria for Storm</u>                               |                          |                                     |                           |                           |  |                   |                     |                         |              |
| Volumetric Runoff Coeff  | 0.750                    | Additional Flow - % of Total Flow   | 10.000                    |                           |  |                   |                     |                         |              |
| Areal Reduction Factor   | 1.000                    | MADD Factor * 10m³/ha               | Storage                   | 2.000                     |  |                   |                     |                         |              |
| Hot Start (mins)   | 0                        | Inlet Coefficient                   | 0.800                     |                           |  |                   |                     |                         |              |
| Hot Start Level (mm)   | 0                        | Flow per Person per Day (l/per/day) | 0.000                     |                           |  |                   |                     |                         |              |
| Manhole Headloss Coeff (Global)                                    | 0.500                    | Run Time (mins)                     | 60                        |                           |  |                   |                     |                         |              |
| Foul Sewage per hectare (l/s)                                      | 0.000                    | Output Interval (mins)              | 1                         |                           |  |                   |                     |                         |              |
| Number of Input Hydrographs  | 0                        | Number of Storage Structures        | 0                         |                           |  |                   |                     |                         |              |
| Number of Online Controls  | 0                        | Number of Time/Area Diagrams        | 0                         |                           |  |                   |                     |                         |              |
| Number of Offline Controls   | 0                        | Number of Real Time Controls        | 0                         |                           |  |                   |                     |                         |              |
| <u>Synthetic Rainfall Details</u>                                  |                          |                                     |                           |                           |  |                   |                     |                         |              |
| Rainfall Model   | FSR                      | Profile Type                        | Summer                    |                           |  |                   |                     |                         |              |
| Return Period (years)  | 100                      | Cv (Summer)                         | 0.750                     |                           |  |                   |                     |                         |              |
| Region   | Scotland and Ireland     | Cv (Winter)                         | 0.840                     |                           |  |                   |                     |                         |              |
| M5-60 (mm)   | 16.500                   | Storm Duration (mins)               | 30                        |                           |  |                   |                     |                         |              |
| Ratio R  | 0.300                    |                                     |                           |                           |  |                   |                     |                         |              |
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| Date 06/05/2021<br>File Proposed watercourse di...                 | Designed by ZS<br>Checked by CD            |   |
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Manhole Headloss for Storm

| PN    | US/MH<br>Name | US/MH<br>Headloss |
|-------|---------------|-------------------|
| 1.000 | 1             | 0.000             |
| 1.001 | ST2           | 0.000             |
| 2.000 | 2             | 0.000             |
| 2.001 | HW-10         | 0.000             |
| 2.002 | HW-11         | 0.000             |
| 2.003 | ST1           | 0.000             |
| 1.002 | HW-8          | 0.000             |
| 1.003 | DIV-01        | 0.500             |
| 1.004 | DIV-02        | 0.500             |
| 1.005 | DIV-03        | 0.500             |
| 1.006 | DIV-04        | 0.500             |

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Seefort Lodge

Castledawson Avenue, Blackrock

Dublin, Ireland

Project:

Huntstown data centre facility

Date 06/05/2021

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Micro Drainage

1 year Return Period Summary of Critical Results by Maximum Level (Rank 1)

for Storm

Simulation Criteria

Areal Reduction Factor

1.000

Additional Flow - % of Total Flow

10.000

Hot Start (mins)

0

MADD Factor \* 10m³/ha Storage

2.000

Hot Start Level (mm)

0

Inlet Coefficient

0.800

Manhole Headloss Coeff (Global)

0.500

Flow per Person per Day (l/per/day)

0.000

Foul Sewage per hectare (l/s)

0.000

Number of Input Hydrographs

0

Number of Storage Structures

0

Number of Online Controls

0

Number of Time/Area Diagrams

0

Number of Offline Controls

0

Number of Real Time Controls

0

Synthetic Rainfall Details

Rainfall Model

FSR

Ratio R

0.300

Region

Scotland and Ireland

Cv (Summer)

0.480

M5-60 (mm)

16.500

Cv (Winter)

0.480

Margin for Flood Risk Warning (mm)

300.0

DVD Status

OFF

Analysis Timestep

Fine

Inertia Status

OFF

DTS Status

ON

Profile(s)

Summer and Winter

Duration(s) (mins)

15, 30, 60, 120, 240, 360, 480, 960, 1440

Return Period(s) (years)

1, 30, 100

Climate Change (%)

10, 10, 10

Water

US/MH

Return

Climate

First (X)

First (Y)

First (Z)

Overflow

Level

PN

Name

Storm

Period

Change

Surcharge

Flood

Overflow

Act.

(m)

1.000

1

60 Summer

1

+10%

77.272

1.001

ST2

60 Summer

1

+10%

77.055

2.000

2

60 Summer

1

+10%

77.146

2.001

HW-10

30 Summer

1

+10%

76.851

2.002

HW-11

30 Summer

1

+10%

76.753

2.003

ST1

30 Summer

1

+10%

76.746

1.002

HW-8

60 Summer

1

+10%

76.662

1.003

DIV-01

60 Summer

1

+10%

76.444

1.004

DIV-02

60 Summer

1

+10%

76.176

1.005

DIV-03

60 Summer

1

+10%

76.088

1.006

DIV-04

60 Summer

1

+10%

76.051

Level

US/MH

Depth

Volume

Flow / Overflow

Half Drain

Pipe

Level

PN

Name

(m)

(m³)

Cap.

(l/s)

(mins)

Flow

Status

Exceeded

1.000

1

-1.464

0.000

0.02

70.2

OK

1.001

ST2

-1.571

0.000

0.01

70.1

OK

2.000

2

-1.430

0.000

0.00

16.0

OK

2.001

HW-10

-0.830


0.000

0.03

23.9

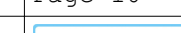
OK\*

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1 year Return Period Summary of Critical Results by Maximum Level (Rank 1)  
for Storm

| PN    | US/MH<br>Name | Surcharged   |                | Flooded        |                   | Half Drain     |               | Pipe   | Level<br>Exceeded |  |
|-------|---------------|--------------|----------------|----------------|-------------------|----------------|---------------|--------|-------------------|--|
|       |               | Depth<br>(m) | Volume<br>(m³) | Flow /<br>Cap. | Overflow<br>(l/s) | Time<br>(mins) | Flow<br>(l/s) | Status |                   |  |
| 2.002 | HW-11         | -1.358       | 0.000          | 0.01           |                   |                | 56.8          | OK     |                   |  |
| 2.003 | ST1           | -1.270       | 0.000          | 0.02           |                   |                | 55.7          | OK     |                   |  |
| 1.002 | HW-8          | -0.698       | 0.000          | 0.11           |                   |                | 102.1         | OK*    |                   |  |
| 1.003 | DIV-01        | -0.706       | 0.000          | 0.12           |                   |                | 100.6         | OK     |                   |  |
| 1.004 | DIV-02        | -0.650       | 0.000          | 0.13           |                   |                | 97.1          | OK     |                   |  |
| 1.005 | DIV-03        | -0.612       | 0.000          | 0.14           |                   |                | 96.1          | OK     |                   |  |
| 1.006 | DIV-04        | -0.578       | 0.000          | 0.28           |                   |                | 95.9          | OK     |                   |  |

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### 30 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for Storm

### Simulation Criteria

|  |  |   |
|--|--|---|
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| Innovyze   | Network 2020.1.3                           |   |

30 year Return Period Summary of Critical Results by Maximum Level (Rank 1)  
for Storm

| PN    | US/MH<br>Name | Surcharged   | Flooded        | Flow /<br>Cap. | Overflow<br>(l/s) | Half Drain     | Pipe          | Status | Level<br>Exceeded |
|-------|---------------|--------------|----------------|----------------|-------------------|----------------|---------------|--------|-------------------|
|       |               | Depth<br>(m) | Volume<br>(m³) |                |                   | Time<br>(mins) | Flow<br>(l/s) |        |                   |
| 2.002 | HW-11         | -1.261       | 0.000          | 0.02           |                   |                | 130.1         | OK     |                   |
| 2.003 | ST1           | -1.172       | 0.000          | 0.05           |                   |                | 124.5         | OK     |                   |
| 1.002 | HW-8          | -0.613       | 0.000          | 0.23           |                   |                | 217.8         | OK*    |                   |
| 1.003 | DIV-01        | -0.594       | 0.000          | 0.26           |                   |                | 214.7         | OK     |                   |
| 1.004 | DIV-02        | -0.487       | 0.000          | 0.27           |                   |                | 204.0         | OK     |                   |
| 1.005 | DIV-03        | -0.434       | 0.000          | 0.29           |                   |                | 202.5         | OK     |                   |
| 1.006 | DIV-04        | -0.398       | 0.000          | 0.59           |                   |                | 202.2         | OK     |                   |

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Seefort Lodge

Castledawson Avenue, Blackrock

Dublin, Ireland

Date 06/05/2021

File Proposed watercourse di...

Project:

Huntstown data centre facility

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100 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for Storm

Simulation Criteria

Areal Reduction Factor

1.000

Additional Flow - % of Total Flow

10.000

Hot Start (mins)

0

MADD Factor \* 10m³/ha Storage

2.000

Hot Start Level (mm)

0

Inlet Coeffiecient

0.800

Manhole Headloss Coeff (Global)

0.500

Flow per Person per Day (l/per/day)

0.000

Foul Sewage per hectare (l/s)

0.000

Number of Input Hydrographs

0

Number of Storage Structures

0

Number of Online Controls

0

Number of Time/Area Diagrams

0

Number of Offline Controls

0

Number of Real Time Controls

0

Synthetic Rainfall Details

Rainfall Model

FSR

Ratio R

0.300

Region Scotland and Ireland Cv (Summer)

0.480

M5-60 (mm)

16.500

Cv (Winter)

0.480

Margin for Flood Risk Warning (mm)

300.0

DVD Status

OFF

Analysis Timestep

Fine

Inertia Status

OFF

DTS Status

ON

Profile(s)

Summer and Winter

Duration(s) (mins)

15, 30, 60, 120, 240, 360, 480, 960, 1440

Return Period(s) (years)

1, 30, 100

Climate Change (%)


10, 10, 10

|       | US/MH  |           | Return | Climate | First (X) | First (Y) | First (Z) | Overflow | Water  |
|-------|--------|-----------|--------|---------|-----------|-----------|-----------|----------|--------|
| PN    | Name   | Storm     | Period | Change  | Surcharge | Flood     | Overflow  | Act.     | Level  |
| 1.000 | 1      | 60 Summer | 100    | +10%    |           |           |           |          | 77.404 |
| 1.001 | ST2    | 60 Summer | 100    | +10%    |           |           |           |          | 77.154 |
| 2.000 | 2      | 60 Summer | 100    | +10%    |           |           |           |          | 77.193 |
| 2.001 | HW-10  | 30 Summer | 100    | +10%    |           |           |           |          | 76.931 |
| 2.002 | HW-11  | 30 Summer | 100    | +10%    |           |           |           |          | 76.893 |
| 2.003 | ST1    | 30 Summer | 100    | +10%    |           |           |           |          | 76.888 |
| 1.002 | HW-8   | 60 Summer | 100    | +10%    |           |           |           |          | 76.776 |
| 1.003 | DIV-01 | 60 Summer | 100    | +10%    |           |           |           |          | 76.600 |
| 1.004 | DIV-02 | 60 Summer | 100    | +10%    |           |           |           |          | 76.425 |
| 1.005 | DIV-03 | 60 Summer | 100    | +10%    |           |           |           |          | 76.358 |
| 1.006 | DIV-04 | 60 Summer | 100    | +10%    |           |           |           |          | 76.322 |

|       | US/MH | Depth  | Volume | Flow / | Half Drain | Pipe   |       | Level    |
|-------|-------|--------|--------|--------|------------|--------|-------|----------|
| PN    | Name  | (m)    | (m³)   | Cap.   | Overflow   | Time   | Flow  | Exceeded |
|       |       |        |        |        | (l/s)      | (mins) | (l/s) | Status   |
| 1.000 | 1     | -1.332 | 0.000  | 0.06   |            |        | 199.9 | OK       |
| 1.001 | ST2   | -1.472 | 0.000  | 0.02   |            |        | 197.6 | OK       |
| 2.000 | 2     | -1.383 | 0.000  | 0.01   |            |        | 45.3  | OK       |
| 2.001 | HW-10 | -0.750 | 0.000  | 0.07   |            |        | 70.1  | OK*      |

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100 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for Storm

| PN    | US/MH<br>Name | Surcharged   | Flooded        | Flow /<br>Cap. | Overflow<br>(l/s) | Half Drain     | Pipe          | Status | Level<br>Exceeded |
|-------|---------------|--------------|----------------|----------------|-------------------|----------------|---------------|--------|-------------------|
|       |               | Depth<br>(m) | Volume<br>(m³) |                |                   | Time<br>(mins) | Flow<br>(l/s) |        |                   |
| 2.002 | HW-11         | -1.218       | 0.000          | 0.03           |                   |                | 168.1         | OK     |                   |
| 2.003 | ST1           | -1.128       | 0.000          | 0.07           |                   |                | 160.5         | OK     |                   |
| 1.002 | HW-8          | -0.584       | 0.000          | 0.29           |                   |                | 275.5         | OK*    |                   |
| 1.003 | DIV-01        | -0.550       | 0.000          | 0.33           |                   |                | 273.4         | OK     |                   |
| 1.004 | DIV-02        | -0.401       | 0.000          | 0.34           |                   |                | 261.3         | OK     |                   |
| 1.005 | DIV-03        | -0.343       | 0.000          | 0.38           |                   |                | 259.3         | OK     |                   |
| 1.006 | DIV-04        | -0.307       | 0.000          | 0.76           |                   |                | 259.0         | OK     |                   |



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Mentec House, Bakers Point, Pottery Road, Dun Laochaire, Co Dublin.

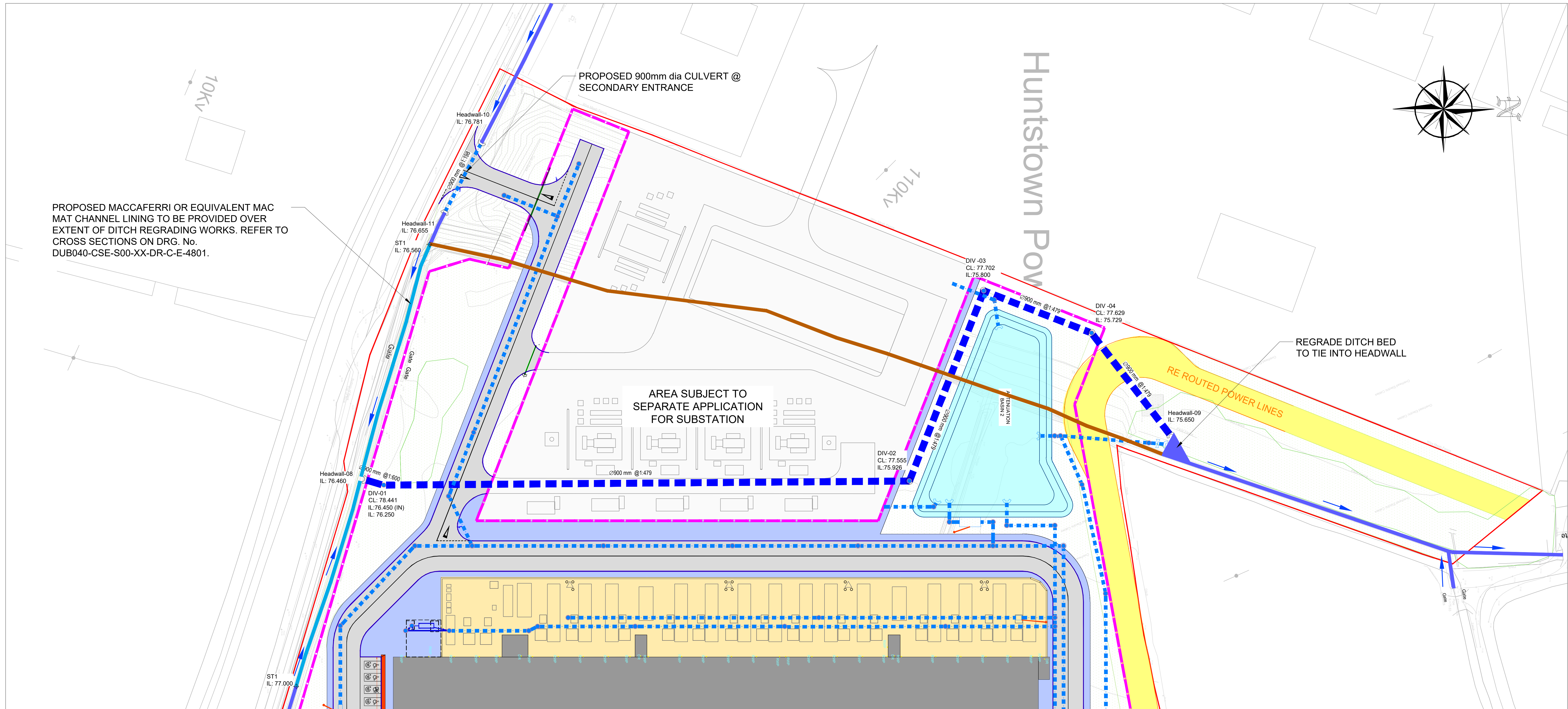
T. +353 1 288 5006 F. +353 1 283 3466 E. [info@csea.ie](mailto:info@csea.ie) W. [www.csea.ie](http://www.csea.ie)



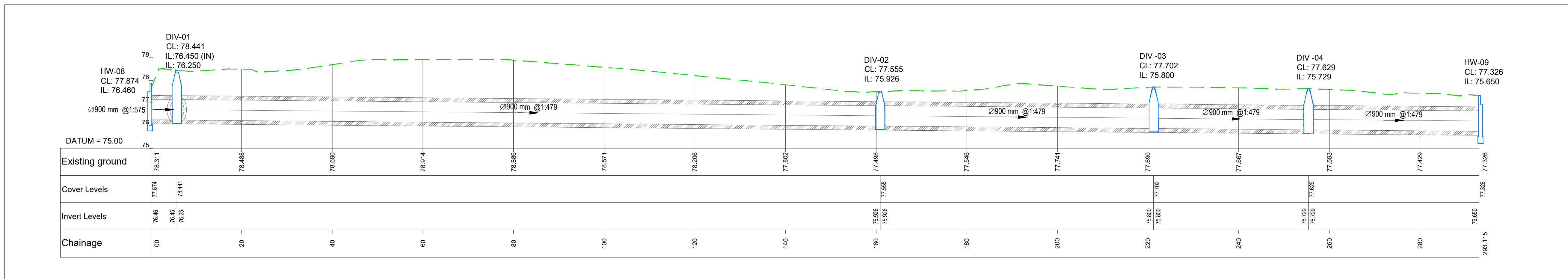
# Appendix B - Huntstown Data Centre Facility Drawings

|                            |   |
|----------------------------|---|
| 20_099-CSE-00-XX-DR-C-2117 | Proposed Ditch Diversion Layout Plan                    |
| 20_099-CSE-00-XX-DR-C-2116 | Proposed Surface Water Attenuation Basin 2 Layout Plans |
| 20_099-CSE-00-XX-DR-C-2210 | Proposed Overall Foul Water Drainage Layout Plan        |



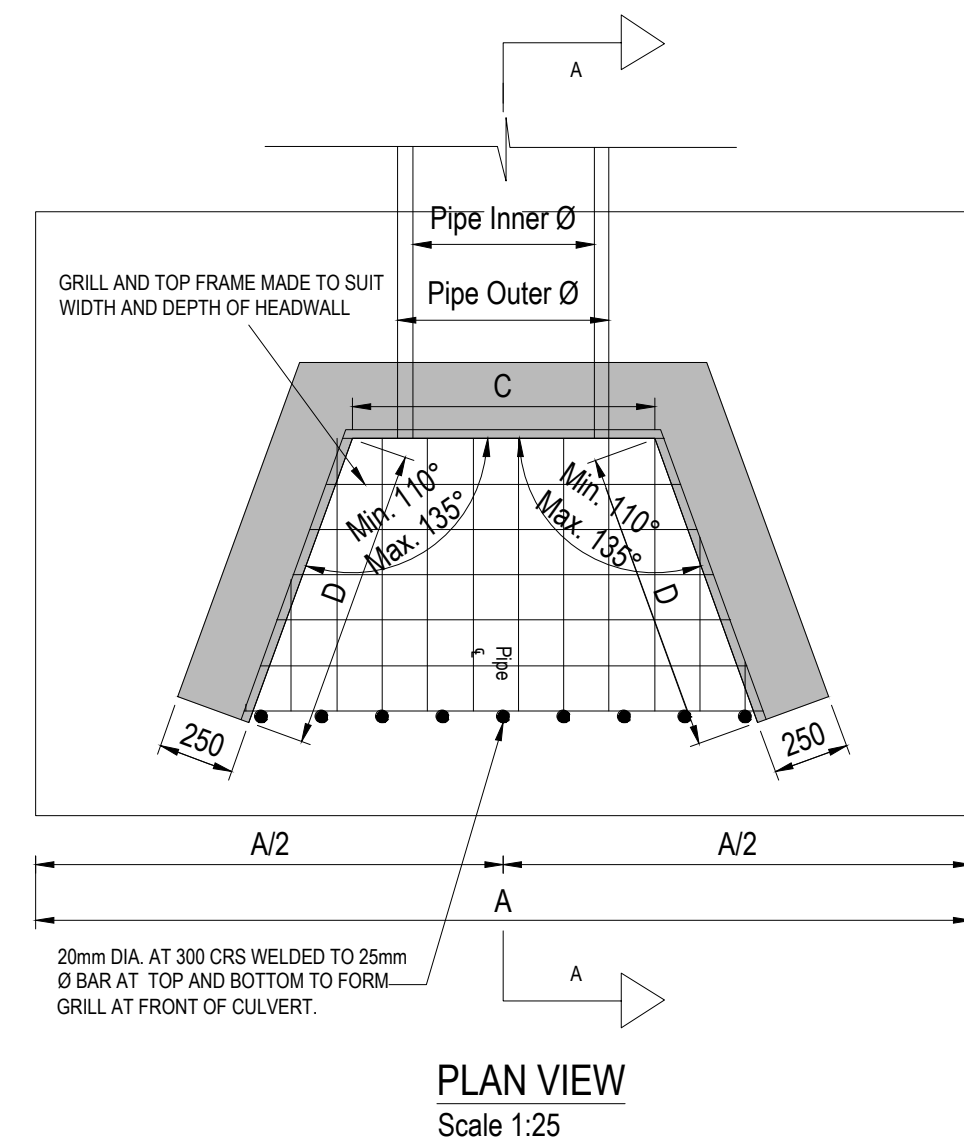


PROPOSED DITCH DIVERSION - LAYOUT PLAN  
Scale: 1:500

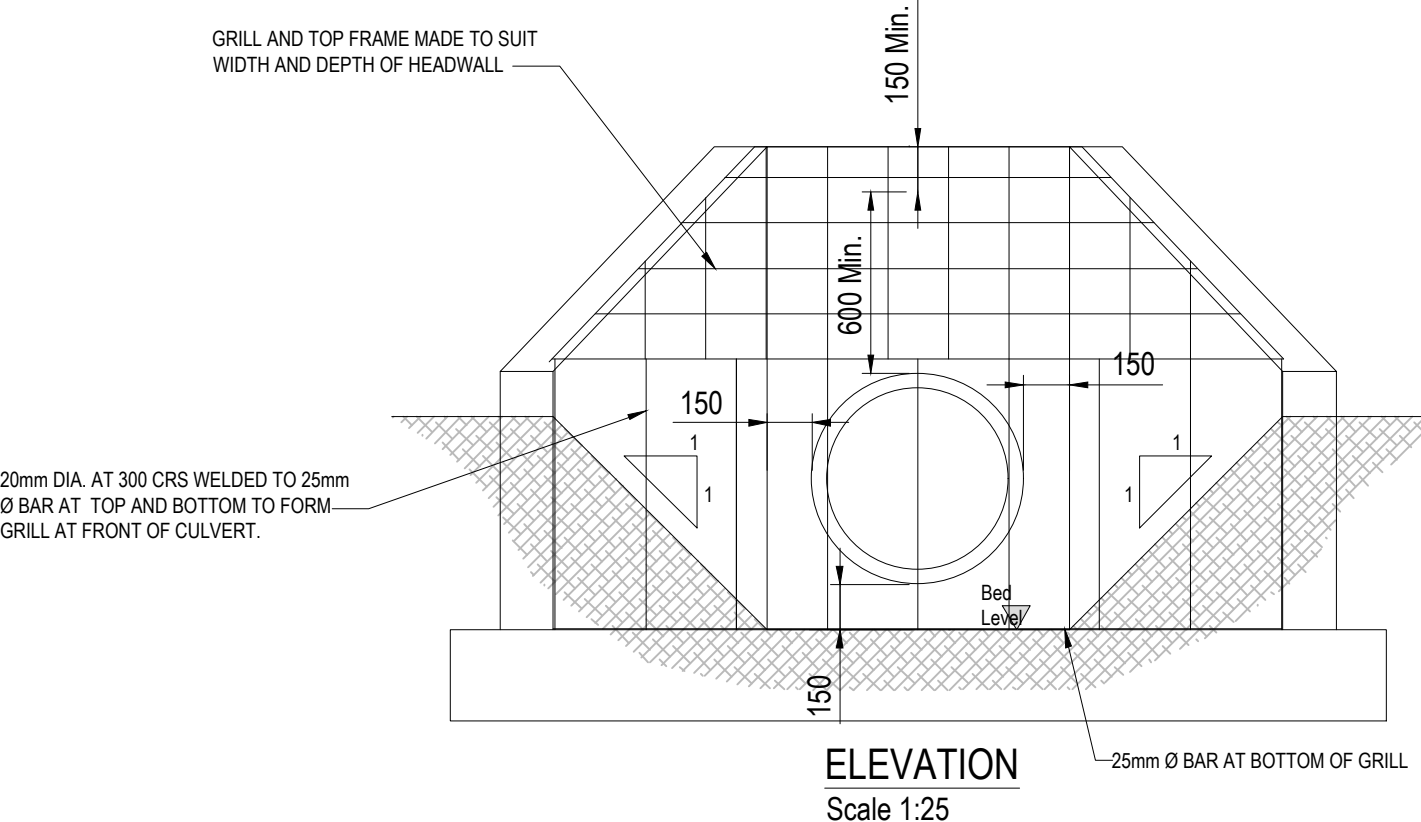


PROPOSED DITCH DIVERSION - PROFILE  
Scale: H 1:500, V 1:100

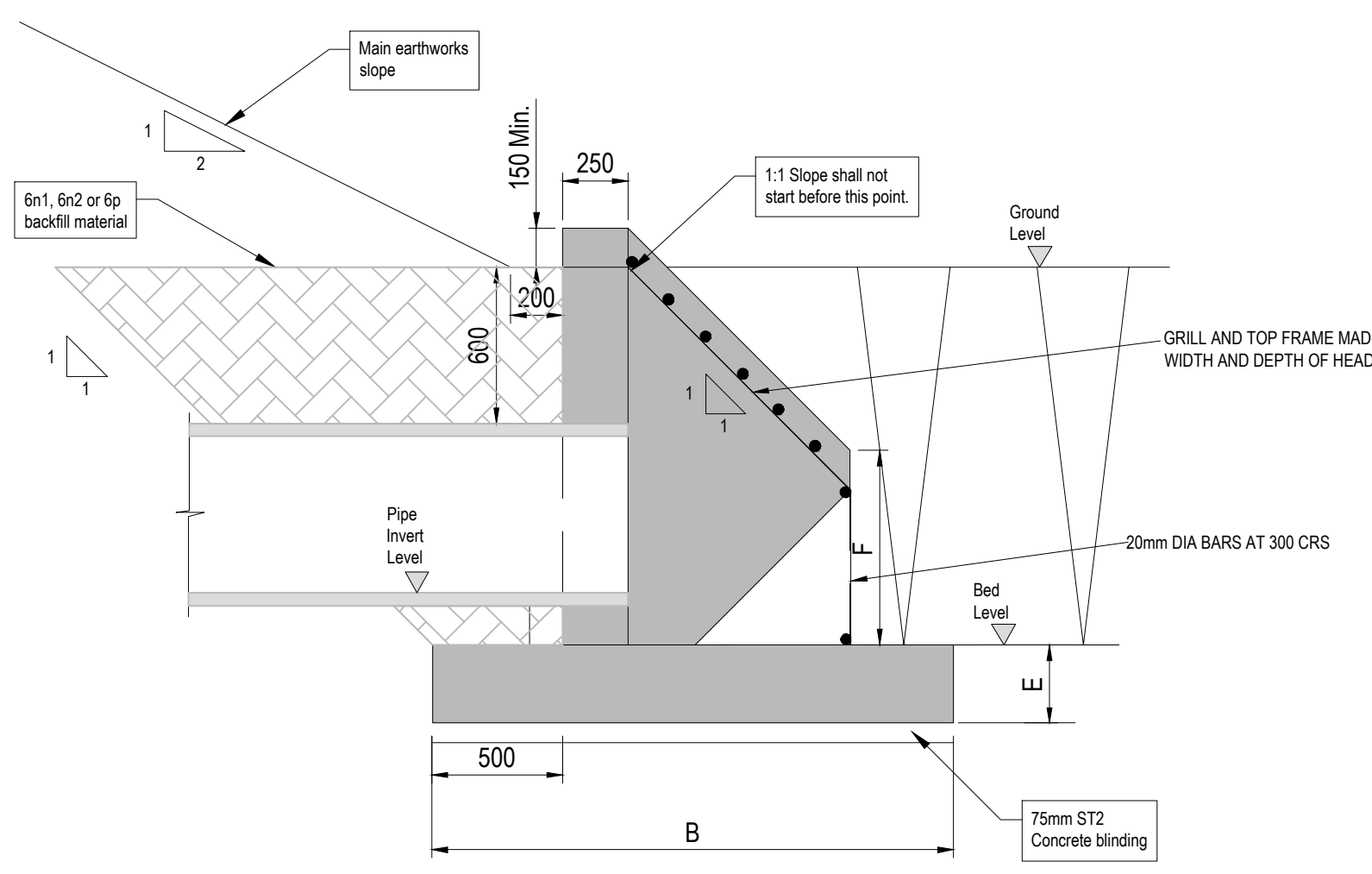
**NOTE:**  
ALL CHAMBERS TO  
HAVE LOCKABLE LIDS.



PLAN VIEW  
Scale 1:25



PROPOSED HEADWALL DETAILS  
Scale 1:25



SECTION A - A  
Scale 1:25

| Schedule of Minimum Dimensions |      |      |                    |      |     |      |
|--------------------------------|------|------|--------------------|------|-----|------|
| Pipe Inner Ø                   | A    | B    | C                  | D    | E   | F    |
| <= 300                         | 2000 | 2000 | Pipe Outer Ø + 300 | 1000 | 400 | 500  |
| 301 - 600                      | 2500 | 2500 | Pipe Outer Ø + 300 | 1250 | 400 | 500  |
| 601 - 900                      | 3000 | 3000 | Pipe Outer Ø + 300 | 1500 | 500 | 700  |
| 901 - 1200                     | 3500 | 3500 | Pipe Outer Ø + 300 | 1800 | 500 | 800  |
| 1201 - 1500                    | 4000 | 4000 | Pipe Outer Ø + 300 | 2100 | 500 | 900  |
| 1501 - 1800                    | 4500 | 4500 | Pipe Outer Ø + 300 | 2350 | 500 | 1000 |

The dimensions contained in the table above are minimums only and the designer shall conform details for specific site conditions. The dimensions contained in the table above are based on the following constraints:

- Angle between headwall and wingwall is 100°.
- Backfill material is free draining.
- There no live load effects on the headwall.
- Characteristic value of internal friction (φ) of the backfill material = 37.5°.
- 600mm cover to the pipe at the rear of the headwall, with a 200mm wide flat area before the commencement of the main slope.
- Slope of fill measured from the rear face of the wingwalls downwards from bed level upwards are both to be 1:1.

**Headwall Notes:**

- All dimensions are in Millimetres.
- This drawing is only to be used in association with a unique structural design. This design is to be carried out in accordance with the NRA Requirements for the use of Eurocodes for the design of road structures.
- Reinforced concrete shall be a minimum grade of C37/40. All structural concrete shall be specified in accordance with Series 1700 of the NRA MCDRW.
- All blinding concrete shall be ST2 in accordance with IS EN 206.
- The Minimum cover to reinforced concrete for durability shall be in accordance with NRA BD 57. Minimum exposure class to be XC4.
- Any exposed concrete surfaces from 100mm below ground level to be class U4/F4. All other surfaces to be class U1/F1 finish unless otherwise specified.
- Headwall wingwalls to be sloped and shall maintain a minimum height of 150mm above adjacent backfill level.
- Rendered concrete blockwork may be used as an alternative to in-situ or precast concrete for pipes up to 300mm inner diameter.
- All headwalls shall be backfilled with class BN1, BN2 or GP backfill material. Headwalls shall be founded on a minimum 75mm layer of ST2 blinding concrete. Details of the sub-base layer to be confirmed based on site conditions.
- Rock armour and/or gabion headwalls and wingwalls are prohibited.

**LEGEND WATERCOURSES:**

- EXISTING DITCH TO BE REGRADED AND RETAINED
- EXISTING DITCH TO BE REMOVED AND BACKFILLED
- EXISTING DITCH TO BE RETAINED
- DIVERSION OF DITCH
- FLOW DIRECTION

ST1  
IL: 76.560  
ST2  
IL: 77.000

EXISTING BED LEVEL OF  
DITCH

| Rev | Description              | Drawn | Checked | Date       |
|-----|--------------------------|-------|---------|------------|
| P04 | ISSUED FOR PLANNING      | DM    | CD      | 04.08.2021 |
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| P01 | DRAFT ISSUE FOR PLANNING | DM    | CD      | 02.03.2021 |



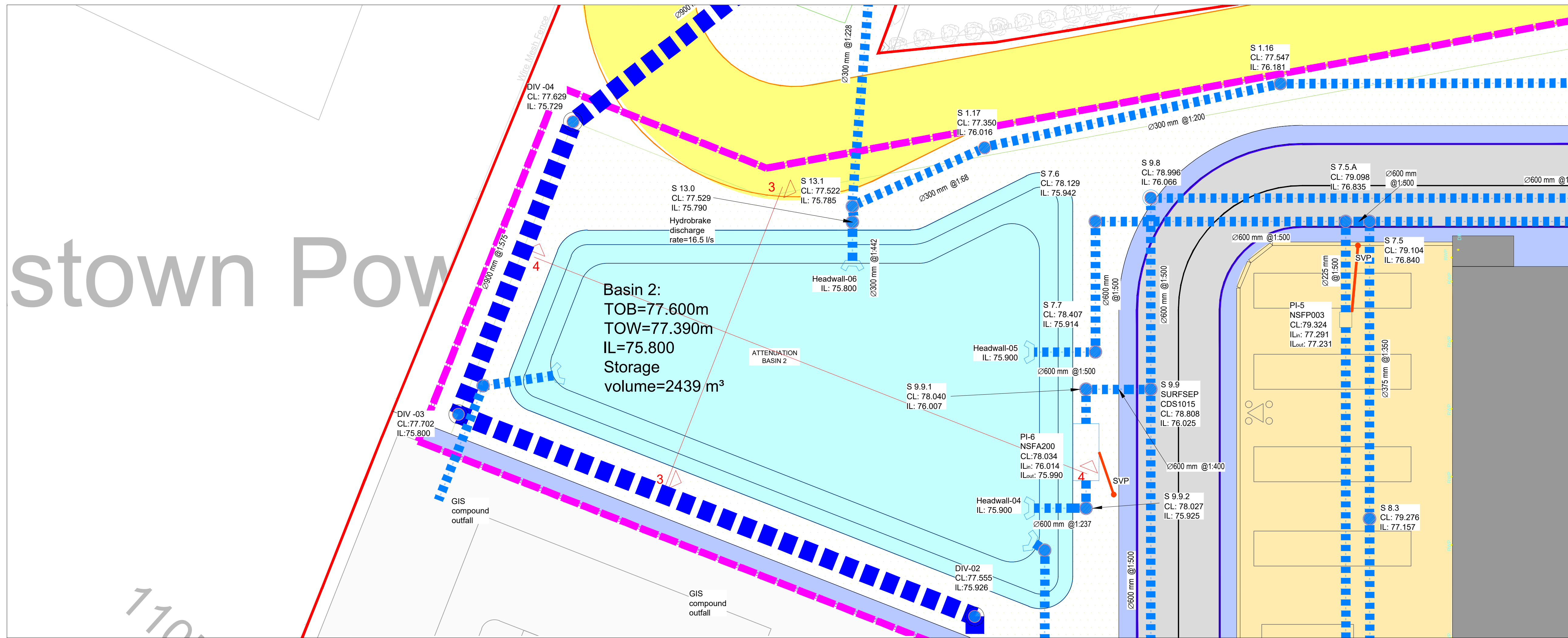
**HUNSTOWN POWER  
COMPANY LTD**

**PROPOSED WATERCOURSE DIVERSION  
LAYOUT & SECTIONS - SHEET 1**

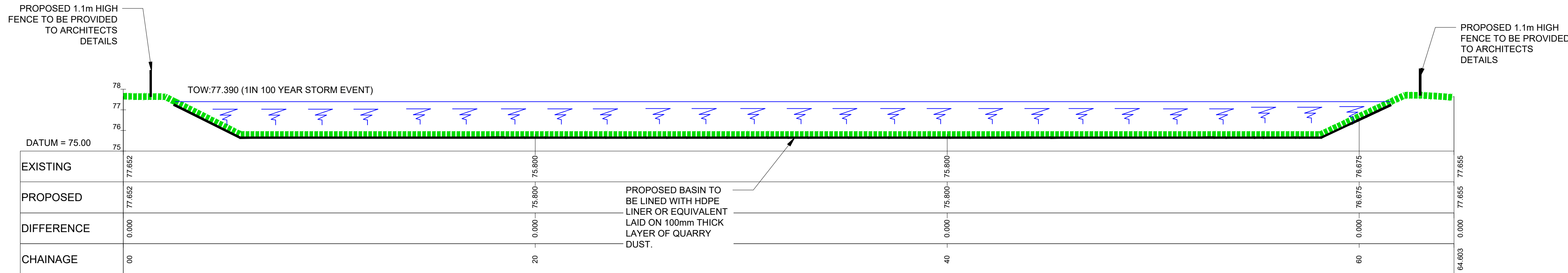
Drawn By: DM Date: MARCH 2021  
Checked By: CD AS INDICATED @ A0  
Project Code: 20\_099 - CSE - 00 - XX - DR - C - 2117  
Status Code: S2 Suitability Description: SUITABLE FOR INFORMATION

Project Status: PLANNING

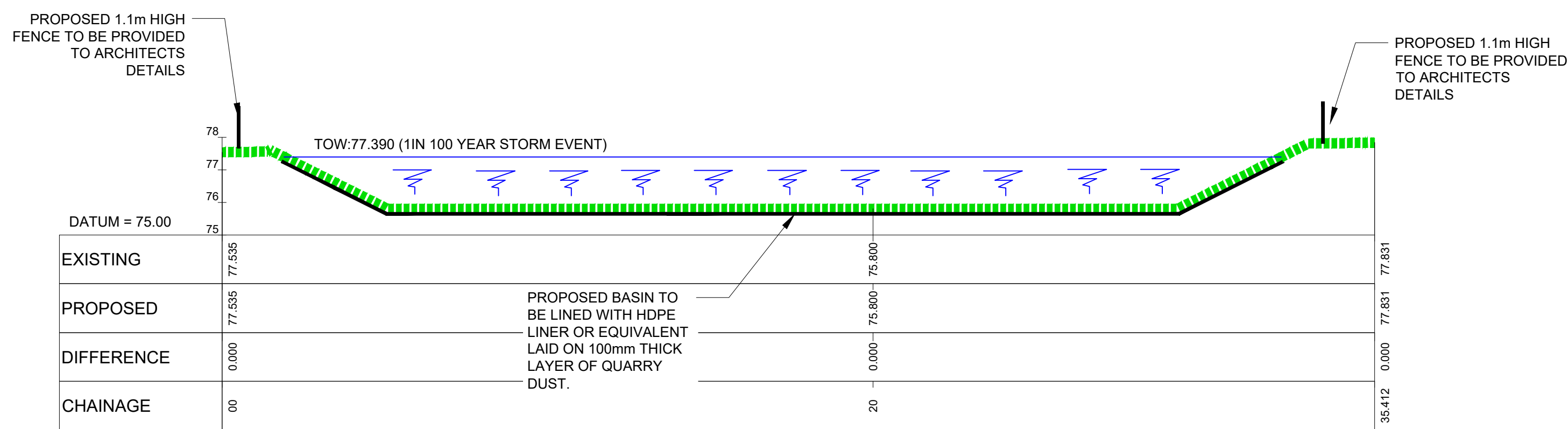




ATTENUATION BASIN 2 LAYOUT PLAN  
SCALE 1:250



BASIN 2(3-3) - PROFILE  
SCALE: H 1:125,V 1:125



BASIN 2(4-4) - PROFILE  
SCALE: H 1:125,V 1:125

| PETROL INTERCEPTOR DESIGN INFORMATION |                |       |                                       |                        |                  |
|---------------------------------------|----------------|-------|---------------------------------------|------------------------|------------------|
| Ref                                   | Type           | Class | Model Specification (by Manufacturer) | Design Flow Rate (l/s) | Oil Capacity (l) |
| PI-1                                  | Full Retention | 1     | NSFP003                               | 3                      | 30               |
| PI-2                                  | Full Retention | 1     | NSFA200                               | 200                    | 200              |
| PI-3                                  | Full Retention | 1     | NSFP003                               | 3                      | 30               |
| PI-4                                  | Full Retention | 1     | NSFA200                               | 200                    | 200              |
| PI-5                                  | Full Retention | 1     | NSFP003                               | 3                      | 30               |
| PI-6                                  | Full Retention | 1     | NSFP003                               | 3                      | 30               |
| PI-7                                  | Bypass         | 1     | NSBE020                               | 20                     | 300              |

GENERAL NOTES:

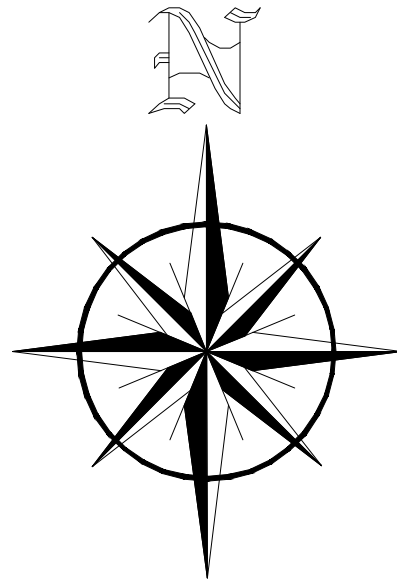
- THIS DRAWING TO BE READ IN CONJUNCTION WITH ALL RELEVANT DRAWINGS AND SPECIFICATIONS
- DO NOT SCALE DIMENSIONS
- THE CONTRACTOR SHALL CHECK ALL DIMENSIONS PRIOR TO CONSTRUCTION. ANY DISCREPANCIES TO BE NOTIFIED TO CSEA
- TEMPORARY SUPPORTS TO THE SIDES OF THE EXCAVATION MAY BE REQUIRED DEPENDENT ON SUBSOIL. METHOD OF WORK AND SITE CONSTRAINTS, AND ARE TO BE AGREED WITH THE ENGINEER PRIOR TO COMMENCEMENT OF EXCAVATION. SIDE SLOPES OF AN UNSUPPORTED EXCAVATION DEPENDANT UPON SUBSOIL, AND SHALL BE AGREED WITH THE ENGINEER
- MAIN CONTRACTOR TO PROVIDE A METHOD STATEMENT AND RISK ASSESSMENT FOR THE EXCAVATION WORKS FOR THE ER TO REVIEW
- THE CONSTRUCTION, AS SHOWN, IS APPLICABLE ONLY WHERE SUBSOIL AT FORMATION LEVEL EXCEEDS 100kN/m² BEARING CAPACITY
- ALL MATERIALS AND WORKMANSHIP TO BE IN ACCORDANCE WITH THE CIVIL WORKS SPECIFICATION

SURFACE WATER NOTES:

- STORM SEWER PIPES TO BE ADS HDPE TWINWALL IN ACCORDANCE WITH EN13476. FOR ALL STORMWATER DRAINAGE FOR PIPES < 450mm IN DIAMETER.
- CONCRETE PIPES TO BE SPECIFIED ON PIPE DIAMETERS OF 450mm AND ABOVE.
- ALL RWP's CONNECTIONS ARE 150mm WELDED HDPE WITH 90° SLOW RADI BENDS SADDLED INTO MAIN SURFACE WATER DRAINAGE.
- FOR ALL MANHOLE DETAILS, PIPE BEDDING, SURROUND AND HAUNCHING DETAILS AS PER DWG DUB40-CSE-00-XX-DR-C-F-4806. MANHOLE COVERS & FRAMES, ROAD GULLIES, TESTING & CLEANING OF DRAINS AND SEWER DIVERSIONS, REFER TO THE CIVIL WORKS SPECIFICATION AND GREATER DUBLIN REGIONAL CODE OF PRACTICE FOR DRAINAGE WORKS VERSION 6.0 WHICH IS PROVIDED IN THE INFORMATION PACK.
- GULLY CONNECTIONS SHALL COMPLY WITH THE CIVIL WORKS SPECIFICATION, SECTION 11 AND SECTION 14.7 OF GREATER DUBLIN REGIONAL CODE OF PRACTICE FOR DRAINAGE WORKS VERSION 6.0.
- ALL MANHOLES SHALL BE IN ACCORDANCE WITH THE FOLLOWING DETAILS OUTLINED IN APPENDIX 1 GREATER DUBLIN REGIONAL CODE OF PRACTICE FOR DRAINAGE WORKS VERSION 6.0 OF THE FOLLOWING:-
  - MANHOLES WHERE LESS THAN 1m COVER TO TOP OF PIPE SHALL BE TYPE A;
  - MANHOLES WITH BETWEEN 1m AND 3m COVER TO TOP OF PIPE SHALL BE TYPE J;
  - MANHOLES WITH GREATER THAN 3m COVER TO TOP OF PIPE SHALL BE TYPE K;
- ALL MANHOLES ON DRAINS OF 450mm DIAMETER AND OVER SHALL BE PROVIDED WITH SAFETY CHAINS FOR PLACING ACROSS THE MOUTH OF THE DRAIN ON THE DOWNSTREAM SIDE OF THE MANHOLE. MILD STEEL SAFETY CHAIN SHALL BE 12mm NOMINAL SIZE GRADE M (4) NON-CALIBRATED CHAIN, TYPE 1, COMPLYING WITH BS EN 818: PART 3. CHAINS SHALL BE HOT DIP GALVANISED TO BS EN ISO 1461. CHAINS SHALL BE SECURED ONLY BY A SAFETY EYEBOLT TO BS 7883: 2005 WITH A STANDARD SCREW GATE RABBITER TO BS EN 362.
- VERTICAL BACKDROP IN MANHOLES SHALL BE IN ACCORDANCE WITH TYPE G MANHOLE DETAIL IN APPENDIX 1 TO THE GREATER DUBLIN REGIONAL CODE OF PRACTICE FOR DRAINAGE WORKS VERSION 6.0.
- ALL COVERS AND GRATINGS SHALL COMPLY BE CLASS D400 TO EN 124.
- ATTENUATION BASIN ABBREVIATIONS  
TOB = TOP OF BANK  
TOW = TOP OF WATER LEVEL FOR 1 IN 100 YEAR EVENT

DRAWING IS PRODUCED USING THE  
IRISH TRANSVERSE MERCATOR (ITM)  
GEOGRAPHIC COORDINATE SYSTEM

A0



LEGEND:

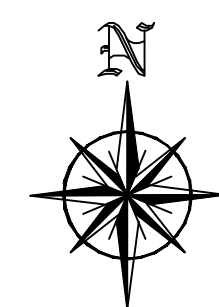
- Proposed Soft Landscape Refer to Landscape Architect Details
- Proposed Concrete Pavement
- Proposed Concrete Footpath
- Proposed Roads
- Proposed Building
- Proposed Permeable Parking
- Proposed Attenuation Basins
- Proposed ESB Wayleave for Diverted Overhead Lines
- Outline of the Site Subject to this application
- Proposed Security Fence Type 1 to Architects Details
- Proposed Security Gates/Barriers to Architects Details
- Proposed Kerb
- Proposed Drainage Kerb
- Proposed Retaining Wall
- Proposed Aco Drain
- Proposed Surface Water Network
- Proposed SW Manhole
- Proposed Ditch to be Retained/Regraded
- Proposed Ditch Flow Direction
- Proposed Diverted Ditch Route. Refer to Drawing No. 2117 for Details
- Proposed Vent Pipe to Terminate 2.5m above Ground Level.
- Proposed Headwall. Refer to Drawing No. 2117 for Details

| Rev | Description              | Drawn | Checked | Date       |
|-----|--------------------------|-------|---------|------------|
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**HUNSTOWN POWER COMPANY LTD**  
Client  
**HUNSTOWN DATA CENTRE FACILITY**  
Project  
**PROPOSED ATTENUATION BASIN LAYOUT & SECTIONS - SHEET 2**  
Dep. Title  
Drawn By: DM Date: MARCH 2021  
Checked By: CD AS INDICATED @ A0  
Project Code: 20\_099 - CSE - 00 - XX - DR - C - 2116  
Status Code: S2 SUITABLE FOR INFORMATION  
Revision: P04 PLANNING





| PUMPING STATION DESIGN INFORMATION |                                       |                     |              |                                 |                         |                             |                             |                                 |                              |  |
|------------------------------------|---------------------------------------|---------------------|--------------|---------------------------------|-------------------------|-----------------------------|-----------------------------|---------------------------------|------------------------------|--|
| Ref                                | Network                               | Pump<br>Dia.<br>(m) | Depth<br>(m) | Design<br>Flow<br>Rate<br>(l/s) | Static<br>Head<br>(l/s) | Rising<br>Main<br>Ø<br>(mm) | Rising<br>Main<br>Ø<br>(mm) | Friction<br>Head<br>Loss<br>(m) | Total<br>Head<br>Loss<br>(m) | Storage<br>Volume<br>Available<br>(m³) |
| PS1                                | DOMESTIC<br>FOUL<br>WATER<br>DRAINAGE | 2.4                 | 5.831        | 3.76                            | 3.891                   | 80                          | 186                         | 1.77                            | 5.838                        | 20.0                                   |
| PS2                                | COOLING<br>WATER<br>DRAINAGE          | 2.4                 | 5.179        | 5.89                            | 6.0                     | 100                         | 255                         | 1.78                            | 7.96                         | 20.0                                   |

Ks=0.15mm  
Design Velocity = 0.75m/s  
Assume additional 10% of Friction Head Loss for head loss due to fittings

## LEGEND:

- Proposed Soft Landscape  
Refer to Landscape Architect  
Details
- Proposed Concrete Pavement
- Proposed Concrete Footpath
- Proposed Roads
- Proposed Building
- Proposed Permeable Parking
- Proposed Attenuation Basins  
Refer to Drawings No. 2115 & 2116  
for Details
- Proposed ESB Wayleave  
for Diverted Overhead Lines
- Outline of the Site Subject  
to this application
- Proposed Security Fence Type 1  
to Architects Details
- Proposed Security Gates/Barriers  
to Architects Details
- Proposed Kerb
- Proposed Drainage Kerb
- Proposed Retaining Wall
- Proposed Tactile Paving & Drop  
Kerb. Refer to Drawing  
No. 2900 for Details.
- Proposed Foul Water  
Network Sewer
- Proposed FW Manhole
- Proposed 80mm DIA Foul  
Water Raising Main
- Proposed Cooling Water  
Discharge Sewer
- Proposed Cooling Water  
Discharge Manhole
- Proposed 100mm DIA  
Cooling Rising WM Main
- Existing Foul Sewer
- Existing FW Manhole

## GENERAL NOTES:

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HUNTSTOWN POWER  
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HUNTSTOWN DATA CENTRE FACILITY

PROPOSED OVERALL FOUL WATER  
LAYOUT PLAN

Drawn By: DM Date: MARCH 2021  
Checked By: CD Scale: 1:1000 @ A0  
Project Code: 20\_099 - CSE - 00 - XX - DR - C - 2210

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P04 PLANNING



